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TECHNICAL NOTE

D-421

INVESTIGATION AT TRANSONIC SPEEDS
OF LOADING OVER A 30° SWEPTBACK WING OF ASPECT
RATIO 3, TAPER RATIO 0.2, AND NACA 65A004 AIRFOIL
SECTION MOUNTED ON A BODY

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NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
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SPEEDS OF LOADING OVER A 30 DEG SWEETBACK
WING OF ASPECT RATIO 3, TAPER RATIO 0.2, AND
NACA 65A004 AIRFOIL SECTION MOUNTED ON A
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SUMMARY

The aerodynamic load characteristics of a wing-body combination were determined experimentally at Mach numbers from 0.80 to 1.03 for angles of attack up to 26 degrees. Two wings, both with 30° sweep of the quarter-chord line, taper ratio of 0.2, aspect ratio of 3, and thickness of 4 percent chord, but of different types of construction, were tested. One wing was of solid steel and the other was of plastic with an inner steel core.

The load distributions for both wings were similar, but loads on the more flexible wing were somewhat reduced. The twist distributions for both wings were calculated. Some typical flow studies of the boundary layer are presented.

INTRODUCTION

Satisfactory stability characteristics have been obtained at subsonic speeds for thin low-aspect-ratio wings with moderate leading-edge sweep (ref. 1). In order to evaluate in detail the load and stability characteristics of this type of wing on a body of revolution throughout the transonic speed range, a wing with an aspect ratio of 3, a taper ratio of 0.2, 30° sweepback of the quarter-chord line, and with NACA 65A004 airfoil sections was selected and the load characteristics are presented. The longitudinal stability characteristics are presented in reference 2. This wing is one of several wings being studied in a general program at the Langley 16-foot transonic tunnel. To date, the load characteristics of other wings in the program have been published in references 3, 4, 5, and 6. Data were obtained at Mach numbers from 0.80

¹Supersedes declassified NACA RM L57G09a by Donald D. Arabian, 1957.

to 1.03 for angles of attack up to about 26° for two wings of the same geometry but constructed of different materials. One wing was made of steel and plastic in an attempt to devise a cheaper and faster method of wing construction. The other was a solid steel wing used for comparison to check the effect of aeroelasticity and to establish the validity of data obtained with the less-rigid reinforced plastic wing. The twist distribution due to aerodynamic loading was calculated for both wings. Some typical flow studies of the boundary layer are also presented.

SYMBOLS

b	wing span
c	wing chord parallel to the plane of symmetry
\bar{c}	average wing chord
c'	mean aerodynamic chord
c_n	wing section normal-force coefficient
c_m	section pitching-moment coefficient about the wing mean aerodynamic chord
c_N	wing-panel normal-force coefficient, $\int_{0.16}^{1.0} c_n \frac{c}{\bar{c}} d\left(\frac{2y}{b}\right)$
c_m	wing-panel pitching-moment coefficient about $0.25c'$, $\int_{0.16}^{1.0} c_m \frac{c^2}{\bar{c}c'} d\left(\frac{2y}{b}\right)$
c_p	pressure coefficient, $\frac{\Delta p}{q}$
M	Mach number
Δp	local static pressure minus the free-stream static pressure
q	dynamic pressure
x	distance parallel to the center line
y	distance normal to the plane of symmetry

α model angle of attack

θ angle of twist of the chord line measured in planes parallel to the plane of symmetry

MODEL DESCRIPTION

The general arrangement of the model is shown in figure 1(a). The wing was mounted to the same steel body of revolution used in references 4 and 5. The fuselage had a fineness ratio of 11, an ogive nose, cylindrical center section and a boattail afterbody. The wing was swept 30° at the quarter-chord line with a taper ratio of 0.2, and aspect ratio of 3, and NACA 65A004 sections parallel to the plane of symmetry. Two wings were constructed of different materials. Figure 1(b) shows typical cross sections of both wings. One was constructed entirely of steel with a leading-edge section and a trailing-edge section which was tongue and grooved to a center section. The spaces left in the grooves were used as ducts for the pressure tubes to the orifices. The other wing was constructed in such manner that a steel core with a thin brass plate at the trailing edge was surrounded with the wing pressure tubes, and then polyester resin was poured about the structure to form the wing contour. This wing hereinafter is called the plastic wing.

The twist characteristics for these wings were determined by the method described in appendix A. The steel wing was found to be less than half as flexible as the plastic wing. The influence coefficients A_{ij} and B_{ij} (see appendix A) used to calculate the twist were as follows:

For the steel wing:

i	$A_{ij} \times 10^{-5}$ at $j = -$				
	1	2	3	4	5
1	0	0	0	-1	-4
2	-2	6	-2	-8	-13
3	-2	5	9	-9	-28
4	1	4	7	11	-27
5	1	4	5	12	-5

i	$B_{ij} \times 10^{-5}$ at $j = -$				
	1	2	3	4	5
1	0	0.1	0.1	0.2	-0.3
2	-.1	1.3	1.1	.9	.3
3	-.1	1.7	3.9	3.2	.3
4	.3	1.7	4.9	11.5	10.5
5	.3	1.8	4.8	14.1	37.9

For the plastic wing:

i	$A_{ij} \times 10^{-5}$ at $j = -$				
	1	2	3	4	5
1	0	-2	-3	-6	-11
2	-1	7	-7	-22	-34
3	1	9	8	-31	-78
4	2	9	14	-2	-100
5	2	9	14	6	-69

i	$B_{ij} \times 10^{-5}$ at $j = -$				
	1	2	3	4	5
1	0	0.3	1.0	0.8	1.1
2	-0.1	1.9	1.8	0	3.1
3	.1	3.3	7.0	7.3	7.6
4	.2	3.5	10.4	23.1	33.4
5	.2	3.5	11.1	30.2	90.8

where A_{ij} and B_{ij} represent the twist in degrees measured parallel to the angle-of-attack plane at the i th station due to a load or moment at the j th station, respectively. The five spanwise stations chosen were located as follows:

Station	$\frac{y}{b/2}$
1	0.245
2	.412
3	.580
4	.750
5	.915

A better comparison of the twist characteristics, however, of the steel and plastic wing is shown in figures 2(a) and (b). The plots show the effect of a unit loading applied at any spanwise station (abscissa), on the particular spanwise stations 1 through 5, for loadings at the 25- and 65-percent-chord lines. The main difference between the two plots results from a change in the stiffness and a shift of the elastic-axis location of the two wings. If the elastic axis is defined as that point of the local chord which gives zero twist when a load is applied at the point, then figure 2 indicates the position of the elastic axis. The plots show that the elastic axis of the plastic wing passes through the 0.25c at about the 0.75b/2 station, while that of the steel wing passes through the 0.25c at the 0.85b/2 station. Inboard of these spanwise stations the elastic axis lies behind the 0.25c line (positive values of twist), and outboard the axis lies ahead of the 0.25c line (negative values of twist).

The rows of pressure orifices were located at 16, 25, 40, 60, 75, and 95 percent semispan stations for both the steel and plastic wings. In each row on both the upper and lower surfaces, the orifices were

located at 1, 2, 5, 7, 10 percent c and at intervals of every 5 percent chord thereafter up to the 95-percent-chord station.

TESTS AND TECHNIQUES

The tests were conducted in the Langley 16-foot transonic tunnel, which is described in reference 7. The Mach number range extended from 0.80 to 1.03, which corresponded to a Reynolds number range from about 7×10^6 to 8×10^6 (based on the wing mean aerodynamic chord). The maximum angle-of-attack range extended from -2° to 26° in 2° increments.

The pressure data were obtained simultaneously with the force data presented in reference 2. The wing pressures were recorded by photographing mercury manometer boards. The data were then processed by electronic calculating machines, which plotted and tabulated the results.

At the termination of the pressure program, a study was made of the flow in the boundary layer of the plastic wing for a reduced Mach number and angle-of-attack range. The technique used in reference 5 was employed to render the flow visible. The technique entails painting the wing surface black and then applying a white ground-glass paint similar to china clay. The wing therefore appears white when dry. Wetting with a clear fluid causes the black sublayer to become visible. Thus, by emitting fluid from a point source on the wing in a stream, the fluid path in the boundary layer is traced. As the fluid trace changes with time, the history of the trace disappears as a result of the evaporation of the fluid, so that the existing trace represents an average flow for a short interval of time. For these tests clear varsol was used as the liquid agent. The point sources were particular pressure orifices through which the fluid was forced. The locations of the sources were as follows:

$\frac{x}{c}$ at -				
$0.25 \frac{b}{2}$	$0.40 \frac{b}{2}$	$0.60 \frac{b}{2}$	$0.75 \frac{b}{2}$	$0.95 \frac{b}{2}$
0.5	0.5	0.5	0.5	0.5
.10	----	----	----	----
.15	.15	----	----	----
.20	.20	----	----	----
.25	.25	.25	.25	----
----	.35	----	----	----
.45	.45	.45	.45	.45
.65	.65	.65	.65	----
.80	.80	.80	.80	.80
.90	.90	.90	.90	----

The flow studies were recorded photographically.

ACCURACY OF MEASUREMENTS

Sufficient time was allowed after a particular test condition was reached for the pressure manometer tubes to settle within about 1 percent of the ultimate value of the manometer level.

The indicated angle of attack was corrected for tunnel-flow angularity. Based on readout accuracy and repeatability, the angle of attack and Mach number are believed to be accurate within the following limits:

α , deg	±0.01
M	±0.005

RESULTS AND DISCUSSION

Flow studies.- Sample photographs of the flow on the right plastic wing are presented in figure 3. No general discussion of swept-wing flow is attempted here. Only those features of the flow studies which represent significant characteristics to be noted in the following wing pressure discussion are covered. A general discussion of the flow over swept wings may be found in references 8, 9, and 10.

Some of the features of the boundary flow which can be noted in the photographs of figure 3 are the indications of shock waves, the indications of flow separation, and the indications of vortex-type flow.

Shock waves are frequently indicated by the fluid path where there are abrupt changes of the streamlines. Note in figure 3(a) at $M = 0.94$ that shadowgraph traces of the waves are visible at angles of attack of 2° and 4° (indicated by the arrows on the figure), and note how the fluid lines are altered where they intersect the wave. The location of the waves is more obvious at the higher angles of attack by the more abrupt turning of the flow.

Separation first appears as an irregular darkened region generally increasing in area with increasing angle of attack. For this wing there appear to be two different areas where separation may commence, depending on the Mach number. At $M = 0.80$ for example, figure 3(a) at $\alpha = 4^\circ$ shows the separation to start along the leading edge near the wing tip. This results from a combination of a swept leading edge, a small leading-edge radius, and a thin wing. At the higher Mach numbers leading-edge separation as such occurs only at much higher angles of attack. (Compare 0.80 with 0.94 and 1.03 Mach numbers of fig. 3(a) for $\alpha = 6^\circ$.) However, separation does start near the tip at the trailing edge before the leading-edge separation occurs. See figure 3(a) at $\alpha = 6^\circ$ for

$M = 0.94$ and figure 3(b) at $\alpha = 10^\circ$ for $M = 1.03$. This separation appears to stem from the intersection, in the vicinity of the wing tip, of the shocks originating at the leading edge and near the trailing edge of the wing-body juncture. Both types of separation extend inboard with increasing angle of attack.

Once separation occurs, the existence of vorticity in the flow above the wing is indicated in the boundary-layer traces by the circulation of the fluid lines in a counterclockwise direction. For example, observe the photographs for $M = 0.80$ at the higher angles of attack. A line through the aftermost points along each of the indicated streamlines should coincide with the projection of the vortex core on the wing surface. Note that at $\alpha = 6^\circ$, the vortex cone sheds near the tip and the point of shedding progresses inboard with increasing angle of attack, as does the separation. At $\alpha = 19^\circ$ (fig. 3(c)) the vortex appears to shed at about $0.25b/2$. The vortex strength at this angle of attack is much greater than at the lower angles of attack, as is shown by the accumulation of the fluid near the vortex origin.

The origin of the vorticity at $M = 0.94$ and $M = 1.03$ appears to be in the vicinity of the intersection of the shock waves where the separation forms. Vorticity is permitted at the shock intersection since different entropy changes occur inboard and outboard of the intersection. The angle of attack at which this vortex forms increases with Mach number. With increasing angle of attack at the higher Mach numbers, the vortex flow finally reverts to a vortex generated along the leading edge once the leading-edge separation occurs at the higher angles of attack.

Chordwise pressure distributions.—A tabulation of the chordwise pressure coefficients for all test conditions for the steel wing is presented in table I. Figure 4 presents a comparison between the chordwise pressure distributions for the plastic and steel wings. As is noted, there are minor differences in the angles of attack for the two wings. In general these differences are of the order of the accuracy of measurements of these angles ($\pm 0.10^\circ$). The differences in the pressure coefficient with one exception may therefore be considered to be caused principally by aeroelastic effects. A significant difference in the variation of the chordwise pressure distributions exists between the two wings at angles of attack from about 2° to 8° at a Mach number of 0.80. As this Mach number was the first for which data were obtained, the discrepancy suggests a temporary difference in the leading-edge surface conditions for the two wings. The plastic-wing flow studies of figure 3(a), which were taken after the pressure tests, for angles of attack of 4° and 6° at a Mach number of 0.80 indicated separation at the outer spanwise stations, but the pressure distributions of the plastic wing indicated attached flow. The outboard stations of the plastic wing generally show the effect of decreased local angles of attack due to load when compared to the steel wing.

For either wing at the low angles of attack the increase in load coefficient progressing toward the tip illustrates the effective spanwise increase of angle of attack induced by the trailing vortices of a highly tapered swept wing. Consequently, the separation appears first at the tip and progresses inboard with increasing angle of attack as indicated by the flow studies of figure 3.

The pressure distributions on the upper surface are fairly constant over most of the wing panel at an angle of attack of about 20° , which of course indicates separation. Increasing the angle above 20° produces more negative pressure coefficients and, in addition, the innermost station shows signs of the streamlines being turned downward toward the wing surface; that is, the pressures near the trailing edge begin to recover or increase in a positive sense. As the angle of attack is further increased this effect tends to progress outboard. These pressure changes are believed to be caused by the change in location and the increasing strength of the vortex that is shown in figure 3 at $M = 0.80$. At $M = 0.94$ to 1.03 for the high angles of attack, the distributions near the root are also influenced by the strong shock wave shown by the chordwise distributions.

Spanwise load distributions.- It is apparent from the chordwise pressures that the type of wing construction, with some exceptions, has only minor effects on load distribution; therefore, the spanwise load distributions are presented only for the steel wing in figure 5. The distributions are nearly elliptical at the low angles of attack, but as the angle of attack increases, the load distributions tend to become triangular, with the triangular loading commencing at the tip. The triangular distribution spreads inboard as separation forms with further increase of angle of attack. At the angles of attack where the load distribution is elliptical inboard and triangular outboard, increasing Mach number tended to reduce the extent of the triangular loading. The implication is that increasing Mach number at a high constant angle of attack extends the attached flow region outboard. This implication is verified by the flow studies (fig. 3(c)). Note that at angles of attack of 15° and 17° , the higher the Mach number, the larger the region of attached flow.

Panel loads.- The variation of the integrated wing loads with angle of attack is shown in figure 6 for the test Mach number range. If compressibility effects are considered, the load-carrying capacity per unit angle of attack should increase to a maximum at approximately $M = 1.00$.

The data show that, for C_N values up to about 0.6, the maximum load-carrying capacity per unit angle of attack occurred at $M \approx 0.94$. For C_N values from 0.6 to the highest test value, the maximum load-carrying capacity occurred at $M \approx 0.98$.

A comparison of the variation of the panel pitching-moment coefficient about the $0.25c'$ with normal-force coefficient and the wing-body pitching-moment data of reference 2 is shown in figure 7. The changes of the slopes $\frac{dC_m}{dC_N}$ with normal-force coefficient agree in general with those of the data of reference 2. The absolute differences in $\frac{dC_m}{dC_N}$ at a given normal-force coefficient are due to the absence of the fuselage stability contribution in the present data.

Center of loads.- Figure 8 presents the exposed panel load centers and the local section load centers for the angle-of-attack and Mach number range of the tests. The spanwise center of load was located at approximately 50 percent of the semispan for all test conditions. The most rearward position was at about 46 percent of the mean aerodynamic chord for the panel load centers and 46 percent of the local chord for the section load centers.

Increasing angle of attack up to about 20° tended to shift the panel center of load rearward and inboard. The single data point for α above 20° shows a tendency for the center of load to become invariant with the higher angles of attack. In general the effects of changes in angle of attack on the center of load decrease with increasing Mach number; this result is to be expected since the chordwise load distribution becomes more rectangular as the flow becomes supersonic over most of the wing.

Twist distribution.- Combining the influence coefficients and the integrated normal forces and moments in the manner described in appendix A or by the method of reference 5 yields the wing spanwise twist distributions. The dynamic pressures corresponding to the measured loads are presented in figure 9 for the test Mach number range. Calculations were made for both wings at angles of attack of 4° , 8° , and 20° and for $M = 0.80$ and 1.00 . A comparison of the resulting spanwise twist distributions for the steel and plastic wings is presented in figures 10(a) and 10(b). At $\alpha = 20^\circ$ and $M = 1.0$ the calculated twist angle of the tip of the plastic wing was -0.9° as compared to -0.4° for the steel wing.

CONCLUDING REMARKS

The following remarks are drawn from the loads investigation of an all steel wing and a geometrically identical reinforced plastic wing. Both wings have 30° sweepback of the quarter chord, a taper ratio of 0.2, and embody NACA 65A004 airfoil sections.

The chordwise pressure distributions for the steel and plastic wings were similar for the test range with some exceptions at Mach number 0.80.

However the type of construction had only minor effects on the chordwise and spanwise load distributions. The order of magnitude of the tip twist was calculated at a Mach number of 1.0 and an angle of attack of 20° to be -0.9° for the plastic wing as compared to -0.4° for the steel wing. The spanwise load distributions were nearly elliptical at the low angles of attack, but at the higher angles the distributions tended to become triangular commencing at the tip. The center of load on the wing panels moved rearward and inboard with increasing angle of attack for all Mach numbers. The movement of the load center with angle of attack decreased considerably with increasing Mach number.

Langley Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., June 19, 1957.

APPENDIX A

METHOD OF COMPUTING WING TWIST DUE TO AERODYNAMIC LOADING

If the spanwise and chordwise distribution of aerodynamic loading of an elastic wing are known, the twist distribution of the wing can be calculated, as follows

$$\{\theta\} = [A]\{l\} + [B]\{m\}$$

where the influence coefficients are defined as the elements of the square matrices $[A]$ and $[B]$.

The elements A_{ij} and B_{ij} represent the twist at the i th spanwise station due to a load or moment at the j th station.

The spanwise load distribution and the spanwise pitching-moment distribution are elements of the column matrices $\{l\}$ and $\{m\}$, respectively, where the elements l_j and m_j are the integrated loads and moments respectively over the j th spanwise segment; that is,

$$l_j = q \bar{c} \frac{b}{2} \int_{(j-1)/n}^{j/n} c_n \frac{c}{\bar{c}} d\left(\frac{2y}{b}\right)$$

and

$$m_j = q c' \bar{c} \frac{b}{2} \int_{(j-1)/n}^{j/n} c_m \frac{c^2}{c' \bar{c}} d\left(\frac{2y}{b}\right)$$

where

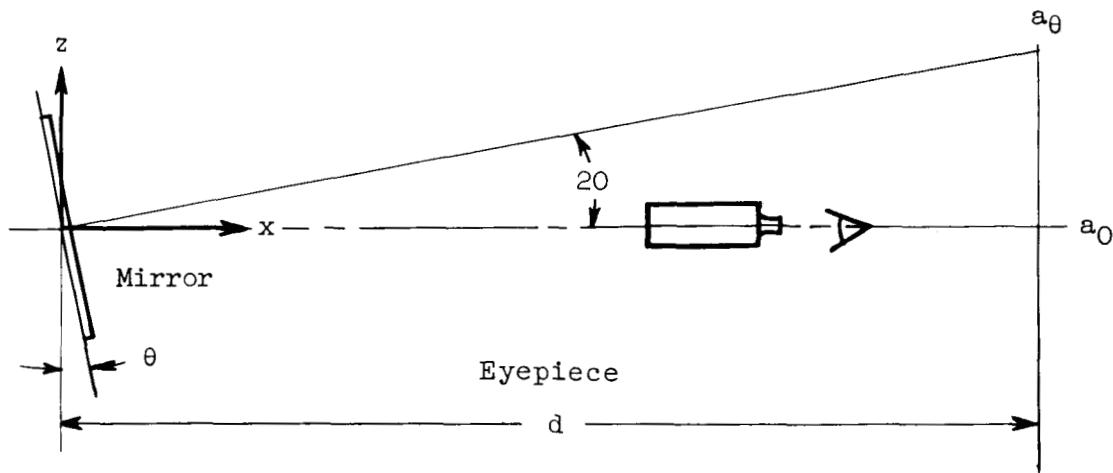
n number of spanwise stations

c' mean aerodynamic chord

\bar{c} average chord

c local chord

The setup for measuring twist with mirrors is shown in figure 11. The technique employed for obtaining the influence coefficients involved principally the use of mirrors, linear scales, and a transit. Loads were applied at the desired points along the wing. A diagram illustrating the twist measurements is shown below:



where

a_0 zero twist reading

a_θ reading due to twist θ

A change in the angle θ of the mirror required a change in the scale reading as sighted through the eyepiece. Small translations of the mirror up or down have little effect on the scale reading. Thus, only twist about the y-axis (perpendicular to the plane of the paper) is observed.

Loading at the jth spanwise station of the $0.25c$ yields the influence coefficients due to normal force of the ith spanwise station. Thus

$$A_{ij} = \frac{\theta_i}{(\text{Load})_j} \frac{\text{deg}}{\text{lb}}$$

where

$$\theta_i = \frac{1}{2} \tan^{-1} \frac{(a_{\theta j} - a_{0j})}{d}$$

Loading at the j th spanwise station of the $0.65c$ yields the influence coefficients due to a moment about the y -axis through the $0.25c$ of the i th station; thus,

$$B_{ij} = \frac{\theta_{i0.65c} - A_{ij}}{(0.65c - 0.25c)_j} \frac{\text{deg}}{\text{in-lb}}$$

where

$$\theta_{i0.65c} = \frac{1}{2} \tan^{-1} \frac{(a_{\theta j} - a_{0j})_{0.65c}}{d}$$

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TABLE I - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER

		Pressure coefficient at:												
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent c		$M = 0.80 \quad \alpha = -1.94^\circ$						$M = 0.80 \quad \alpha = -0.04^\circ$						
Upper surface		.041	.631	.569	.510	.454	.299	.050	.677	.640	.561	.624	.675	
Lower surface		.290	.233	.257	.267	.298	.288	.161	.001	-.009	-.026	-.070	-.068	
Upper surface		.238	.132	.148	.178	.203	.193	.120	-.049	-.050	-.050	-.088	-.082	
Lower surface		.164	.099	.096	.109	.114	.145	.031	-.049	-.056	-.089	-.109	-.107	
Upper surface		.145	.065	.083	.065	.067	.083	.034	-.049	-.056	-.089	-.109	-.107	
Lower surface		.092	.040	.046	.038	.037	.033	.012	-.055	-.079	-.100	-.109	-.124	
Upper surface		.061	.010	.003	.020	.006	.035	.020	-.075	-.096	-.093	-.117	-.145	
Lower surface		.022	-.017	-.025	-.014	-.020	-.072	.035	-.094	.116	.112	.126	.145	
Upper surface		-.006	-.020	-.041	-.048	-.053	-.109	.071	-.096	.118	.135	.151	.156	
Lower surface		.024	-.042	-.051	-.061	-.068	-.103	.075	-.104	-.124	-.137	-.152	-.136	
Upper surface		-.054	-.061	-.069	-.069	-.085	-.114	.104	-.120	-.136	-.139	-.158	-.141	
Lower surface		-.068	-.065	-.090	-.090	-.093	-.152	.113	-.120	-.139	-.149	-.158	-.175	
Upper surface		-.068	-.073	-.093	-.100	-.114	-.130	.110	-.120	-.145	-.149	-.166	-.145	
Lower surface		-.054	-.084	-.099	-.108	-.119	-.134	.092	-.120	-.144	-.149	-.161	-.141	
Upper surface		-.063	-.091	-.103	-.108	-.125	-.126	.088	-.124	-.143	-.146	-.158	-.127	
Lower surface		-.087	-.092	-.097	-.103	-.114	-.100	.112	-.124	-.131	-.136	-.138	-.094	
Upper surface		-.079	-.083	-.086	-.089	-.094	-.112	.095	-.103	-.114	-.109	-.110	-.106	
Lower surface		-.072	-.074	-.072	-.075	-.082	-.067	.087	-.092	-.089	-.092	-.058		
Upper surface		-.056	-.058	-.058	-.055	-.058	-.055	.079	-.072	-.064	-.065	-.043		
Lower surface		-.056	-.040	-.034	-.034	-.034	-.034	.063	-.059	-.049	-.038	-.036		
Upper surface		-.051	-.028	-.017	-.011	-.007	-.015	.056	-.033	-.024	-.011	-.005		
Lower surface		-.021	-.016	-.007	-.017	-.021	-.003	.015	-.013	-.001	-.011	-.030		
Upper surface		.014	.032	.043	.021	.008	.023	.009	.033	.049	.037	.019		
Lower surface														
Upper surface		-.032	-.038	-.048	-.069	-.092	-.760	.135	.008	-.038	-.072	-.081	-.108	
Lower surface		-.077	-.262	-.331	-.436	-.547	-.646	.076	-.044	-.063	-.079	-.085	-.103	
Upper surface		-.094	-.188	-.238	-.317	-.403	-.545	.044	-.027	-.061	-.073	-.081	-.104	
Lower surface		-.107	-.184	-.229	-.287	-.346	-.441	.019	-.049	-.078	-.091	-.093	-.116	
Upper surface		-.137	-.178	-.216	-.280	-.319	-.376	.016	-.060	-.092	-.108	-.106	-.126	
Lower surface		-.137	-.172	-.201	-.250	-.290	-.294	.032	-.071	-.094	-.113	-.124	-.143	
Upper surface		-.159	-.151	-.201	-.253	-.272	-.249	.063	-.068	-.112	-.141	-.134	-.156	
Lower surface		-.164	-.161	-.187	-.232	-.252	-.216	.072	-.071	-.112	-.136	-.134	-.145	
Upper surface		-.174	-.171	-.190	-.228	-.243	-.206	.057	-.093	-.121	-.137	-.139	-.145	
Lower surface		-.169	-.176	-.196	-.223	-.225	-.191	.097	-.113	-.141	-.155	-.147	-.141	
Upper surface		-.149	-.185	-.195	-.221	-.223	-.225	.084	-.122	-.146	-.162	-.156	-.147	
Lower surface		-.178	-.186	-.193	-.213	-.207	-.177	.121	-.132	-.141	-.162	-.147	-.141	
Upper surface		-.172	-.178	-.191	-.184	-.194	-.152	.117	-.129	-.143	-.154	-.119		
Lower surface		-.162	-.168	-.175	-.167	-.170	-.132	.102	-.122	-.129	-.135	-.136		
Upper surface		-.155	-.150	-.163	-.161	-.160	-.142	.102	-.120	-.144	-.145	-.122		
Lower surface		-.144	-.148	-.158	-.158	-.158	-.138	.083	-.093	-.096	-.098	-.084		
Upper surface		-.137	-.116	-.116	-.100	-.094	-.084	.094	-.089	-.084	-.079	-.070		
Lower surface		-.101	-.090	-.101	-.066	-.069	-.063	.073	-.067	-.061	-.051	-.044		
Upper surface		-.078	-.061	-.073	-.031	-.041	-.021	.025	-.019	-.006	-.009	-.011		
Lower surface		-.009	-.044	-.034	-.038	-.003	-.021	.012	-.004	-.034	-.026	-.037		
Upper surface														
Lower surface														
Upper surface		$M = 0.80 \quad \alpha = 1.94^\circ$						$M = 0.80 \quad \alpha = 3.90^\circ$						
Lower surface														
Upper surface		.025	.561	.447	.449	.419	.606	.030	.341	.191	.124	.067	.505	
Lower surface		-.027	-.339	-.484	-.667	-.797	-.557	-.236	-.1001	-.909	-.1014	-.1008	-.671	
Upper surface		-.061	-.304	-.357	-.459	-.576	-.660	-.256	.736	.815	.968	.981	.733	
Lower surface		-.168	-.249	-.285	-.352	-.423	-.543	-.367	-.578	-.715	-.902	-.932	-.718	
Upper surface		-.160	-.207	-.254	-.312	-.377	-.435	-.335	-.379	-.588	-.844	-.881	-.704	
Lower surface		-.158	-.196	-.247	-.300	-.329	-.385	-.296	-.344	-.504	-.768	-.826	-.688	
Upper surface		-.148	-.201	-.240	-.265	-.301	-.314	-.255	-.319	-.401	-.603	-.722	-.656	
Lower surface		-.143	-.211	-.245	-.254	-.285	-.268	-.226	-.307	-.367	-.466	-.607	-.619	
Upper surface		-.185	-.196	-.227	-.300	-.329	-.385	-.255	-.319	-.394	-.507	-.547	-.474	
Lower surface		-.182	-.195	-.215	-.230	-.266	-.295	-.211	-.242	-.265	-.368	-.426	-.372	
Upper surface		-.157	-.157	-.210	-.211	-.215	-.178	-.190	-.231	-.248	-.345	-.377	-.280	
Lower surface		-.182	-.188	-.194	-.187	-.187	-.147	-.214	-.215	-.218	-.221	-.204	-.243	
Upper surface		-.158	-.160	-.168	-.155	-.154	-.149	-.186	-.181	-.196	-.181	-.211		
Lower surface		-.145	-.143	-.141	-.133	-.131	-.106	-.164	-.159	-.158	-.151	-.144	-.179	
Upper surface		-.129	-.122	-.117	-.102	-.101	-.091	-.144	-.137	-.133	-.121	-.113	-.159	
Lower surface		-.107	-.093	-.086	-.078	-.070	-.066	-.116	-.105	-.096	-.083	-.077	-.137	
Upper surface		-.095	-.068	-.054	-.042	-.035	-.040	-.100	-.072	-.070	-.058	-.043	-.115	
Lower surface		-.054	-.043	-.025	-.015	-.001	-.023	-.054	-.041	-.038	-.026	-.006	-.094	
Upper surface		-.013	-.018	.010	.023	.013	.018	-.010	-.013	.003	.014	.002	-.079	
Lower surface														
Upper surface		-.257	.228	.230	.268	.321	.246	.403	.416	.416	.457	.511	.404	
Lower surface		.190	.130	.152	.181	.210	.180	.339	.301	.328	.358	.392	.331	
Upper surface		.147	.096	.094	.114	.132	.118	.282	.231	.234	.249	.282	.260	
Lower surface		.108	.052	.046	.065	.090	.063	.230	.174	.181	.191	.225	.188	
Upper surface		.070	.025	.017	.033	.048	.023	.183	.141	.144	.145	.174	.133	
Lower surface		-.001	-.008	-.029	-.041	-.029	-.048	-.142	-.111	-.104	-.099	-.114	-.045	
Upper surface		-.017	-.017	-.042	-.061	-.055	-.053	.072	.059	.031	.036	.038	.016	
Lower surface		-.006	-.005	-.003	-.011	-.011	-.017	.058	.029	.021	.001	.013	-.089	
Upper surface		-.045	-.064	-.077	-.098	-.097	-.101	.016	.003	-.010	-.027	-.016	-.103	
Lower surface		-.066	-.078	-.091	-.106	-.101	-.138	.002	-.014	-.027	-.042	-.028	-.112	
Upper surface		-.057	-.093	-.102	-.123	-.115	-.150	.004	-.033	-.040	-.068	-.050	-.122	
Lower surface		-.100	-.112	-.112	-.118	-.135	-.128	-.054	-.049	-.060	-.079	-.064	-.125	
Upper surface		-.103	-.111	-.11										

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:											
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent c	M = 0.80	a = 5.01°						M = 0.80 a = 7.95°					
		M = 0.80	a = 5.01°					M = 0.80	a = 7.95°				
Upper surface	0.00	.039	.107	-.054	-.360	-.197	.396	.029	-.132	-.343	-.465	-.449	.247
	1.25	-.465	-1.373	-1.130	-1.014	-812	-.518	-.671	-.676	-.148	-.226	-.700	.475
	2.50	-.504	-1.276	-1.108	-1.014	-.805	-.546	-.734	-.574	-1.318	-.923	-.697	.484
	5.00	-.643	-1.057	-1.089	-1.017	-.794	-.446	-.804	-.524	-1.327	-.913	-.689	.479
	7.50	-.510	-1.811	-1.047	-1.003	-.785	-.446	-.800	-.521	-1.281	-.903	-.682	.479
	10.00	-.481	-1.502	-1.007	-0.995	-.777	-.549	-.722	-.402	-1.312	-.890	-.677	.482
	12.50	-.371	-1.393	-.853	-.962	-.760	-.551	-.513	-.522	-1.213	-.869	-.668	.486
	20.00	-.330	-1.393	-.642	-.888	-.742	-.549	-.442	-.475	-1.087	-.847	-.657	.486
	25.00	-.371	-1.360	-.558	-.818	-.716	-.542	-.485	-.429	-.889	-.827	-.642	.485
	30.00	-.339	-1.353	-.352	-.705	-.688	-.530	-.423	-.407	-.588	-.795	-.624	.485
Lower surface	35.00	-.351	-1.345	-.316	-.606	-.660	-.515	-.412	-.385	-.367	-.766	-.604	.481
	40.00	-.322	-1.315	-.299	-.486	-.620	-.499	-.372	-.352	-.283	-.733	-.583	.475
	45.00	-.310	-1.296	-.285	-.400	-.592	-.476	-.353	-.337	-.280	-.703	-.568	.471
	50.00	-.268	-1.280	-.268	-.332	-.542	-.458	-.317	-.318	-.200	-.664	-.545	.463
	55.00	-.223	-1.262	-.256	-.279	-.502	-.440	-.267	-.303	-.276	-.617	-.529	.454
	60.00	-.241	-1.240	-.233	-.247	-.462	-.415	-.283	-.283	-.257	-.580	-.511	.444
	65.00	-.205	-1.207	-.195	-.204	-.413	-.388	-.242	-.243	-.233	-.518	-.489	.437
	70.00	-.182	-1.179	-.168	-.166	-.369	-.364	-.226	-.220	-.206	-.460	-.468	.429
	75.00	-.159	-1.150	-.143	-.139	-.324	-.349	-.197	-.191	-.189	-.417	-.451	.423
	80.00	-.127	-1.119	-.096	-.089	-.281	-.328	-.160	-.157	-.150	-.374	-.432	.418
Upper surface	85.00	-.107	-1.084	-.077	-.067	-.237	-.307	-.139	-.121	-.120	-.325	-.408	.418
	90.00	-.059	-1.051	-.037	-.034	-.185	-.295	-.090	-.086	-.082	-.283	-.380	.417
	95.00	-.011	-1.018	-.006	-.005	-.156	-.281	-.037	-.045	-.031	-.225	-.369	.413
Lower surface	1.25	.531	.547	.536	.570	.592	.464	.637	.638	.615	.621	.629	.500
	5.00	.472	.430	.448	.475	.494	.394	.593	.529	.534	.540	.550	.437
	7.50	.348	.345	.350	.384	.384	.326	.515	.436	.436	.437	.449	.374
	10.00	.292	.247	.249	.256	.264	.243	.444	.367	.373	.375	.387	.299
	15.00	.235	.193	.189	.196	.205	.110	.318	.267	.260	.268	.263	.151
	20.00	.182	.174	.147	.143	.153	.040	.251	.237	.211	.198	.207	.076
	25.00	.149	.129	.114	.105	.109	-.010	.212	.189	.173	.161	.157	.029
	30.00	.125	.092	.088	.079	.079	-.049	.184	.149	.135	.131	.123	.015
	35.00	.070	.064	.059	.048	.040	-.052	.112	.116	.107	.090	.094	.027
	40.00	.064	.043	.044	.027	.022	-.086	.112	.091	.077	.063	.056	.1074
Upper surface	45.00	.057	.021	.016	.001	-.002	-.117	.103	.065	.052	.035	.026	.114
	50.00	.006	-.002	-.016	-.026	-.024	-.126	.043	.039	.030	.009	-.003	-.130
	55.00	-.010	-.016	-.011	-.023	-.030	-.124	.022	.020	.015	-.003	-.037	-.133
	60.00	-.010	-.025	-.026	-.039	-.059	-.124	.022	.004	-.002	-.020	-.056	-.141
	65.00	-.020	-.029	-.026	-.049	-.072	-.133	.005	-.006	-.011	-.038	-.075	-.154
	70.00	-.015	-.025	-.024	-.041	-.058	-.121	.001	-.011	-.017	-.039	-.075	-.153
	75.00	-.049	-.031	-.028	-.040	-.065	-.124	-.027	-.021	-.025	-.049	-.086	-.161
	80.00	-.036	-.027	-.018	-.031	-.056	-.121	-.028	-.014	-.017	-.049	-.121	.149
	85.00	-.028	-.017	-.009	-.015	-.039	-.111	-.023	-.015	-.014	-.053	-.121	.149
	90.00	-.015	-.006	-.007	-.015	-.034	-.134	-.020	-.012	-.012	-.060	-.137	.206
Lower surface	95.00	-.010	-.005	-.028	-.009	-.062	-.145	.000	-.009	-.009	-.085	-.187	.226
	1.25	M = 0.80	a = 9.89°					M = 0.80	a = 11.84°				
	5.00	.036	-.351	-.605	-.666	-.599	.087	.047	-.575	-.835	-.922	-.763	.094
	1.25	-.821	-1.733	-1.270	-.783	-.626	-.452	-.957	-.1640	-.1026	-.726	-.600	.440
	2.50	-.905	-1.714	-1.252	-.777	-.625	-.453	-.1050	-.1612	-.1019	-.718	-.595	.438
	5.00	-.1043	-.1598	-1.241	-.771	-.617	-.453	-.182	-.1531	-.1013	-.716	-.586	.438
	7.50	-.950	-1.481	-1.208	-.765	-.612	-.453	-.1100	-.1449	-.983	-.718	-.579	.438
	10.00	-.902	-1.341	-1.207	-.756	-.612	-.450	-.1000	-.1366	-.972	-.715	-.579	.438
	15.00	-.666	-.992	-1.160	-.742	-.608	-.455	-.673	-.1226	-.945	-.712	-.576	.440
	20.00	-.508	-.416	-.1090	-.727	-.604	-.455	-.552	-.939	-.930	-.699	-.571	.440
Upper surface	25.00	-.483	-.392	-.1023	-.705	-.599	-.457	-.539	-.662	-.926	-.689	-.566	.440
	30.00	-.511	-.409	-.1920	-.689	-.593	-.460	-.565	-.516	-.671	-.563	-.441	
	35.00	-.430	-.409	-.1814	-.667	-.584	-.462	-.489	-.475	-.682	-.634	-.444	
	40.00	-.400	-.378	-.1696	-.656	-.574	-.463	-.450	-.435	-.682	-.643	-.447	
	45.00	-.384	-.367	-.1591	-.642	-.567	-.463	-.435	-.420	-.672	-.626	-.450	
	50.00	-.361	-.357	-.1513	-.626	-.555	-.463	-.420	-.405	-.656	-.616	-.452	
	55.00	-.311	-.349	-.1445	-.614	-.544	-.463	-.397	-.380	-.607	-.583	-.457	
	60.00	-.326	-.356	-.1398	-.588	-.536	-.463	-.361	-.344	-.554	-.574	-.461	
	65.00	-.297	-.348	-.1363	-.570	-.522	-.463	-.324	-.326	-.515	-.555	-.521	
	70.00	-.276	-.275	-.1316	-.547	-.507	-.465	-.300	-.304	-.472	-.534	-.517	
Lower surface	75.00	-.248	-.248	-.1280	-.518	-.495	-.466	-.262	-.273	-.438	-.520	-.499	
	80.00	-.207	-.215	-.1251	-.493	-.484	-.468	-.226	-.235	-.427	-.507	-.497	
	85.00	-.179	-.174	-.1212	-.472	-.470	-.473	-.177	-.177	-.419	-.491	-.488	
	90.00	-.126	-.131	-.1167	-.437	-.449	-.475	-.177	-.194	-.348	-.491	-.483	
	95.00	-.086	-.117	-.119	-.441	-.477	-.477	-.104	-.141	-.293	-.479	-.481	
Upper surface	1.25	.733	.709	.667	.657	.645	.531	.805	.761	.708	.689	.660	.556
	5.00	.703	.615	.607	.600	.588	.477	.801	.687	.658	.644	.625	.509
	7.50	.625	.520	.513	.503	.491	.418	.720	.598	.579	.554	.553	.460
	10.00	.545	.449	.442	.445	.440	.347	.631	.527	.517	.499	.494	.399
	15.00	.476	.415	.397	.395	.385	.291	.558	.484	.471	.452	.441	.349
	20.00	.397	.340	.332	.331	.317	.203	.471	.411	.400	.386	.375	.255
	25.00	.325	.305	.272	.259	.260	.130	.398	.375	.343	.316	.313	.182
	28.00	.285	.252	.232	.217	.209	.075	.351	.318	.295	.276	.265	.123
	30.00	.250	.210	.197	.185	.169	.022	.311	.271	.250	.222	.224	.073
	35.00	.172	.174	.162	.159	.123	-.002	.231	.230	.214	.199	.177	.047
Lower surface	40.00	-.171	-.195	-.195	-.205	-.205	-.045	-.224	-.192	-.187	-.153	-.149	-.006
	45.00	-.056	-.113	-.103	-.073	-.064	-.090	-.209	-.164	-.149	-.125	-.114	-.053
	50.00	-.097	-.064	-.059	-.049	-.029	-.125	-.146	-.132	-.119	-.087	-.077	-.081
	55.00	-.066	-.058	-.049	-.042	-.030	-.123	-.112	-.104	-.091	-.068	-.034	-.094
	60.00	-.020	-.020	-.019	-.019	-.009	-.123	-.112	-.081	-.068	-.039	-.002	-.114
	65.00	-.041	-.022	-.013	-.021	-.062	-.156	-.080	-.057	-.049	-.015	-.028	-.135
	70.00	-.029	-.015	-.001	-.033	-.065	-.159	-.059	-.048	-.025	-.005	-.026	-.161
	75.00</td												

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:												
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent	C	M = 0.80	a = 13.95°					M = 0.80	a = 17.24°					
Upper surface	0.00	.022	-.849	-1.079	-1.081	-.665	-.333	.002	-1.047	-1.017	-.753	-.646	-.573	
	1.25	-.106	-1.338	-1.009	-.724	-.622	-.493	-.849	-.879	-.795	-.723	-.623	-.541	
	2.50	-.1265	-1.380	-1.035	-.703	-.621	-.491	-.826	-.884	-.785	-.713	-.627	-.561	
	5.00	-.1293	-1.383	-1.033	-.697	-.617	-.491	-.840	-.885	-.795	-.692	-.624	-.540	
	7.50	-.1250	-1.248	-1.044	-.698	-.611	-.491	-.856	-.896	-.799	-.690	-.617	-.541	
	10.00	-.1258	-1.248	-1.057	-.698	-.611	-.491	-.867	-.896	-.809	-.690	-.617	-.541	
	15.00	-.847	-1.187	-.920	-.696	-.604	-.492	-.853	-.878	-.801	-.686	-.617	-.544	
	20.00	-.740	-1.089	-.896	-.695	-.600	-.492	-.814	-.864	-.785	-.684	-.610	-.547	
	25.00	-.674	-.979	-.873	-.689	-.598	-.492	-.772	-.855	-.773	-.680	-.608	-.549	
	30.00	-.677	-.863	-.855	-.680	-.595	-.494	-.735	-.823	-.761	-.674	-.608	-.552	
Lower surface	35.00	-.576	-.776	-.836	-.673	-.593	-.495	-.675	-.808	-.756	-.674	-.606	-.557	
	40.00	-.533	-.675	-.810	-.666	-.593	-.498	-.635	-.773	-.750	-.674	-.606	-.554	
	45.00	-.511	-.611	-.789	-.661	-.591	-.500	-.598	-.748	-.743	-.670	-.607	-.559	
	50.00	-.504	-.560	-.749	-.650	-.590	-.504	-.581	-.715	-.739	-.670	-.608	-.560	
	55.00	-.444	-.525	-.725	-.645	-.588	-.507	-.572	-.688	-.729	-.666	-.608	-.562	
	60.00	-.465	-.507	-.691	-.630	-.588	-.509	-.560	-.673	-.719	-.658	-.612	-.566	
	65.00	-.444	-.477	-.662	-.625	-.585	-.513	-.542	-.651	-.709	-.657	-.612	-.572	
	70.00	-.438	-.460	-.636	-.613	-.581	-.516	-.550	-.636	-.698	-.656	-.611	-.575	
	75.00	-.409	-.447	-.614	-.601	-.579	-.523	-.523	-.622	-.686	-.645	-.615	-.574	
	80.00	-.380	-.417	-.588	-.589	-.574	-.527	-.508	-.601	-.673	-.639	-.615	-.580	
Upper surface	85.00	-.362	-.387	-.555	-.582	-.566	-.533	-.502	-.569	-.659	-.636	-.610	-.586	
	90.00	-.307	-.356	-.527	-.568	-.557	-.537	-.481	-.545	-.639	-.628	-.602	-.588	
	95.00	-.217	-.293	-.490	-.561	-.557	-.541	-.414	-.505	-.621	-.623	-.606	-.590	
Lower surface	1.25	.846	.790	.722	.676	.642	.550	.906	.826	.738	.675	.626	.541	
	2.50	.871	.731	.690	.663	.634	.514	.965	.800	.736	.690	.656	.528	
	5.00	.780	.647	.615	.586	.573	.474	.872	.731	.677	.646	.620	.506	
	7.50	.855	.575	.544	.526	.522	.416	.776	.666	.621	.599	.578	.459	
	10.00	.607	.528	.508	.485	.466	.359	.699	.616	.580	.556	.538	.413	
	15.00	.514	.457	.435	.414	.400	.273	.604	.532	.513	.486	.461	.326	
	20.00	.440	.415	.372	.345	.340	.195	.524	.492	.451	.419	.405	.252	
	25.00	.385	.354	.328	.295	.289	.137	.469	.437	.401	.373	.356	.186	
	30.00	.340	.305	.280	.258	.247	.082	.423	.384	.354	.329	.308	.123	
	35.00	.254	.239	.215	.197	.049		.334	.337	.309	.282	.257	.092	
Upper surface	40.00	.247	.225	.203	.176	.166	-.005	.319	.298	.269	.241	.225	.034	
	45.00	.228	.188	.170	.132	.123	-.058	.297	.256	.230	.198	.183	-.023	
	50.00	.163	.149	.131	.097	.085	-.089	.228	.215	.188	.160	.141	-.055	
	55.00	.123	.118	.104	.077	.043	-.100	.181	.172	.159	.130	.092	-.079	
	60.00	.120	.089	.069	.038	.006	-.125	.173	.147	.120	.095	.051	-.103	
	65.00	.077	.061	.047	.005	.026	-.152	.122	.108	.092	.055	.012	-.129	
	70.00	.047	.042	.025	-.012	-.042	-.161	.081	.084	.057	.030	-.003	-.147	
	75.00	.025	.012	-.009	-.042	-.074	-.182	.050	.041	.022	-.005	-.042	-.170	
	80.00	-.006	-.007	-.031	-.065	-.097	-.197	.019	.00	-.009	-.037	-.073	-.196	
	85.00	-.038	-.038	-.053	-.095	-.137	-.188	.013	-.024	-.041	-.112	-.119	-.194	
Lower surface	90.00	-.068	-.067	-.100	-.142	-.176	-.256	-.057	-.068	-.100	-.122	-.162	-.237	
	95.00	-.099	-.111	-.144	-.226	-.246	-.280	-.163	-.151	-.171	-.217	-.240	-.286	
Upper surface	0.00	M = 0.80	a = 19.29°					M = 0.80	a = 21.30°					
	1.25	-.017	-.711	-.719	-.697	-.627	-.601	-.059	-.779	-.771	-.744	-.697	-.660	
	2.50	-.698	-.687	-.700	-.691	-.618	-.574	-.786	-.768	-.762	-.738	-.691	-.635	
	5.00	-.691	-.693	-.694	-.673	-.621	-.572	-.771	-.769	-.758	-.734	-.692	-.634	
	7.50	-.657	-.699	-.701	-.670	-.621	-.571	-.742	-.775	-.762	-.729	-.690	-.633	
	10.00	-.658	-.702	-.719	-.666	-.616	-.574	-.753	-.780	-.756	-.727	-.686	-.635	
	15.00	-.667	-.707	-.702	-.665	-.620	-.577	-.758	-.780	-.762	-.727	-.688	-.636	
	20.00	-.683	-.713	-.705	-.663	-.618	-.580	-.768	-.785	-.765	-.726	-.687	-.637	
	25.00	-.695	-.713	-.704	-.662	-.613	-.581	-.772	-.787	-.766	-.724	-.688	-.638	
	30.00	-.699	-.717	-.710	-.657	-.614	-.583	-.772	-.788	-.769	-.723	-.684	-.639	
Upper surface	35.00	-.697	-.717	-.709	-.657	-.613	-.585	-.767	-.789	-.767	-.720	-.683	-.640	
	40.00	-.681	-.717	-.707	-.657	-.614	-.589	-.742	-.785	-.769	-.720	-.684	-.642	
	45.00	-.669	-.717	-.707	-.660	-.618	-.589	-.723	-.780	-.766	-.723	-.684	-.643	
	50.00	-.648	-.714	-.704	-.659	-.618	-.591	-.693	-.778	-.766	-.722	-.686	-.645	
	55.00	-.648	-.706	-.704	-.661	-.622	-.596	-.701	-.766	-.766	-.723	-.688	-.649	
	60.00	-.633	-.700	-.700	-.661	-.623	-.598	-.687	-.760	-.763	-.723	-.688	-.651	
	65.00	-.623	-.698	-.698	-.655	-.628	-.602	-.686	-.746	-.754	-.715	-.690	-.644	
	70.00	-.615	-.686	-.682	-.657	-.627	-.607	-.681	-.746	-.751	-.717	-.689	-.657	
	75.00	-.623	-.682	-.682	-.662	-.632	-.611	-.686	-.740	-.751	-.717	-.689	-.657	
	80.00	-.599	-.676	-.688	-.654	-.634	-.614	-.659	-.727	-.742	-.711	-.692	-.658	
Lower surface	85.00	-.597	-.670	-.680	-.652	-.635	-.617	-.647	-.715	-.734	-.705	-.691	-.660	
	90.00	-.588	-.637	-.666	-.647	-.624	-.626	-.616	-.672	-.715	-.700	-.677	-.661	
	95.00	-.531	-.610	-.650	-.641	-.629	-.629	-.534	-.627	-.706	-.693	-.686	-.660	
Upper surface	1.25	.920	.842	.741	.666	.603	.525	.899	.848	.736	.646	.566	.502	
	2.50	.999	.834	.758	.696	.656	.525	1.005	.858	.768	.702	.651	.514	
	5.00	.922	.771	.715	.668	.636	.513	.944	.813	.743	.691	.655	.517	
	7.50	.823	.710	.666	.626	.603	.476	.858	.757	.704	.658	.600	.489	
	10.00	.754	.665	.623	.590	.562	.432	.796	.711	.666	.628	.593	.452	
	15.00	.657	.593	.557	.525	.494	.353	.695	.641	.603	.568	.530	.380	
	20.00	.580	.525	.501	.460	.444	.281	.615	.573	.544	.507	.480	.312	
	25.00	.523	.487	.446	.411	.395	.218	.564	.530	.490	.461	.433	.247	
	30.00	.477	.432	.402	.372	.348	.155	.514	.476	.443	.415	.386	.184	
	35.00	.387	.385	.353	.323	.297	.120	.443	.448	.401	.368	.336	.145	
Lower surface	40.00	.375	.340	.314	.281	.264	.069	.412	.392	.357	.324	.301	.091	
	45.00	.343	.306	.273	.236	.221	.011	.385	.342	.318	.282	.259	.026	
	50.00	.275	.263	.232	.197	.176	-.030	.310	.300	.274	.240	.216	-.006	
	55.00	.229	.221	.200	.169	.128	-.036	.266	.243	.240	.209	.184	-.036	
	60.00	.214	.185	.154	.130	.084	-.003	.246	.219	.198	.164	.117	-.063	
	65.00	.141	.141	.128	.086	.046	-.112	.193	.180	.141	.123	.081	-.096	
	70.00	.115	.116	.092	.058	.027	-.137	.117	.148	.124	.094	.077	-.155	
	75.00	.085	.071	.052	.019	-.017	-.160	.106	.097	.082	.052	.012	-.183	
	80.00	.042	.036	.016	-.015	-.053	-.191	.066	.063	.042	.011	-.027	-.183	
	85.00	.001	-.003											

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:												
Percent c	M = 0.80 $\alpha = 23.46^\circ$						M = 0.80 $\alpha = 25.45^\circ$					
	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Upper surface												
0.00	-0.134	-0.955	-0.946	-0.956	-0.875	-0.823	-0.191	-1.032	-1.028	-1.029	-0.964	-0.865
1.25	-0.957	-0.951	-0.942	-0.923	-0.865	-0.778	-1.049	-1.032	-1.029	-1.017	-0.950	-0.812
2.50	-0.949	-0.953	-0.936	-0.913	-0.865	-0.776	-1.032	-1.023	-1.022	-1.014	-0.944	-0.809
5.00	-0.932	-0.952	-0.941	-0.909	-0.863	-0.773	-1.026	-1.035	-1.029	-1.005	-0.947	-0.808
7.50	-0.942	-0.955	-0.935	-0.907	-0.856	-0.774	-1.026	-1.035	-1.022	-1.005	-0.940	-0.808
10.00	-0.944	-0.955	-0.941	-0.908	-0.856	-0.773	-1.030	-1.039	-1.030	-1.004	-0.939	-0.807
15.00	-0.944	-0.948	-0.944	-0.905	-0.854	-0.773	-1.030	-1.043	-1.032	-1.001	-0.936	-0.807
20.00	-0.940	-0.958	-0.944	-0.902	-0.854	-0.772	-1.022	-1.041	-1.031	-0.987	-0.934	-0.804
25.00	-0.928	-0.959	-0.944	-0.900	-0.852	-0.772	-0.986	-1.039	-1.031	-0.984	-0.930	-0.801
30.00	-0.909	-0.953	-0.944	-0.898	-0.849	-0.773	-0.932	-1.032	-1.030	-0.983	-0.927	-0.803
35.00	-0.841	-0.948	-0.942	-0.898	-0.848	-0.777	-0.865	-1.021	-1.030	-0.981	-0.925	-0.805
40.00	-0.801	-0.931	-0.943	-0.899	-0.847	-0.778	-0.830	-1.028	-0.981	-0.920	-0.807	
45.00	-0.775	-0.919	-0.941	-0.895	-0.847	-0.779	-0.800	-0.954	-1.025	-0.977	-0.919	-0.807
50.00	-0.753	-0.887	-0.940	-0.895	-0.846	-0.780	-0.732	-0.888	-1.019	-0.975	-0.916	-0.807
55.00	-0.724	-0.860	-0.934	-0.892	-0.845	-0.781	-0.687	-0.814	-1.007	-0.971	-0.912	-0.806
60.00	-0.717	-0.831	-0.927	-0.881	-0.845	-0.780	-0.637	-0.736	-0.981	-0.958	-0.909	-0.803
65.00	-0.680	-0.780	-0.918	-0.881	-0.843	-0.781	-0.573	-0.645	-0.959	-0.956	-0.905	-0.801
70.00	-0.640	-0.740	-0.903	-0.881	-0.836	-0.778	-0.548	-0.586	-0.935	-0.952	-0.900	-0.796
75.00	-0.596	-0.692	-0.886	-0.869	-0.837	-0.778	-0.511	-0.518	-0.886	-0.941	-0.898	-0.792
80.00	-0.555	-0.632	-0.862	-0.866	-0.836	-0.774	-0.467	-0.459	-0.835	-0.933	-0.895	-0.786
85.00	-0.525	-0.563	-0.830	-0.862	-0.827	-0.774	-0.462	-0.400	-0.774	-0.918	-0.885	-0.783
90.00	-0.448	-0.506	-0.781	-0.858	-0.820	-0.771	-0.415	-0.384	-0.678	-0.896	-0.871	-0.781
95.00	-0.340	-0.405	-0.712	-0.854	-0.834	-0.766	-0.363	-0.351	-0.566	-0.871	-0.883	-0.775
Lower surface												
1.25	.852	.837	.715	.609	.511	.471	.813	.833	.702	.581	.476	.452
2.50	.997	.873	.772	.685	.639	.497	.987	.894	.778	.677	.626	.489
5.00	.970	.849	.768	.704	.666	.519	.983	.879	.795	.726	.679	.526
7.50	.898	.799	.740	.684	.619	.503	.926	.839	.772	.711	.677	.522
10.00	.834	.761	.705	.657	.629	.572	.867	.803	.746	.691	.659	.498
15.00	.737	.690	.644	.602	.570	.409	.779	.737	.693	.643	.607	.441
20.00	.669	.637	.588	.545	.521	.342	.716	.682	.641	.592	.567	.382
25.00	.612	.577	.541	.501	.477	.282	.662	.630	.592	.548	.524	.323
30.00	.569	.527	.491	.461	.432	.215	.611	.583	.546	.505	.477	.263
35.00	.483	.479	.447	.410	.381	.179	.538	.536	.496	.459	.432	.224
40.00	.461	.437	.409	.367	.347	.119	.519	.493	.463	.418	.399	.164
45.00	.434	.395	.365	.326	.305	.055	.482	.448	.419	.379	.357	.101
50.00	.363	.349	.324	.283	.261	.021	.417	.402	.381	.335	.315	.066
55.00	.318	.308	.289	.250	.206	-.012	.372	.365	.343	.303	.263	.032
60.00	.301	.269	.245	.206	.161	-.044	.352	.320	.298	.260	.215	-.001
65.00	.239	.225	.209	.165	.118	-.076	.300	.283	.262	.214	.170	-.032
70.00	.186	.196	.171	.132	.096	-.107	.239	.252	.225	.181	.147	-.060
75.00	.145	.145	.127	.090	.067	-.137	.206	.187	.153	.139	.106	-.100
80.00	.116	.114	.088	.049	.004	-.172	.157	.162	.140	.093	.051	-.134
85.00	.062	.074	.049	.007	-.047	-.175	.106	.121	.099	.046	-.002	-.141
90.00	.010	.018	-.011	-.059	-.105	-.254	.043	.066	-.037	-.019	-.064	-.225
95.00	-.049	-.047	-.100	-.173	-.200	-.292	-.031	-.000	-.044	-.135	-.164	-.264

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:													
	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent	c	M = 0.90	a = -2.02°				M = 0.90	a = -0.04°					
Upper surface													
0.00	.037	.476	.613	.374	.509	.371	.057	.702	.669	.654	.605	.623	
1.25	.311	.231	.248	.273	.249	.289	.236	.101	.099	.110	.075	.130	
2.50	.249	.139	.146	.167	.183	.171	.172	.047	.032	.029	.035	.019	
5.00	.181	.110	.094	.101	.094	.111	.107	.033	.010	.006	.016	.037	
7.50	.166	.072	.059	.055	.049	.062	.101	.019	.008	.021	.054	.073	
10.00	.101	.049	.027	.033	.017	.014	.043	.003	.034	.047	.056	.106	
15.00	.073	.017	.014	.004	.021	.073	.026	.029	.061	.058	.089	.157	
20.00	.030	-.017	-.039	-.033	-.043	-.151	-.005	-.060	-.086	-.082	-.114	-.204	
25.00	-.001	-.029	-.057	-.067	-.080	-.232	-.037	-.066	-.091	-.121	-.145	-.251	
30.00	.061	-.043	-.073	-.090	-.099	-.223	.110	.083	.104	.124	.154	.221	
35.00	-.056	-.071	-.093	-.107	-.125	-.214	-.089	-.106	-.127	-.140	-.174	-.206	
40.00	-.075	-.082	-.113	-.130	-.145	-.247	-.104	-.119	-.144	-.164	-.186	-.246	
45.00	-.088	-.095	-.135	-.148	-.171	-.205	-.119	-.125	-.162	-.176	-.210	-.212	
50.00	-.073	-.114	-.146	-.164	-.188	-.192	-.101	-.136	-.174	-.190	-.219	-.193	
55.00	-.082	-.131	-.161	-.177	-.200	-.169	-.101	-.156	-.184	-.195	-.230	-.166	
60.00	-.126	-.136	-.151	-.167	-.183	-.133	-.150	-.159	-.171	-.195	-.200	-.116	
65.00	-.115	-.121	-.142	-.145	-.141	-.138	-.129	-.139	-.153	-.146	-.142	-.116	
70.00	-.108	-.112	-.120	-.120	-.116	-.079	-.111	-.117	-.121	-.105	-.102	-.063	
75.00	-.073	-.087	-.098	-.088	-.082	-.062	-.094	-.103	-.088	-.064	-.062	-.041	
80.00	-.076	-.069	-.067	-.079	-.064	-.035	-.068	-.062	-.061	-.018	-.025	-.014	
85.00	-.063	-.039	-.035	-.021	-.005	-.013	-.004	-.026	-.016	-.002	-.011	-.010	
90.00	-.020	-.020	-.008	-.009	-.029	-.005	-.009	-.007	-.014	-.034	-.048	-.028	
95.00	.017	.010	.026	.045	.038	.005	.030	.024	.048	.071	.057	.030	
Lower surface													
0.00	.018	-.297	-.464	-.822	-.987	-.1407	.138	-.062	-.147	-.283	-.433	-.493	
1.25	-.036	-.234	-.308	-.528	-.832	-.999	.068	-.079	-.125	-.216	-.386	-.435	
5.00	-.060	-.168	-.253	-.310	-.424	-.899	.037	-.042	-.094	-.145	-.195	-.392	
7.50	-.078	-.172	-.243	-.313	-.332	-.751	-.009	-.089	-.118	-.168	-.181	-.335	
10.00	-.118	-.174	-.233	-.321	-.347	-.576	-.025	-.082	-.134	-.174	-.184	-.274	
15.00	-.126	-.177	-.226	-.297	-.335	-.415	-.047	-.091	-.128	-.169	-.193	-.261	
20.00	-.152	-.162	-.235	-.297	-.342	-.399	-.083	-.091	-.147	-.200	-.209	-.288	
25.00	-.171	-.173	-.230	-.282	-.324	-.291	-.095	-.094	-.147	-.193	-.215	-.246	
30.00	-.147	-.192	-.238	-.288	-.327	-.252	-.080	-.124	-.156	-.200	-.224	-.236	
35.00	-.171	-.219	-.245	-.307	-.342	-.230	-.103	-.149	-.176	-.221	-.243	-.205	
40.00	-.207	-.212	-.257	-.320	-.345	-.247	-.135	-.153	-.188	-.231	-.247	-.229	
45.00	-.180	-.231	-.280	-.339	-.356	-.247	-.119	-.175	-.210	-.253	-.264	-.232	
50.00	-.234	-.259	-.301	-.349	-.350	-.228	-.175	-.196	-.223	-.265	-.264	-.207	
55.00	-.245	-.268	-.326	-.320	-.320	-.186	-.182	-.207	-.223	-.250	-.264	-.163	
60.00	-.254	-.264	-.284	-.288	-.293	-.145	-.194	-.207	-.211	-.220	-.212	-.127	
65.00	-.220	-.225	-.225	-.220	-.220	-.161	-.128	-.167	-.178	-.180	-.158	-.104	
70.00	-.142	-.146	-.146	-.148	-.148	-.098	-.104	-.145	-.141	-.132	-.117	-.076	
75.00	-.172	-.146	-.125	-.102	-.095	-.079	-.066	-.145	-.122	-.101	-.082	-.045	
80.00	-.115	-.103	-.085	-.059	-.041	-.005	-.094	-.082	-.065	-.042	-.031	-.033	
85.00	-.077	-.060	-.042	-.024	-.016	-.005	-.011	-.019	-.012	-.016	-.032	-.034	-.017
90.00	-.036	-.026	-.011	-.011	-.021	-.016	-.022	-.019	-.012	-.016	-.034	-.036	
95.00	.006	.007	.026	.039	.055	.026	.022	-.019	-.046	-.056	-.067	-.056	
Upper surface		M = 0.90	a = 1.96°				M = 0.90	a = 3.91°					
0.00	.060	.642	.542	.557	.528	.642	.041	.531	.390	.388	.342	.566	
1.25	.071	-.231	-.314	-.644	-.765	-.737	-.065	-.697	-.831	-.986	-.1065	-.970	
2.50	.011	.214	.289	.382	.644	.896	.129	.416	.739	.833	.959	.156	
5.00	-.082	-.174	-.221	-.280	-.345	-.814	-.248	-.332	-.496	-.674	-.777	-.1082	
7.50	-.095	-.140	-.213	-.271	-.341	-.707	-.240	-.265	-.314	-.634	-.749	-.1003	
10.00	-.104	-.137	-.210	-.275	-.311	-.582	-.232	-.248	-.316	-.567	-.657	-.943	
15.00	-.088	-.157	-.209	-.254	-.311	-.398	-.182	-.252	-.329	-.362	-.641	-.862	
20.00	-.091	-.176	-.225	-.254	-.313	-.352	-.175	-.280	-.339	-.362	-.543	-.826	
25.00	-.148	-.170	-.222	-.261	-.308	-.297	-.242	-.259	-.322	-.372	-.424	-.613	
30.00	-.192	-.192	-.228	-.262	-.315	-.246	-.335	-.283	-.334	-.372	-.424	-.483	
35.00	-.190	-.213	-.235	-.273	-.323	-.224	-.283	-.308	-.344	-.382	-.438	-.483	
40.00	-.202	-.210	-.248	-.287	-.326	-.258	-.317	-.312	-.360	-.403	-.446	-.489	
45.00	-.219	-.214	-.257	-.295	-.342	-.225	-.317	-.312	-.360	-.403	-.447	-.526	
50.00	-.197	-.226	-.270	-.302	-.333	-.205	-.294	-.317	-.364	-.419	-.472	-.527	
55.00	-.248	-.283	-.319	-.342	-.374	-.174	-.265	-.338	-.383	-.418	-.451	-.508	
60.00	-.234	-.248	-.282	-.329	-.321	-.125	-.236	-.352	-.382	-.400	-.423	-.511	
65.00	-.199	-.204	-.209	-.220	-.210	-.131	-.299	-.308	-.326	-.326	-.360	-.426	
70.00	-.163	-.157	-.148	-.104	-.088	-.077	-.241	-.227	-.202	-.129	-.080	-.087	
75.00	-.119	-.112	-.094	-.086	-.056	-.057	-.161	-.143	-.115	-.065	-.046	-.077	
80.00	-.078	-.073	-.054	-.026	-.023	-.031	-.103	-.091	-.072	-.030	-.020	-.061	
85.00	-.057	-.035	-.014	-.004	-.016	-.005	-.075	-.052	-.032	-.001	-.013	-.042	
90.00	-.010	-.008	-.016	-.035	-.049	-.016	-.030	-.025	-.002	-.027	-.037	-.029	
95.00	.029	.024	.051	.074	.063	.027	.010	.009	.032	.060	.048	.021	
Lower surface													
0.00	.299	.247	.233	.257	.293	.212	.389	.368	.352	.393	.429	.332	
1.25	.236	.161	.165	.181	.182	.156	.321	.268	.276	.293	.307	.262	
5.00	.190	.129	.120	.124	.130	.100	.267	.218	.211	.208	.228	.193	
7.50	.147	.082	.070	.078	.093	.045	.215	.155	.148	.152	.177	.125	
10.00	.111	.057	.034	.048	.053	.010	.175	.123	.103	.119	.127	.080	
15.00	.073	.032	.015	.005	.007	-.066	.127	.091	.081	.076	.074	-.010	
20.00	.033	.007	-.012	-.038	-.029	-.140	.081	.080	.042	.014	.034	-.092	
25.00	.016	.002	-.021	-.056	-.057	-.193	.059	.048	.015	-.009	-.010	-.167	
30.00	.016	-.022	-.042	-.071	-.079	-.202	.051	.016	-.010	-.030	-.035	-.19	
35.00	-.016	-.048	-.069	-.094	-.109	-.173	.004	.016	-.015	-.057	-.066	-.196	
40.00	-.045	-.059	-.083	-.114	-.122	-.194	-.015	-.033	-.058	-.079	-.087	-.248	
45.00	-.038	-.087	-.105	-.141	-.144	-.194	-.010	-.062	-.080	-.107	-.116	-.274	
50.00	-.093	-.104	-.114	-.154	-.164	-.176	-.070	-.084	-.104	-.128	-.138	-.267	
55.00	-.102	-.121	-.128	-.149	-.181	-.143	-.092	-.071	-.117	-.128	-.163	-.229	
60.00	-.125	-.115	-.145	-.164	-.146	-.119	-.097	-.106	-.117	-.128	-.163	-.179	
65.00	-.102	-.113	-.117	-.133	-.146	-.109	-.090	-.105	-.111	-.128	-.161	-.139	
70.00	-.092	-.094	-.098	-.103	-.094	-.082	-.083	-.088	-.095	-.110	-.117	-.100	
75.00	-.116	-.085	-.108	-.075	-.061	-.116	-.016	-.095	-.090	-.093	-.095	-.081	
80.00	-.078	-.064	-.052	-.045	-.037	-.041	-.085	-.072	-.065	-.063	-.062	-.061	
85.00	-.051	-.040	-.017	-.007	-.011	-.013	-.062	-.046	-.033	-.025	-.035	-.005	
90.00	-.013	-.007	.011	.029	.02								

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:												
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent C														
Upper surface	M = 0.90	$\alpha = 5.88^\circ$						M = 0.90	$\alpha = 7.82^\circ$					
	0.00	.048	.395	.235	.184	.100	.448	.044	.222	.044	.197	.308		
	1.25	-.205	-1.021	-1.139	-1.198	-1.040	-.779	-.355	-1.262	-1.309	-1.318	-1.059	-.618	
	2.50	-.266	-1.012	-1.059	-1.100	-1.021	-.968	-.424	-1.111	-1.239	-1.261	-1.036	-.656	
	5.00	-.410	-1.616	-1.724	-1.902	-1.947	-.968	-.580	-1.863	-1.152	-1.177	-1.976	-.652	
	7.50	-.364	-1.360	-1.601	-1.897	-1.943	-.917	-.540	-1.600	-1.039	-1.126	-1.950	-.648	
	10.00	-.374	-1.360	-1.724	-1.947	-1.022	-.941	-.512	-1.537	-1.956	-1.090	-1.927	-.645	
	12.50	-.372	-1.344	-1.422	-1.718	-1.931	-.893	-.439	-1.488	-1.693	-1.984	-1.912	-.650	
	15.00	-.253	-1.359	-1.419	-1.621	-1.878	-.874	-.368	-1.468	-1.579	-1.900	-1.872	-.645	
	20.00	-.315	-1.336	-1.399	-1.528	-1.772	-.844	-.409	-1.433	-1.504	-1.762	-1.841	-.657	
Lower surface	25.00	-.402	-1.359	-1.407	-1.467	-1.748	-.780	-.484	-1.452	-1.492	-1.616	-1.820	-.659	
	30.00	-.348	-1.378	-1.417	-1.464	-1.697	-.686	-.438	-1.466	-1.490	-1.569	-1.785	-.646	
	35.00	-.374	-1.386	-1.436	-1.479	-1.587	-.665	-.466	-1.475	-1.500	-1.552	-1.706	-.634	
	40.00	-.389	-1.389	-1.444	-1.492	-1.551	-.567	-.466	-1.475	-1.505	-1.540	-1.674	-.612	
	45.00	-.370	-1.389	-1.445	-1.504	-1.497	-.504	-.461	-1.471	-1.495	-1.544	-1.629	-.593	
	50.00	-.332	-1.408	-1.463	-1.514	-1.469	-.475	-.415	-1.483	-1.483	-1.544	-1.599	-.581	
	55.00	-.412	-1.433	-1.476	-1.514	-1.398	-.428	-.491	-1.503	-1.476	-1.541	-1.571	-.560	
	60.00	-.398	-1.416	-1.458	-1.399	-1.283	-.368	-.477	-1.470	-1.425	-1.480	-1.518	-.528	
	65.00	-.346	-1.215	-1.163	-1.095	-1.132	-.357	-.413	-1.280	-1.305	-1.344	-1.430	-.423	
	70.00	-.245	-1.017	-1.065	-1.040	-1.033	-.315	-.318	-1.111	-1.093	-1.232	-1.357	-.463	
Upper surface	75.00	-.126	-1.052	-1.020	-1.004	-1.050	-.260	-.318	-1.118	-1.111	-1.093	-1.322	-.472	
	80.00	-.070	-1.052	-1.020	-1.004	-1.050	-.260	-.301	-1.118	-1.111	-1.093	-1.322	-.472	
	85.00	-.017	-1.018	-1.015	-1.024	-1.015	-.260	-.305	-1.053	-1.049	-1.179	-1.227	-.472	
	90.00	.026	-1.017	.043	.059	.012	-.239	-.009	-1.023	-.007	-1.147	-.287	-.459	
	95.00													
Lower surface	1.25	.516	.508	.489	.515	.545	.443	.630	.621	.590	.603	.617	.508	
	2.50	.453	.403	.406	.416	.432	.369	.582	.521	.515	.521	.521	.442	
	5.00	.394	.332	.322	.329	.345	.301	.510	.436	.426	.423	.433	.377	
	7.50	.334	.264	.261	.252	.288	.233	.440	.363	.356	.356	.377	.308	
	10.00	.284	.229	.206	.220	.233	.180	.387	.329	.309	.314	.323	.254	
	12.50	.227	.188	.170	.167	.174	.081	.317	.272	.256	.255	.258	.157	
	15.00	.169	.166	.125	.094	.123	-.001	.248	.243	.209	.183	.202	.073	
	20.00	.140	.125	.086	.068	.078	-.077	.216	.192	.163	.148	.154	.002	
	25.00	.084	.063	.040	.046	.123	-.123	.192	.154	.133	.119	.120	-.047	
	30.00	.064	.054	.036	.012	.009	-.134	.118	.121	.103	.085	.077	-.010	
Upper surface	35.00	.055	.034	.013	-.014	.013	-.190	.113	.096	.083	.053	.051	-.123	
	40.00	.055	.004	-.011	-.045	.040	-.230	.107	.059	.050	.018	.021	-.171	
	45.00	.009	-.021	-.036	-.067	.060	-.244	.038	-.024	-.018	-.014	-.016	-.196	
	50.00	-.025	-.040	-.049	-.011	-.098	-.232	.019	-.009	-.004	-.019	-.051	-.193	
	55.00	-.039	-.049	-.054	-.059	-.091	-.111	-.021	-.005	-.009	-.018	-.034	-.203	
	60.00	-.039	-.049	-.054	-.059	-.090	-.123	-.021	-.004	-.019	-.025	-.057	-.218	
	65.00	-.044	-.054	-.059	-.064	-.084	-.100	-.021	-.004	-.019	-.033	-.085	-.193	
	70.00	-.032	-.045	-.049	-.059	-.075	-.100	-.021	-.004	-.019	-.027	-.062	-.100	
	75.00	-.072	-.057	-.056	-.075	-.091	-.145	-.021	-.047	-.037	-.043	-.062	-.100	
	80.00	-.049	-.041	-.043	-.050	-.070	-.124	-.021	-.042	-.032	-.034	-.058	-.189	
Lower surface	85.00	-.038	-.021	-.015	-.021	-.049	-.069	-.021	-.037	-.025	-.020	-.046	-.102	
	90.00	-.008	-.001	-.004	-.004	-.017	-.098	-.023	-.015	-.013	-.041	-.094	-.181	
	95.00	.028	-.018	.037	.024	.005	-.088	.007	-.004	-.009	-.051	.114	-.174	
Upper surface	M = 0.90	$\alpha = 9.87^\circ$						M = 0.90	$\alpha = 11.82^\circ$					
	0.00	.037	.026	-.174	-.324	-.481	.124	.025	-.211	-.442	-.634	.704	-.111	
	1.25	-.492	-1.377	-1.387	-1.093	-.826	-.584	-.651	-.1435	-.1771	-.917	.700	-.579	
	2.50	-.572	-1.251	-1.333	-1.065	-.832	-.592	-.752	-.1374	-.1449	-.892	-.793	-.577	
	5.00	-.728	-1.076	-1.273	-1.053	-.809	-.584	-.907	-.1240	-.1143	-.895	-.757	-.573	
	7.50	-.690	-.184	-.181	-.103	-.798	-.579	-.850	-.1147	-.1115	-.890	-.748	-.565	
	10.00	-.653	.799	.126	.002	-.811	-.579	-.808	-.1081	-.1101	-.882	-.760	-.565	
	12.50	-.525	.730	.192	.063	-.800	-.579	-.763	-.1041	-.1007	-.882	-.760	-.565	
	15.00	-.476	.802	.184	.044	-.82	-.579	-.756	-.0981	-.1007	-.882	-.760	-.565	
	20.00	-.419	.519	.112	.048	-.748	-.584	-.658	-.0610	-.0877	-.857	-.757	-.566	
Lower surface	25.00	-.465	.492	.170	.071	-.761	-.765	-.599	-.0528	-.0836	-.839	-.751	-.570	
	30.00	-.501	.499	.162	.074	-.746	-.757	-.557	-.0542	-.0801	-.817	-.740	-.574	
	35.00	-.502	.502	.173	.073	-.735	-.753	-.579	-.0542	-.0776	-.790	-.727	-.576	
	40.00	-.497	.498	.166	.076	-.718	-.753	-.548	-.0542	-.0758	-.754	-.720	-.580	
	45.00	-.447	.487	.167	.077	-.700	-.759	-.500	-.0541	-.0713	-.714	-.706	-.583	
	50.00	-.494	.509	.151	.062	-.659	-.583	-.557	-.0554	-.0688	-.692	-.699	-.584	
	55.00	-.487	.498	.152	.058	-.639	-.573	-.535	-.0535	-.0664	-.671	-.692	-.585	
	60.00	-.465	.465	.197	.055	-.609	-.568	-.520	-.0515	-.0617	-.649	-.677	-.588	
	65.00	-.413	.443	.140	.053	-.584	-.576	-.480	-.0490	-.0576	-.630	-.667	-.598	
	70.00	-.327	.311	.279	.254	-.263	-.131	-.395	-.379	-.345	-.320	-.318	-.181	
Upper surface	75.00	-.299	.259	.231	.203	-.212	-.066	-.352	-.320	-.297	-.276	-.269	-.119	
	80.00	-.229	.235	.285	.246	-.236	-.054	-.375	-.348	-.320	-.280	-.262	-.062	
	85.00	-.141	.163	.225	.146	-.508	-.559	-.280	-.304	-.297	-.242	-.246	-.034	
	90.00	-.073	.106	.163	.093	-.484	-.550	-.184	-.225	-.225	-.194	-.180	-.032	
	95.00	.179	.182	.186	.138	.130	-.017	.225	.204	.188	.159	.150	-.034	
Lower surface	1.25	.733	.709	.660	.653	.651	.542	.799	.690	.663	.643	.626	.518	
	2.50	.701	.610	.593	.585	.584	.483	.719	.600	.576	.557	.551	.471	
	5.00	.624	.525	.502	.497	.495	.428	.143	.129	.117	.090	.072	.115	
	7.50	.546	.454	.440	.423	.440	.360	.631	.529	.511	.493	.494	.409	
	10.00	.480	.414	.394	.381	.384	.309	.559	.485	.472	.452	.441	.359	
	12.50	.403	.346	.334	.320	.317	.214	.474	.416	.396	.388	.374	.264	
	15.00	.327	.271	.254	.263	.261	.131	.395	.379	.345	.320	.318	.181	
	20.00	.290	.259	.231	.203	.212	.066	.352	.320	.297	.276	.269	.119	
	25.00	.259	.218	.196	.177	.174	.010	.314	.275	.260	.237	.228	.063	
	30.00	.179	.182	.186	.138	.130	-.017	.227	.225	.225	.194	.180	-.032	
Upper surface	35.00	.173	.152	.128	.108	.100	-.077	.225	.204	.188	.159	.150	-.034	

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:											
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent	C	M = 0.90	a = 15.43°				M = 0.90	a = 17.43°					
Upper surface	0.00	.026	-.674	-.899	-1.011	-.691	-.492	.010	-.816	-.967	-.787	-.667	-.601
	1.25	-.880	-1.177	-.924	-.785	-.659	-.560	-.813	-.862	-.789	-.757	-.650	-.593
	2.50	-.1004	-1.200	-.914	-.750	-.650	-.550	-.709	-.847	-.786	-.715	-.616	-.554
	5.00	-.1169	-1.180	-.920	-.716	-.654	-.558	-.807	-.872	-.797	-.716	-.645	-.582
	7.50	-.1042	-1.159	-.923	-.710	-.648	-.559	-.810	-.875	-.792	-.691	-.644	-.583
	10.00	-.982	-1.120	-.930	-.710	-.647	-.559	-.821	-.871	-.809	-.691	-.638	-.585
	15.00	-.795	-1.086	-.909	-.717	-.645	-.561	-.810	-.870	-.818	-.687	-.643	-.586
	20.00	-.723	-1.026	-.882	-.717	-.640	-.561	-.780	-.857	-.797	-.681	-.643	-.586
	25.00	-.679	-.961	-.852	-.717	-.638	-.560	-.742	-.838	-.766	-.685	-.639	-.585
	30.00	-.641	-.874	-.826	-.710	-.635	-.560	-.714	-.822	-.760	-.681	-.639	-.583
	35.00	-.602	-.803	-.807	-.705	-.635	-.562	-.654	-.808	-.756	-.680	-.638	-.580
	40.00	-.583	-.724	-.788	-.699	-.632	-.563	-.625	-.779	-.751	-.680	-.636	-.588
	45.00	-.541	-.678	-.775	-.692	-.632	-.566	-.586	-.753	-.745	-.678	-.638	-.586
	50.00	-.552	-.638	-.764	-.688	-.631	-.567	-.589	-.722	-.736	-.677	-.638	-.588
	55.00	-.567	-.610	-.750	-.682	-.628	-.568	-.583	-.698	-.729	-.672	-.638	-.593
	60.00	-.560	-.599	-.729	-.671	-.628	-.570	-.589	-.684	-.724	-.666	-.639	-.596
	65.00	-.531	-.573	-.703	-.663	-.625	-.572	-.573	-.670	-.714	-.659	-.638	-.593
	70.00	-.521	-.565	-.696	-.663	-.623	-.574	-.565	-.658	-.708	-.658	-.632	-.597
	75.00	-.488	-.557	-.682	-.653	-.622	-.575	-.559	-.644	-.697	-.658	-.633	-.604
	80.00	-.488	-.547	-.665	-.648	-.620	-.578	-.559	-.638	-.691	-.655	-.632	-.604
	85.00	-.494	-.533	-.654	-.645	-.613	-.581	-.560	-.625	-.684	-.657	-.624	-.602
	90.00	-.471	-.512	-.635	-.641	-.604	-.582	-.554	-.612	-.675	-.653	-.618	-.608
	95.00	-.371	-.464	-.613	-.637	-.612	-.581	-.484	-.582	-.663	-.658	-.625	-.609
Lower surface	1.25	.928	.851	.775	.719	.678	.586	.959	.876	.788	.724	.669	.585
	2.50	.964	.799	.751	.712	.684	.562	1.014	.844	.779	.737	.701	.572
	5.00	.872	.724	.682	.650	.634	.534	.918	.772	.726	.693	.667	.557
	7.50	.749	.660	.625	.598	.588	.486	.825	.709	.673	.646	.629	.515
	10.00	.697	.611	.583	.560	.544	.439	.750	.660	.631	.608	.584	.471
	15.00	.603	.543	.513	.488	.478	.354	.654	.590	.565	.540	.516	.390
	20.00	.527	.500	.451	.422	.422	.277	.578	.546	.504	.476	.460	.314
	25.00	.471	.435	.402	.378	.373	.211	.522	.487	.456	.431	.414	.250
	30.00	.431	.384	.360	.338	.328	.148	.477	.441	.414	.392	.370	.186
	35.00	.336	.343	.319	.294	.280	.119	.388	.393	.370	.343	.323	.155
	40.00	.336	.303	.281	.257	.251	.055	.382	.354	.335	.306	.292	.093
	45.00	.312	.269	.246	.217	.210	-.005	.355	.318	.297	.267	.251	.032
	50.00	.245	.227	.207	.179	.172	-.033	.288	.273	.257	.226	.212	.001
	55.00	.204	.194	.179	.156	.125	-.055	.242	.238	.228	.200	.164	-.025
	60.00	.194	.165	.145	.123	.087	-.079	.232	.208	.190	.164	.127	-.051
	65.00	.150	.128	.120	.098	.052	-.101	.188	.170	.162	.133	.092	-.072
	70.00	.111	.111	.096	.068	.042	-.113	.142	.150	.134	.111	.080	-.090
	75.00	.088	.075	.063	.041	.012	-.127	.118	.108	.100	.078	.064	-.107
	80.00	.061	.052	.037	.020	-.009	-.144	.095	.084	.074	.07	.050	-.127
	85.00	.030	.028	.021	-.003	-.037	-.11	.052	.058	.052	.031	-.009	-.116
	90.00	.007	.002	.022	-.033	-.061	-.174	.014	.022	.008	-.006	-.042	-.166
	95.00	-.053	-.059	-.068	-.098	-.112	-.180	-.018	-.040	-.043	-.078	-.098	-.174
Upper surface	0.00	.014	-.814	-.778	-.771	-.706	-.667	.092	-.830	-.828	-.814	-.784	-.750
	1.25	-.752	-.755	-.758	-.762	-.695	-.653	-.819	-.819	-.821	-.807	-.777	-.722
	2.50	-.735	-.752	-.745	-.746	-.694	-.654	-.808	-.824	-.813	-.800	-.778	-.721
	5.00	-.725	-.752	-.749	-.730	-.694	-.654	-.800	-.825	-.819	-.795	-.776	-.718
	7.50	-.730	-.755	-.749	-.730	-.692	-.654	-.808	-.827	-.810	-.795	-.771	-.720
	10.00	-.734	-.755	-.753	-.730	-.685	-.655	-.806	-.828	-.817	-.795	-.772	-.719
	15.00	-.742	-.769	-.759	-.728	-.692	-.658	-.814	-.833	-.819	-.794	-.772	-.720
	20.00	-.752	-.769	-.759	-.723	-.694	-.658	-.817	-.831	-.821	-.798	-.771	-.720
	25.00	-.752	-.764	-.759	-.723	-.694	-.657	-.811	-.833	-.821	-.790	-.768	-.720
	30.00	-.752	-.764	-.759	-.724	-.691	-.653	-.815	-.833	-.822	-.789	-.768	-.721
	35.00	-.713	-.768	-.760	-.724	-.691	-.651	-.763	-.831	-.822	-.789	-.768	-.721
	40.00	-.692	-.765	-.760	-.726	-.691	-.661	-.738	-.824	-.821	-.791	-.767	-.723
	45.00	-.661	-.759	-.726	-.694	-.658	-.605	-.709	-.821	-.821	-.788	-.767	-.723
	50.00	-.666	-.749	-.725	-.695	-.661	-.661	-.704	-.811	-.811	-.788	-.767	-.726
	55.00	-.647	-.740	-.724	-.697	-.667	-.667	-.715	-.804	-.811	-.785	-.766	-.728
	60.00	-.662	-.738	-.724	-.718	-.670	-.667	-.705	-.787	-.813	-.777	-.755	-.727
	65.00	-.647	-.731	-.749	-.714	-.664	-.664	-.705	-.780	-.810	-.779	-.751	-.729
	70.00	-.635	-.718	-.739	-.714	-.664	-.659	-.676	-.767	-.805	-.776	-.742	-.730
	75.00	-.621	-.709	-.739	-.714	-.664	-.658	-.676	-.767	-.794	-.776	-.742	-.730
	80.00	-.624	-.703	-.737	-.714	-.665	-.657	-.681	-.754	-.799	-.776	-.742	-.730
	85.00	-.622	-.694	-.733	-.714	-.668	-.654	-.684	-.733	-.793	-.776	-.754	-.729
	90.00	-.626	-.688	-.726	-.709	-.681	-.681	-.675	-.717	-.783	-.773	-.745	-.729
	95.00	-.553	-.651	-.713	-.713	-.689	-.683	-.562	-.670	-.770	-.771	-.757	-.726
Lower surface	1.25	.971	.898	.873	.712	.642	.567	.948	.891	.783	.695	.608	.546
	2.50	1.048	.885	.807	.741	.698	.570	1.050	.908	.816	.743	.692	.560
	5.00	.968	.830	.768	.714	.684	.567	.990	.860	.793	.733	.698	.570
	7.50	.879	.769	.719	.677	.652	.533	.908	.803	.754	.704	.713	.547
	10.00	.806	.725	.679	.643	.613	.495	.840	.767	.719	.676	.656	.514
	15.00	.714	.653	.616	.584	.553	.422	.749	.691	.659	.622	.588	.449
	20.00	.638	.589	.557	.523	.506	.353	.678	.629	.605	.563	.541	.381
	25.00	.581	.549	.510	.476	.459	.288	.622	.587	.556	.518	.497	.321
	30.00	.538	.502	.466	.438	.416	.225	.576	.542	.508	.479	.452	.258
	35.00	.448	.452	.421	.389	.368	.192	.489	.494	.463	.431	.412	.149
	40.00	.441	.413	.385	.351	.337	.13	.440	.42	.420	.387	.372	.143
	45.00	.347	.374	.343	.310	.296	.049	.448	.413	.399	.350	.334	.100
	50.00	.347	.332	.306	.270	.257	.036	.381	.345	.344	.312	.293	.065
	55.00	.304	.293	.274	.246	.210	.007	.320	.310	.286	.248	.237	.037
	60.00	.291	.260	.236	.209	.169	-.021	.325	.297	.247	.203	.166	-.022
	65.00	.237	.224	.220	.171	.132	-.043	.271	.254	.242	.210	.166	-.022
	70.00	.192	.201	.176	.148	.118	-.068	.220	.227	.215	.184	.149	-.048
	75.00	.167	.160	.143	.117	.080	-.098	.188	.184	.177	.149	.111	-.069
	80.00	.132	.131	.116	.088	.052	-.112	.156	.156	.143	.117	.079	-.098
	85.00	.092	.096	.087	.055	.021	-.103	.105	.121	.112	.086	.040	-.091
	90.00	.043	.059	.									

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:														
Percent c	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2	
Upper surface	M = 0.90	$\alpha = 23.68^\circ$						M = 0.90	$\alpha = 25.78^\circ$					
0.00	-+.246	-.998	-.991	-.973	-.947	-.898		-.310	-.1093	-.1.092	-.1.062	-.1.033	-.056	
1.25	-.983	-.991	-.986	-.970	-.934	-.859		-.1.082	-.1.063	-.1.086	-.1.061	-.1.021	-.022	
2.50	-.970	-.990	-.979	-.960	-.931	-.857		-.1.070	-.1.089	-.1.057	-.1.051	-.1.014	-.020	
5.00	-.969	-.993	-.985	-.951	-.928	-.853		-.1.070	-.1.087	-.1.089	-.1.077	-.1.030	-.016	
7.50	-.971	-.992	-.974	-.951	-.923	-.854		-.1.075	-.1.086	-.1.076	-.1.074	-.1.037	-.017	
10.00	-.972	-.986	-.961	-.951	-.920	-.854		-.1.079	-.1.088	-.1.084	-.1.047	-.1.007	-.016	
12.50	-.979	-.982	-.955	-.950	-.923	-.853		-.1.082	-.1.091	-.1.091	-.1.048	-.1.005	-.014	
20.00	-.975	-.988	-.985	-.942	-.925	-.850		-.1.064	-.1.098	-.1.091	-.1.039	-.1.009	-.013	
25.00	-.931	-.988	-.981	-.946	-.921	-.850		-.952	-.1.087	-.1.082	-.1.044	-.1.002	-.008	
30.00	-.889	-.994	-.983	-.943	-.920	-.849		-.894	-.1.085	-.1.087	-.1.039	-.1.002	-.003	
35.00	-.820	-.990	-.980	-.941	-.919	-.849		-.857	-.1.075	-.1.087	-.1.037	-.1.000	-.000	
40.00	-.793	-.974	-.980	-.941	-.915	-.854		-.833	-.1.047	-.1.086	-.1.037	-.093	-.009	
45.00	-.773	-.948	-.977	-.938	-.915	-.853		-.787	-.990	-.1.081	-.1.031	-.095	-.004	
50.00	-.738	-.918	-.973	-.937	-.913	-.853		-.740	-.923	-.1.071	-.1.032	-.090	-.003	
55.00	-.714	-.888	-.970	-.932	-.910	-.856		-.715	-.853	-.1.062	-.1.024	-.087	-.006	
60.00	-.732	-.856	-.964	-.918	-.909	-.856		-.695	-.803	-.1.051	-.1.012	-.085	-.004	
65.00	-.709	-.804	-.958	-.918	-.905	-.852		-.663	-.724	-.1.032	-.1.004	-.079	-.006	
70.00	-.685	-.780	-.951	-.918	-.901	-.852		-.634	-.677	-.1.007	-.098	-.069	-.003	
75.00	-.665	-.753	-.938	-.916	-.898	-.855		-.598	-.628	-.966	-.1.000	-.065	-.007	
80.00	-.656	-.735	-.920	-.914	-.896	-.851		-.574	-.578	-.926	-.092	-.059	-.002	
85.00	-.652	-.694	-.901	-.914	-.884	-.848		-.545	-.511	-.876	-.082	-.045	-.000	
90.00	-.611	-.649	-.866	-.908	-.876	-.846		-.468	-.455	-.817	-.068	-.031	-.003	
95.00	-.465	-.551	-.786	-.900	-.890	-.842		-.357	-.375	-.681	-.043	-.040	-.078	
Lower surface		.913	.893	.774	.669	.569	.516	.871	.890	.762	.641	.534	.489	
1.25	1.045	.928	.930	.740	.684	.544		1.034	.942	.831	.731	.671	.531	
5.00	1.012	.899	.823	.760	.712	.568		1.026	.927	.842	.771	.721	.567	
7.50	.948	.851	.793	.738	.730	.558		.971	.890	.822	.759	.718	.566	
10.00	.881	.812	.763	.713	.677	.531		.913	.855	.799	.741	.702	.548	
15.00	.792	.748	.703	.661	.622	.471		.831	.791	.743	.695	.654	.495	
20.00	.723	.686	.651	.609	.577	.411		.767	.736	.693	.646	.614	.438	
25.00	.662	.593	.574	.537	.537	.352		.714	.686	.646	.605	.576	.376	
30.00	.622	.575	.560	.528	.494	.329		.669	.638	.605	.567	.534	.327	
35.00	.545	.562	.515	.480	.447	.255		.592	.595	.563	.523	.491	.288	
40.00	.529	.500	.476	.439	.417	.196		.574	.556	.527	.486	.459	.231	
45.00	.495	.456	.436	.401	.377	.130		.543	.511	.486	.441	.419	.168	
50.00	.436	.414	.395	.359	.337	.095		.478	.467	.444	.402	.381	.135	
55.00	.388	.382	.364	.331	.287	.062		.433	.431	.408	.375	.332	.099	
60.00	.370	.338	.321	.292	.246	.032		.412	.389	.368	.336	.288	.069	
65.00	.308	.299	.290	.252	.206	.000		.361	.347	.334	.294	.250	.035	
70.00	.258	.273	.251	.224	.188	-.032		.300	.320	.303	.265	.228	.004	
75.00	.231	.226	.218	.191	.146	-.055		.274	.270	.260	.225	.185	.027	
80.00	.193	.193	.181	.157	.109	-.082		.233	.238	.225	.191	.147	.057	
85.00	.138	.155	.148	.122	.070	-.082		.180	.200	.190	.151	.105	.057	
90.00	.085	.110	.096	.072	.025	-.148		.123	.150	.133	.100	.054	.128	
95.00	.001	.036	.026	-.018	-.049	-.168		.039	.079	-.056	.002	-.024	-.150	

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:												
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent C		$M = 0.94$ $\alpha = -2.02^\circ$						$M = 0.94$ $\alpha = 0^\circ$						
Upper surface	0.00	.041	.701	.645	.609	.549	.456	.056	.730	.678	.685	.648	.685	
	1.25	.323	.238	.257	.271	.256	.290	.217	.038	.021	.024	.058	.060	
	2.50	.266	.146	.162	.170	.174	.165	.152	-.013	-.029	-.065	-.093	-.118	
	5.00	.201	.125	.108	.101	.093	.115	.088	-.016	-.027	-.074	-.115	-.120	
	7.50	.167	.089	.076	.059	.046	.068	.060	-.016	-.046	-.091	-.133	-.145	
	10.00	.132	.061	.040	.032	.015	.023	.033	-.025	-.067	-.111	-.142	-.161	
	15.00	.090	.030	.002	.010	-.024	-.060	.013	-.049	-.086	-.109	-.156	-.197	
	20.00	.040	-.003	-.026	-.023	-.051	-.136	-.004	-.077	-.115	-.133	-.166	-.233	
	25.00	.014	-.022	-.046	-.065	-.088	-.239	-.053	-.089	-.128	-.154	-.189	-.298	
	30.00	-.004	-.038	-.060	-.089	-.101	-.268	-.131	-.106	-.136	-.171	-.199	-.298	
	35.00	-.046	-.066	-.084	-.110	-.134	-.288	-.104	-.133	-.144	-.189	-.222	-.294	
	40.00	-.069	-.076	-.108	-.137	-.155	-.353	-.122	-.133	-.172	-.208	-.241	-.340	
	45.00	-.073	-.093	-.114	-.143	-.165	-.346	-.142	-.147	-.171	-.229	-.265	-.334	
	50.00	-.073	-.115	-.162	-.186	-.206	-.366	-.154	-.161	-.214	-.240	-.297	-.348	
	55.00	-.092	-.152	-.190	-.217	-.252	-.366	-.124	-.198	-.240	-.274	-.315	-.368	
	60.00	-.158	-.173	-.193	-.226	-.278	-.348	-.206	-.228	-.259	-.296	-.339	-.393	
	65.00	-.154	-.166	-.196	-.230	-.278	-.367	-.207	-.223	-.264	-.312	-.344	-.371	
	70.00	-.165	-.170	-.193	-.230	-.298	-.326	-.229	-.230	-.259	-.309	-.373	-.331	
	75.00	-.149	-.170	-.186	-.210	-.281	-.241	-.207	-.230	-.259	-.284	-.340	-.234	
	80.00	-.129	-.133	-.132	-.137	-.183	-.125	-.162	-.180	-.179	-.045	-.179	-.091	
	85.00	-.093	-.060	-.052	-.044	-.036	-.027	-.098	-.062	-.040	-.019	-.009	-.018	
	90.00	-.022	-.019	-.005	-.027	-.049	-.031	-.011	-.000	-.029	-.068	-.093	-.078	
	95.00	-.022	-.016	-.043	-.072	-.071	-.046	-.044	-.041	-.073	-.108	-.118	-.100	
Lower surface	1.25	.063	-.248	-.401	-.727	-.874	-.936	.203	.066	.006	-.037	-.038	-.101	
	2.50	.003	-.195	-.263	-.551	-.742	-.875	.138	.005	-.026	-.056	-.068	-.100	
	5.00	-.024	-.131	-.206	-.261	-.421	-.794	.101	.019	-.026	-.057	-.085	-.114	
	7.50	-.045	-.132	-.233	-.268	-.527	-.717	.071	-.010	-.048	-.084	-.103	-.136	
	10.00	-.083	-.143	-.204	-.281	-.322	-.600	.031	-.027	-.064	-.099	-.120	-.146	
	15.00	-.096	-.146	-.201	-.265	-.315	-.415	.005	-.040	-.075	-.111	-.139	-.178	
	20.00	-.123	-.145	-.202	-.284	-.332	-.406	-.028	-.060	-.102	-.137	-.163	-.240	
	25.00	-.144	-.149	-.199	-.265	-.330	-.394	-.049	-.049	-.103	-.146	-.174	-.280	
	30.00	-.157	-.167	-.217	-.237	-.313	-.317	-.035	-.035	-.097	-.117	-.143	-.243	
	35.00	-.148	-.202	-.239	-.291	-.329	-.311	-.107	-.137	-.183	-.213	-.245	-.345	
	40.00	-.198	-.202	-.239	-.292	-.329	-.346	-.104	-.101	-.158	-.200	-.227	-.308	
	45.00	-.169	-.208	-.258	-.317	-.345	-.373	-.083	-.132	-.187	-.232	-.252	-.337	
	50.00	-.219	-.246	-.286	-.343	-.374	-.394	-.146	-.170	-.214	-.258	-.281	-.359	
	55.00	-.239	-.266	-.298	-.361	-.407	-.411	-.167	-.189	-.233	-.269	-.315	-.374	
	60.00	-.270	-.290	-.321	-.379	-.430	-.412	-.201	-.217	-.251	-.292	-.336	-.374	
	65.00	-.284	-.295	-.331	-.397	-.450	-.419	-.209	-.220	-.256	-.316	-.359	-.376	
	70.00	-.292	-.287	-.329	-.383	-.438	-.391	-.214	-.211	-.250	-.291	-.435	-.327	
	75.00	-.339	-.320	-.335	-.385	-.411	-.328	-.257	-.238	-.247	-.291	-.336	-.232	
	80.00	-.305	-.309	-.320	-.319	-.354	-.224	-.205	-.202	-.220	-.217	-.190	-.106	
	85.00	-.213	-.199	-.217	-.213	-.261	-.215	-.115	-.089	-.073	-.042	-.010	-.036	
	90.00	-.075	-.058	-.010	-.027	-.034	-.001	-.020	-.006	-.040	-.060	-.077	-.066	
	95.00	-.009	-.009	-.055	-.073	-.083	-.058	-.037	-.037	-.075	-.097	-.120	-.111	
Upper surface	0.00	$M = 0.94$ $\alpha = 1.92^\circ$						$M = 0.94$ $\alpha = 3.88^\circ$						
	1.25	.039	.658	.559	.569	.547	.643	.044	.542	.414	.388	.359	.598	
	2.50	.078	-.222	-.341	-.757	-.867	-.716	.058	-.945	-.1079	-.1158	-.1176	-.023	
	5.00	.018	-.49	-.251	-.458	-.764	-.916	.122	.510	.954	.1042	.1099	-.145	
	7.50	-.101	-.151	-.232	-.252	-.300	-.768	.247	.401	.758	.1011	.013	-.109	
	10.00	-.100	-.151	-.214	-.224	-.296	-.361	.162	.702	.239	.286	.315	-.901	
	15.00	-.085	-.155	-.225	-.280	-.353	-.503	.175	.448	.321	.390	.421	-.885	
	20.00	-.089	-.187	-.234	-.297	-.347	-.407	.166	.269	.349	.402	.478	-.938	
	25.00	-.154	-.177	-.236	-.290	-.338	-.409	.234	.262	.325	.380	.445	-.927	
	30.00	-.237	-.202	-.251	-.300	-.344	-.348	.310	.281	.333	.384	.417	-.879	
	35.00	-.196	-.232	-.264	-.312	-.361	-.336	.267	.303	.346	.392	.426	-.803	
	40.00	-.222	-.235	-.285	-.337	-.376	-.394	.299	.310	.365	.419	.445	-.816	
	45.00	-.245	-.246	-.290	-.339	-.394	-.394	.319	.322	.375	.430	.460	-.774	
	50.00	-.224	-.252	-.298	-.356	-.410	-.419	.297	.322	.382	.444	.485	-.722	
	55.00	-.203	-.280	-.320	-.371	-.427	-.428	.269	.346	.400	.463	.508	-.605	
	60.00	-.286	-.308	-.340	-.383	-.438	-.410	.353	.374	.415	.468	.527	-.499	
	65.00	-.292	-.305	-.348	-.398	-.434	-.436	.360	.374	.421	.478	.521	-.480	
	70.00	-.306	-.309	-.344	-.401	-.452	-.411	.373	.374	.416	.479	.536	-.458	
	75.00	-.301	-.321	-.353	-.395	-.424	-.348	.366	.386	.424	.475	.536	-.439	
	80.00	-.288	-.313	-.331	-.272	-.268	-.216	.387	-.043	-.425	-.614	-.505	-.429	
	85.00	-.215	-.190	-.168	-.118	-.064	-.083	.0361	-.357	-.388	-.358	-.234	-.356	
	90.00	-.075	-.058	-.018	.014	.038	.006	.0184	-.173	-.148	-.091	-.043	-.190	
	95.00	-.015	.009	.052	.076	.081	.044	.0205	-.038	-.003	.024	.030	-.077	
Lower surface	1.25	.314	.262	.246	.263	.315	.231	.436	.431	.416	.438	.486	.384	
	2.50	.248	.166	.170	.188	.217	.167	.382	.323	.342	.374	.311		
	5.00	.204	.133	.121	.128	.126	.114	.328	.262	.253	.252	.270	.247	
	7.50	.163	.090	.074	.081	.090	.055	.277	.209	.197	.198	.214	.182	
	10.00	.123	.061	.046	.045	.046	.016	.228	.173	.164	.154	.159	.127	
	15.00	.083	.035	.019	.003	-.005	-.057	.183	.138	.126	.109	.104	.037	
	20.00	.045	.005	.017	.040	.043	.140	.134	.137	.077	.054	.064	-.047	
	25.00	.024	-.008	-.027	-.061	-.077	-.221	.108	.091	.051	.023	.022	-.134	
	30.00	.020	-.028	-.045	.082	.097	.264	.095	.053	.025	-.005	-.003	-.178	
	35.00	-.021	-.055	-.069	.113	.125	.258	.037	.022	-.002	-.034	-.044	-.178	
	40.00	-.045	-.067	-.092	.138	.148	.319	.021	.002	-.030	-.064	-.066	-.254	
	45.00	-.040	-.094	.125	.168	.180	.359	.021	-.027	-.059	-.092	-.100	-.308	
	50.00	-.105	-.131	-.156	-.194	.207	.379	-.040	-.1058	-.1088	-.1122	-.1129	-.338	
	55.00	-.124	-.150	-.175	.212	.250	.384	-.067	-.083	-.104	-.137	-.173	-.362	
	60.00	-.157	-.171	-.193	.229	.276	.376	-.086	-.099	-.119	-.157	-.195	-.349	
	65.00	-.157	-.177	-.195	.244	.300	.382	-.097	-.109	-.136	-.179	-.224	-.392	
	70.00	-.161	-.166	-.188	.229	.292	.343	-.097	-.106	-.134	-.171	-.224	-.385	
	75.00	-.206	-.192	-.199	.236</									

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:													
	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent c	M = 0.94	a = 5.91°		M = 0.94	a = 7.80°								
Upper surface													
0.00	.052	.411	.262	.191	.114	.479		.032	.237	.073	.052	.196	.293
1.25	-.190	-1.156	-1.251	-1.305	-1.324	-1.088		-.334	-1.338	-1.385	-1.389	-1.404	-1.255
2.50	-.260	-1.059	-1.119	-1.200	-1.260	-1.320		-.412	-1.237	-1.273	-1.339	-1.364	-1.422
5.00	-.407	-1.730	-1.030	-1.120	-1.168	-1.240		-.568	-1.94	-1.424	-1.263	-1.305	-1.368
7.50	-.384	-1.408	-1.966	-1.063	-1.103	-1.179		-.536	-1.665	-1.105	-1.240	-1.144	-1.320
10.00	-.361	-1.383	-1.898	-1.020	-1.091	-1.144		-.513	-1.79	-1.095	-1.165	-1.225	-1.287
15.00	-.278	-1.346	-1.446	-1.040	-1.071	-1.111		-.412	-1.498	-1.061	-1.091	-1.181	-1.254
20.00	-.257	-1.347	-1.396	-1.055	-1.083	-1.076		-.378	-1.460	-1.012	-1.064	-1.133	-1.218
25.00	-.213	-1.348	-1.400	-1.072	-1.047	-1.061		-.307	-1.440	-1.043	-1.027	-1.097	-1.200
30.00	-.372	-1.349	-1.400	-1.015	-1.022	-1.022		-.455	-1.440	-1.091	-1.076	-1.169	
35.00	-.379	-1.368	-1.411	-1.074	-1.097	-1.039		-.431	-1.458	-1.492	-1.783	-1.062	-1.077
40.00	-.373	-1.375	-1.428	-1.074	-1.025	-1.048		-.463	-1.462	-1.501	-1.688	-1.053	-1.080
45.00	-.373	-1.382	-1.440	-1.080	-1.078	-1.011		-.437	-1.470	-1.515	-1.653	-1.047	-1.047
50.00	-.364	-1.386	-1.452	-1.099	-1.000	-1.011		-.445	-1.470	-1.527	-1.633	-1.040	-1.053
55.00	-.330	-1.408	-1.462	-1.521	-1.585	-1.910		-.415	-1.487	-1.539	-1.626	-1.299	-1.052
60.00	-.414	-1.432	-1.476	-1.528	-1.584	-1.895		-.501	-1.512	-1.546	-1.616	-1.874	-1.044
65.00	-.422	-1.434	-1.484	-1.543	-1.577	-1.998		-.501	-1.512	-1.555	-1.626	-1.795	-1.053
70.00	-.428	-1.436	-1.477	-1.540	-1.588	-1.909		-.512	-1.522	-1.548	-1.623	-1.771	-1.057
75.00	-.417	-1.449	-1.486	-1.538	-1.592	-1.904		-.491	-1.532	-1.560	-1.612	-1.745	-1.057
80.00	-.445	-1.463	-1.485	-1.536	-1.592	-1.886		-.520	-1.548	-1.561	-1.612	-1.711	-1.057
85.00	-.459	-1.454	-1.485	-1.534	-1.495	-1.767		-.545	-1.545	-1.561	-1.612	-1.629	-1.058
90.00	-.343	-1.357	-1.394	-1.353	-1.236	-1.578		-.500	-1.521	-1.546	-1.598	-1.488	-1.020
95.00	-.110	-1.142	-.110	-.098	-.109	-.529		-.267	-1.332	-.369	-.393	-.373	-.950
Lower Surface													
0.00	.565	.566	.535	.555	.585	.474		.667	.660	.629	.627	.636	.526
1.25	.514	.456	.451	.464	.479	.409		.624	.556	.549	.547	.546	.467
2.50	.500	.367	.366	.373	.342	.342		.556	.468	.457	.445	.454	.405
5.00	.394	.317	.306	.305	.317	.268		.487	.403	.395	.388	.395	.330
7.50	.339	.278	.270	.259	.263	.212		.425	.367	.360	.336	.336	.273
10.00	.277	.231	.216	.203	.202	.117		.358	.303	.292	.278	.270	.179
15.00	.224	.213	.162	.146	.150	.032		.296	.277	.239	.218	.215	.088
20.00	.191	.165	.133	.110	.106	.049		.252	.226	.198	.182	.182	.019
25.00	.168	.127	.102	.083	.075	.193		.225	.185	.167	.145	.132	.045
30.00	.096	.093	.073	.046	.035	.118		.145	.148	.129	.109	.091	.069
40.00	.090	.069	.040	.015	.009	.191		.143	.121	.099	.077	.061	.144
45.00	.086	.040	.014	-.017	-.029	.247		.134	.091	.072	.040	.025	.200
50.00	.019	.007	-.019	-.051	-.062	.279		.063	.057	.040	.011	.011	.235
60.00	-.006	-.015	-.040	-.063	-.104	.303		.034	.029	.014	-.011	-.051	.261
65.00	-.017	-.036	-.060	-.089	-.128	.315		.028	.009	-.009	-.037	-.084	.279
70.00	-.033	-.052	-.070	-.113	-.163	.348		.005	-.012	-.023	-.063	-.120	.317
75.00	-.038	-.052	-.079	-.115	-.166	.348		-.002	-.018	-.038	-.072	-.124	.306
80.00	-.095	-.079	-.096	-.139	-.197	.344		-.053	-.047	-.059	-.152	-.216	.316
85.00	-.083	-.075	-.090	-.130	-.196	.351		-.058	-.053	-.053	-.157	-.217	.317
90.00	-.075	-.061	-.084	-.105	-.183	.301		-.068	-.054	-.060	-.166	-.218	.321
95.00	-.047	-.042	-.044	-.077	-.132	.335		-.063	-.060	-.063	-.193	-.215	.283
Lower surface													
0.00	M = 0.94	a = 9.91°		M = 0.94	a = 13.64°								
Upper surface													
0.00	.039	.064	-.125	-.305	-.514	.042		.032	.332	-.596	-.836	-.871	.431
1.25	-.440	-.1375	-.1385	-.1356	-.1367	-.1318		-.685	-.1417	-.1320	-.1150	-.1019	-.841
2.50	-.532	-.167	-.1325	-.1325	-.1325	-.1402		-.801	-.1381	-.1297	-.1125	-.1039	-.828
5.00	-.688	-.1090	-.1274	-.1293	-.1309	-.1377		-.943	-.1328	-.1320	-.1127	-.1033	-.819
7.50	-.650	-.890	-.1204	-.1252	-.1281	-.1347		-.894	-.1266	-.1266	-.1114	-.1020	-.807
10.00	-.611	-.810	-.1175	-.1234	-.1244	-.1326		-.844	-.1213	-.1256	-.1099	-.1046	-.802
15.00	-.513	-.715	-.1108	-.1167	-.1232	-.1296		-.719	-.1132	-.1188	-.1091	-.1028	-.802
20.00	-.460	-.629	-.791	-.1130	-.1204	-.1280		-.643	-.1015	-.1134	-.1086	-.1012	-.796
25.00	-.644	-.541	-.739	-.1114	-.1167	-.1253		-.598	-.088	-.1095	-.1048	-.1022	-.805
30.00	-.508	-.666	-.666	-.1088	-.1154	-.1214		-.618	-.1033	-.1055	-.1034	-.1091	-.825
35.00	-.441	-.496	-.615	-.645	-.654	-.1232		-.551	-.363	-.4038	-.1100	-.0955	-.834
40.00	-.612	-.496	-.660	-.714	-.722	-.1440		-.607	-.576	-.613	-.986	-.091	-.812
45.00	-.479	-.500	-.572	-.814	-.814	-.1110		-.570	-.586	-.598	-.954	-.917	-.823
50.00	-.490	-.509	-.577	-.802	-.810	-.1118		-.589	-.598	-.594	-.924	-.910	-.819
55.00	-.471	-.521	-.594	-.795	-.810	-.1119		-.609	-.616	-.893	-.899	-.897	-.813
60.00	-.547	-.556	-.602	-.776	-.781	-.1112		-.644	-.637	-.827	-.861	-.888	-.813
65.00	-.547	-.561	-.606	-.755	-.755	-.1112		-.661	-.634	-.747	-.845	-.874	-.820
70.00	-.547	-.566	-.606	-.725	-.726	-.1116		-.627	-.640	-.676	-.828	-.863	-.810
75.00	-.535	-.577	-.613	-.706	-.758	-.1137		-.609	-.643	-.632	-.784	-.850	-.800
80.00	-.560	-.597	-.614	-.688	-.789	-.1132		-.632	-.643	-.592	-.759	-.829	-.801
85.00	-.577	-.596	-.616	-.675	-.721	-.1118		-.619	-.614	-.570	-.741	-.802	-.814
90.00	-.561	-.590	-.603	-.658	-.649	-.1113		-.564	-.555	-.540	-.712	-.767	-.804
95.00	-.387	-.489	-.588	-.606	-.592	-.1058		-.386	-.446	-.450	-.684	-.764	-.794
Lower Surface													
0.00	.771	.745	.691	.679	.675	.568		.902	.837	.776	.734	.694	.602
1.25	.743	.647	.630	.617	.607	.518		.909	.769	.735	.705	.682	.550
2.50	.666	.558	.536	.519	.524	.463		.819	.697	.657	.631	.618	.530
5.00	.590	.492	.477	.459	.466	.398		.730	.621	.576	.576	.568	.477
7.50	.522	.454	.436	.422	.411	.342		.656	.574	.560	.536	.517	.430
10.00	.374	.384	.352	.344	.343	.244		.559	.489	.486	.467	.449	.338
15.00	.372	.324	.311	.286	.284	.158		.485	.467	.428	.403	.395	.260
20.00	.330	.298	.267	.246	.239	.088		.436	.407	.378	.359	.350	.192
30.00	.295	.254	.230	.210	.202	.025		.395	.354	.342	.323	.306	.126
35.00	.211	.215	.193	.167	.158	-.006		.309	.318	.301	.279	.260	.094
40.00	.199	.154	.130	.103	.089	-.0432		.311	.280	.269	.241	.229	.028
50.00	.131	.117	.098	.067	.050	-.174		.218	.203	.196	.166	.155	-.068
60.00	.096	.091	.074	.047	.011	-.198		.184	.177	.171	.145	.108	-.090
65.00	.092	.063	.045	.017	-.025	-.222		.181	.149	.139	.117	.071	-.115
70.00	.065	.043	.028	-.010	-.057	-.259		.137	.120	.116	.084	.037	-.139
75.00	.040	.034	.011	-.023	-.064	-.251		.104	.107	.095	.067	.032	-.146
80.00	.022	.007	-.007	-.042	-.089	-.267		.083	.075	.068	.042	.004	-.152
85.00	.002	-.005	-.020	-.049	-.096	-.273		.058	.063	.053	.030	-.012	-.184
90.00	-.022	-.015	-.025	-.057	-.109	-.232		.036	.043	.041	.015	-.027	-.136
95.00	-.035	-.031	-.043	-.065	-.109	-.274		.019	.021	.010	-.003	-.045	-.183
Lower surface													
0.00	-.073	-.065	-.057	-.102	-.127	-.246		-.012	-.023	-.024	-.059	-.085	-.170

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:													
Percent c	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Upper surface								Upper surface					
0.00	.039	-.569	-.790	-1.037	-1.104	-.640		.044	-.744	-.962	-.948	-.821	-.733
1.25	-.819	-1.430	-1.181	-.999	-.843	-.724		-.916	-1.243	-1.007	-.875	-.799	-.723
2.50	-.925	-1.428	-1.161	-.971	-.850	-.718		-1.015	-1.233	-1.007	-.857	-.799	-.719
5.00	-.1049	-1.390	-1.181	-.973	-.849	-.718		-1.162	-1.219	-1.029	-.841	-.792	-.719
7.50	-.1005	-1.347	-1.168	-.95	-.856	-.716		-1.107	-1.180	-1.011	-.839	-.787	-.719
10.00	-.961	-1.297	-1.135	-.972	-.860	-.716		-1.051	-1.183	-1.017	-.839	-.786	-.719
15.00	-.816	-1.240	-1.098	-.972	-.849	-.716		-.744	-1.121	-.949	-.836	-.782	-.719
20.00	-.845	-1.176	-1.064	-.975	-.846	-.713		-.692	-1.058	-.929	-.837	-.777	-.719
25.00	-.642	-1.025	-1.041	-.959	-.852	-.716		-.656	-.973	-.931	-.822	-.775	-.718
30.00	-.655	-.722	-1.002	-.950	-.836	-.720		-.612	-.862	-.928	-.824	-.774	-.716
35.00	-.629	-.635	-.989	-.923	-.819	-.725		-.615	-.769	-.918	-.821	-.771	-.717
40.00	-.636	-.609	-.970	-.886	-.810	-.718		-.600	-.722	-.904	-.812	-.770	-.718
45.00	-.607	-.616	-.956	-.852	-.804	-.724		-.538	-.688	-.887	-.804	-.767	-.719
50.00	-.619	-.624	-.938	-.835	-.803	-.722		-.620	-.681	-.863	-.796	-.765	-.723
55.00	-.632	-.635	-.902	-.826	-.796	-.720		-.657	-.688	-.839	-.778	-.763	-.723
60.00	-.671	-.654	-.863	-.803	-.795	-.719		-.633	-.677	-.817	-.775	-.760	-.723
65.00	-.654	-.641	-.826	-.808	-.792	-.723		-.598	-.672	-.808	-.774	-.757	-.723
70.00	-.627	-.635	-.791	-.807	-.791	-.724		-.584	-.670	-.796	-.768	-.756	-.723
75.00	-.589	-.634	-.756	-.778	-.787	-.715		-.527	-.670	-.786	-.766	-.753	-.723
80.00	-.599	-.632	-.727	-.768	-.782	-.718		-.520	-.652	-.772	-.766	-.743	-.723
85.00	-.589	-.604	-.693	-.757	-.764	-.724		-.460	-.639	-.757	-.760	-.734	-.723
90.00	-.545	-.560	-.659	-.742	-.744	-.717		-.451	-.606	-.728	-.760	-.751	-.723
95.00	-.391	-.471	-.620	-.728	-.757	-.714		-.453	-.606	-.728	-.760	-.751	-.723
Lower surface								Lower surface					
0.00	.957	.880	.803	.748	.699	.609		.986	.907	.815	.750	.683	.612
1.25	.989	.828	.783	.743	.707	.588		1.038	.871	.815	.765	.723	.603
2.50	.988	.828	.783	.743	.707	.588		.955	.907	.782	.734	.695	.551
5.00	.793	.682	.661	.637	.618	.518		.745	.715	.693	.650	.622	.551
7.50	.722	.632	.622	.601	.571	.472		.788	.699	.671	.645	.622	.551
10.00	.624	.570	.549	.533	.509	.392		.691	.630	.608	.580	.560	.435
15.00	.552	.527	.495	.469	.452	.312		.617	.580	.553	.517	.499	.365
20.00	.503	.464	.447	.422	.406	.245		.566	.534	.500	.476	.458	.297
30.00	.458	.422	.406	.386	.367	.187		.524	.478	.460	.438	.415	.230
35.00	.368	.375	.365	.341	.321	.151		.436	.438	.416	.392	.368	.200
40.00	.366	.342	.330	.306	.286	.084		.430	.397	.385	.355	.336	.135
45.00	.345	.307	.294	.266	.251	.026		.403	.364	.338	.316	.297	.076
50.00	.275	.261	.258	.226	.212	-.003		.340	.321	.308	.281	.260	.041
55.00	.237	.231	.230	.206	.170	-.030		.297	.290	.278	.253	.213	.013
60.00	.233	.202	.196	.173	.130	-.057		.292	.258	.244	.220	.178	.013
65.00	.186	.172	.172	.140	.094	-.080		.245	.223	.220	.184	.141	.038
70.00	.149	.154	.151	.120	.086	-.097		.195	.203	.195	.166	.127	.057
75.00	.128	.115	.120	.096	.056	-.107		.175	.163	.159	.137	.096	.074
80.00	.102	.102	.099	.076	.034	-.127		.147	.146	.137	.114	.072	.092
85.00	.066	.076	.082	.058	.012	-.097		.110	.117	.113	.091	.046	.071
90.00	.043	.047	.052	.035	-.008	-.153		.075	.089	.081	.058	.021	.128
95.00	.022	-.001	.005	-.028	-.055	-.144		.045	.029	.030	-.007	-.050	-.131
Upper surface								Upper surface					
0.00	M = 0.94	a = 15.66°						M = 0.94	a = 17.76°				
1.25	.023	-.931	-1.104	-.949	-.848	-.806		-.022	-1.003	-.964	-.936	-.894	-.860
2.50	-.002	-.118	-.979	-.932	-.835	-.778		-.939	-.952	-.945	-.931	-.885	-.832
5.00	-.019	-.110	-.976	-.889	-.834	-.776		-.924	-.953	-.937	-.916	-.893	-.832
7.50	-.066	-.109	-.106	-.872	-.831	-.773		-.924	-.955	-.943	-.906	-.883	-.829
10.00	-.088	-.107	-.997	-.868	-.827	-.774		-.929	-.956	-.931	-.905	-.878	-.829
15.00	-.106	-.109	-.999	-.867	-.825	-.774		-.933	-.955	-.939	-.905	-.874	-.829
20.00	-.960	-.109	-.982	-.863	-.827	-.774		-.939	-.962	-.942	-.897	-.861	-.830
25.00	-.788	-.104	-.961	-.859	-.822	-.773		-.902	-.952	-.937	-.901	-.876	-.828
30.00	-.734	-.105	-.957	-.853	-.818	-.771		-.880	-.949	-.937	-.887	-.876	-.825
35.00	-.673	-.968	-.952	-.849	-.817	-.770		-.784	-.944	-.937	-.894	-.874	-.824
40.00	-.661	-.914	-.945	-.847	-.814	-.772		-.780	-.932	-.937	-.896	-.873	-.829
45.00	-.631	-.868	-.935	-.840	-.815	-.773		-.754	-.925	-.933	-.894	-.873	-.827
50.00	-.649	-.822	-.920	-.838	-.813	-.773		-.735	-.912	-.929	-.892	-.872	-.829
55.00	-.642	-.796	-.903	-.831	-.809	-.774		-.711	-.896	-.928	-.888	-.870	-.831
60.00	-.707	-.779	-.886	-.818	-.810	-.775		-.794	-.891	-.920	-.875	-.861	-.831
65.00	-.651	-.753	-.873	-.817	-.801	-.770		-.778	-.872	-.917	-.875	-.857	-.836
70.00	-.657	-.740	-.859	-.815	-.803	-.774		-.773	-.858	-.912	-.875	-.851	-.830
75.00	-.638	-.731	-.842	-.810	-.803	-.774		-.773	-.840	-.904	-.874	-.850	-.822
80.00	-.674	-.740	-.842	-.810	-.802	-.774		-.783	-.834	-.899	-.875	-.859	-.829
85.00	-.681	-.713	-.834	-.810	-.790	-.770		-.774	-.810	-.890	-.875	-.848	-.825
90.00	-.673	-.704	-.821	-.806	-.782	-.773		-.756	-.800	-.877	-.872	-.838	-.827
95.00	-.583	-.681	-.795	-.806	-.799	-.770		-.660	-.768	-.862	-.871	-.855	-.827
Lower surface								Lower surface					
0.00	.991	.921	.817	.740	.663	.591		.965	.922	.813	.719	.631	.570
1.25	1.073	.914	.835	.773	.724	.599		.938	.848	.773	.721	.586	
2.50	.995	.860	.799	.750	.715	.599		1.017	.892	.828	.770	.731	.601
5.00	.902	.782	.756	.715	.686	.569		.941	.841	.789	.741	.759	.579
7.50	.836	.758	.715	.681	.649	.533		.872	.804	.753	.712	.699	.550
10.00	.743	.686	.653	.626	.591	.463		.781	.733	.697	.658	.628	.486
15.00	.667	.624	.598	.565	.546	.398		.710	.670	.641	.605	.580	.423
20.00	.587	.587	.549	.523	.499	.334		.661	.627	.597	.561	.537	.364
30.00	.574	.536	.507	.483	.457	.271		.614	.580	.551	.523	.494	.301
35.00	.489	.493	.466	.434	.410	.235		.532	.534	.509	.477	.451	.265
40.00	.479	.454	.429	.398	.380	.177		.521	.496	.487	.436	.416	.207
45.00	.453	.414	.390	.362	.341	.113		.494	.455	.429	.401	.381	.144
50.00	.389	.375	.352	.325	.303	.080		.427	.411	.393	.362	.342	.112
55.00	.346	.336	.323	.299	.256	.050		.384	.378	.363	.334	.293	.080
60.00	.331	.305	.285	.262	.217	.023		.367	.342	.324	.296	.254	.048
65.00	.284	.269	.258	.225	.181	.004		.321	.302	.295	.259	.217	.022
70.00	.236	.208	.199	.175	.132	.047		.247	.239	.230	.203	.166	.006
75.00	.202	.183	.169	.147	.103	.049		.206	.209	.195	.171	.134	.053
80.00	.178	.157	.146	.119	.073	.059		.158	.172	.169	.142	.099	.046
85.00	.137	.151	.146	.119	.073	.059		.113	.133	.123	.102	.063	.017
90.00	.099	.114	.105	.088	.041	.014		.113	.133	.123	.102	.063	.017
95.00	.047	.051	.048	.011	-.								

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Percent c	Pressure coefficient at:											
	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2
$M = 0.94 \quad \alpha = 23.90^\circ$												
0.00	-0.090	-1.009	-0.986	-0.964	-0.946	-0.906	-0.312	-1.140	-1.120	-1.100	-1.041	-1.002
1.25	-0.986	-1.994	-0.982	-0.961	-0.939	-0.887	-1.004	-1.123	-1.109	-1.089	-1.050	-0.973
2.50	-0.976	-1.975	-0.973	-0.957	-0.938	-0.883	-1.002	-1.116	-1.102	-1.078	-1.044	-0.971
5.00	-0.978	-1.976	-0.979	-0.953	-0.946	-0.880	-1.091	-1.124	-1.115	-1.070	-1.043	-0.967
7.50	-0.978	-1.979	-0.976	-0.952	-0.930	-0.881	-1.101	-1.119	-1.095	-1.070	-1.037	-0.967
10.00	-0.982	-1.001	-0.971	-0.952	-0.921	-0.883	-1.109	-1.116	-1.103	-1.073	-1.031	-0.966
15.00	-0.980	-1.006	-0.981	-0.950	-0.932	-0.881	-1.094	-1.126	-1.108	-1.068	-1.037	-0.966
20.00	-0.982	-1.999	-0.981	-0.945	-0.931	-0.881	-1.017	-1.126	-1.110	-1.056	-1.041	-0.966
25.00	-0.926	-1.997	-0.981	-0.947	-0.929	-0.879	-0.869	-1.111	-1.101	-1.065	-1.034	-0.960
30.00	-0.892	-1.995	-0.980	-0.945	-0.928	-0.879	-0.843	-1.108	-1.105	-1.056	-1.033	-0.955
35.00	-0.817	-1.990	-0.980	-0.943	-0.928	-0.879	-0.846	-1.091	-1.104	-1.055	-1.031	-0.950
40.00	-0.817	-1.976	-0.978	-0.943	-0.925	-0.882	-0.824	-1.046	-1.105	-1.054	-1.026	-0.960
45.00	-0.786	-1.965	-0.977	-0.941	-0.925	-0.882	-0.797	-0.997	-1.097	-1.050	-1.027	-0.955
50.00	-0.779	-1.946	-0.974	-0.940	-0.924	-0.883	-0.768	-0.928	-1.087	-1.048	-1.023	-0.955
55.00	-0.744	-1.929	-0.971	-0.938	-0.921	-0.885	-0.745	-0.875	-1.081	-1.044	-1.020	-0.957
60.00	-0.819	-1.921	-0.969	-0.920	-0.921	-0.885	-0.741	-0.848	-1.070	-1.027	-1.019	-0.956
65.00	-0.826	-1.897	-0.964	-0.924	-0.918	-0.882	-0.720	-0.798	-1.056	-1.024	-1.012	-0.945
70.00	-0.780	-1.882	-0.960	-0.927	-0.915	-0.883	-0.688	-0.757	-1.043	-1.020	-1.003	-0.946
75.00	-0.777	-1.872	-0.956	-0.923	-0.915	-0.885	-0.669	-0.724	-1.015	-1.023	-0.999	-0.952
80.00	-0.822	-1.870	-0.948	-0.923	-0.913	-0.883	-0.644	-0.704	-0.99	-1.018	-0.996	-0.946
85.00	-0.818	-1.848	-0.938	-0.924	-0.900	-0.879	-0.654	-0.683	-0.963	-1.010	-0.978	-0.935
90.00	-0.805	-1.836	-0.924	-0.922	-0.892	-0.880	-0.644	-0.673	-0.930	-0.99	-0.962	-0.938
95.00	-0.695	-0.812	-0.895	-0.918	-0.910	-0.878	-0.524	-0.623	-0.877	-0.985	-0.971	-0.938
1.25	.934	.926	.806	.700	.603	.554	.913	.925	.794	.680	.571	.528
2.50	1.070	.960	.856	.774	.716	.581	1.071	.978	.867	.766	.706	.566
5.00	1.038	.930	.857	.789	.744	.606	1.061	.960	.874	.802	.756	.604
7.50	.971	.888	.825	.771	.776	.598	1.005	.924	.858	.794	.752	.606
10.00	.914	.847	.794	.750	.712	.575	.950	.890	.831	.777	.734	.588
15.00	.823	.784	.740	.696	.659	.518	.863	.828	.780	.735	.690	.540
20.00	.753	.727	.688	.648	.617	.459	.803	.775	.730	.686	.651	.486
25.00	.706	.678	.641	.604	.578	.405	.758	.729	.691	.646	.613	.434
30.00	.663	.630	.597	.569	.538	.345	.711	.682	.646	.607	.574	.376
35.00	.581	.584	.558	.524	.492	.308	.635	.635	.605	.566	.531	.342
40.00	.566	.543	.518	.480	.461	.247	.618	.596	.568	.527	.501	.286
45.00	.536	.502	.476	.444	.424	.185	.590	.561	.528	.488	.454	.224
50.00	.473	.458	.439	.409	.387	.153	.527	.513	.491	.451	.425	.187
55.00	.432	.422	.409	.377	.338	.120	.484	.475	.456	.421	.378	.154
60.00	.433	.385	.367	.339	.297	.070	.465	.437	.412	.355	.325	.122
65.00	.362	.317	.287	.249	.240	.058	.443	.392	.386	.345	.298	.074
70.00	.307	.317	.299	.276	.241	.028	.356	.371	.352	.317	.280	.061
75.00	.276	.273	.264	.242	.202	.003	.329	.324	.310	.282	.236	.031
80.00	.240	.246	.236	.209	.167	-.024	.288	.295	.278	.247	.202	.003
85.00	.191	.210	.202	.177	.132	-.020	.238	.254	.242	.211	.161	.002
90.00	.137	.164	.152	.132	.088	-.083	.182	.204	.187	.164	.114	-.063
95.00	.054	.087	.086	.046	.021	-.100	.080	.122	.119	.072	.041	-.086

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:													
	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent c	M = 0.98	a = -2.00°					M = 0.98	a = -0.08°					
Upper surface													
0.00	.029	.718	.668	.630	.570	.485	.061	.761	.714	.711	.473	.708	
1.25	.045	.259	.273	.206	.271	.307	.268	.107	.088	.062	.024	.120	
2.50	.038	.179	.175	.186	.101	.181	.205	.040	.020	.009	.011	.055	
5.00	.026	.149	.130	.116	.113	.140	.147	.052	.039	.009	.041	.067	
7.50	.025	.115	.095	.079	.063	.089	.119	.047	.015	.025	.070	.084	
10.00	.019	.089	.063	.056	.035	.046	.091	.033	.006	.045	.069	.101	
15.00	.015	.052	.022	.026	.003	.029	.065	.006	.032	.057	.092	.130	
20.00	.005	.017	.015	.013	.033	.102	.036	.024	.061	.084	.115	.165	
25.00	.037	-.003	-.024	-.048	-.066	.205	-.005	-.035	-.068	-.111	-.131	.242	
30.00	-.005	-.021	-.041	-.063	-.084	.240	-.072	-.057	-.089	-.119	-.139	.242	
35.00	-.030	-.046	-.064	-.082	-.112	.259	-.060	-.084	-.108	-.124	-.164	.240	
40.00	-.052	-.051	-.089	-.120	-.134	.327	-.086	-.101	-.121	-.153	-.184	.292	
45.00	-.061	-.069	-.113	-.143	-.164	.322	-.103	-.103	-.132	-.169	-.207	.281	
50.00	-.049	-.092	-.143	-.169	-.194	.350	-.078	-.106	-.153	-.194	-.231	.304	
55.00	-.072	-.132	-.176	-.199	-.225	.354	-.083	-.141	-.184	-.218	-.259	.316	
60.00	-.143	-.163	-.186	-.216	-.256	.338	-.158	-.176	-.205	-.239	-.275	.303	
65.00	-.147	-.159	-.187	-.227	-.263	.364	-.161	-.176	-.209	-.250	-.280	.330	
70.00	-.160	-.170	-.198	-.228	-.292	.366	-.178	-.183	-.216	-.258	-.306	.334	
75.00	-.166	-.181	-.211	-.232	-.307	.357	-.183	-.193	-.223	-.259	-.321	.325	
80.00	-.186	-.200	-.211	-.241	-.315	.346	-.198	-.214	-.226	-.254	-.323	.315	
85.00	-.209	-.190	-.211	-.245	-.307	.321	-.225	-.208	-.226	-.253	-.304	.295	
90.00	-.177	-.182	-.196	-.240	-.283	.301	-.195	-.203	-.217	-.253	-.275	.277	
95.00	-.147	-.178	-.195	-.230	-.277	.309	-.145	-.188	-.204	-.239	-.272	.285	
Lower surface													
1.25	.091	-.206	-.377	-.682	-.859	-.915	.235	.090	.019	.033	-.078	-.138	
2.50	.029	.167	.225	.554	.732	.844	.171	.042	-.002	.056	-.105	-.122	
5.00	.006	-.094	-.179	.241	.434	.766	.137	.055	.005	.034	-.073	-.127	
7.50	-.016	-.108	-.184	.253	.268	.693	.104	.026	-.019	.060	-.077	-.136	
10.00	-.054	-.118	-.183	.262	.294	.601	.070	.008	-.040	.075	-.089	-.132	
15.00	-.070	-.120	-.181	.243	.289	.397	.041	-.005	-.042	.085	-.101	-.146	
20.00	-.099	-.120	-.187	.263	.309	.377	.001	-.019	-.067	.116	-.126	-.193	
25.00	-.124	-.130	-.178	.242	.288	.377	-.017	-.019	-.075	.111	-.134	.231	
30.00	-.107	-.142	-.190	.250	.293	.316	-.006	-.045	-.089	.115	-.142	.244	
35.00	-.126	-.179	-.217	.277	.313	.291	-.036	-.085	-.096	.139	-.169	.218	
40.00	-.182	-.186	-.226	.288	.320	.329	-.082	-.086	-.100	.157	-.179	.259	
45.00	-.151	-.190	-.236	.300	.341	.361	-.051	-.095	-.133	.194	-.207	.289	
50.00	-.200	-.224	-.268	.326	.360	.385	-.112	-.129	-.167	.223	-.235	.311	
55.00	-.220	-.245	-.284	.339	.381	.401	-.131	-.152	-.180	.233	-.271	.329	
60.00	-.253	-.272	-.303	.360	.399	.407	-.166	-.182	-.208	.253	-.291	.334	
65.00	-.268	-.279	-.316	.377	.422	.411	-.175	-.192	-.217	.275	-.308	.340	
70.00	-.275	-.267	-.314	.365	.414	.405	-.183	-.200	-.217	.265	-.307	.340	
75.00	-.324	-.271	-.312	.375	.440	.390	-.238	-.213	-.223	.270	-.303	.325	
80.00	-.328	-.323	-.330	.382	.405	.384	-.240	-.233	-.244	.280	-.328	.334	
85.00	-.342	-.326	-.331	.349	.398	.337	-.255	-.234	-.244	.271	-.332	.277	
90.00	-.319	-.321	-.331	.354	.382	.376	-.234	-.239	-.244	.269	-.317	.312	
95.00	-.225	-.274	-.293	.313	.334	.343	-.170	-.211	-.232	.277	-.289	.273	
Upper surface							M = 0.98	a = 1.96°					
0.00	.064	.713	.606	.616	.600	.680	.069	.610	.488	.465	.438	.643	
1.25	.150	-.133	-.260	.614	-.701	-.584	.021	-.779	-.887	-.952	-.982	-.782	
2.50	.087	-.145	-.224	.372	-.612	-.764	-.041	-.386	-.795	-.861	-.904	-.998	
5.00	.010	-.107	-.170	.246	-.342	-.699	-.162	-.303	-.641	-.772	-.830	-.942	
7.50	-.009	-.077	-.160	.248	-.284	-.637	-.158	-.206	-.226	-.733	-.794	-.885	
10.00	-.027	-.081	-.165	.245	-.275	-.589	-.153	-.186	-.240	-.694	-.754	-.848	
15.00	-.022	-.086	-.175	.220	-.279	-.430	-.110	-.181	-.246	-.302	-.378	-.630	
20.00	-.024	-.119	-.185	.240	-.285	-.333	-.099	-.201	-.271	-.307	-.388	-.808	
25.00	-.086	-.115	-.187	.237	-.274	-.347	-.168	-.195	-.255	-.307	-.427	-.792	
30.00	-.165	-.139	-.199	.247	-.280	-.292	-.246	-.211	-.262	-.311	-.341	-.740	
35.00	-.133	-.166	-.218	.263	-.297	-.275	-.207	-.238	-.276	-.319	-.353	-.666	
40.00	-.163	-.174	-.235	.290	-.313	-.328	-.233	-.248	-.297	-.346	-.369	-.700	
45.00	-.181	-.187	-.250	.298	-.331	-.329	-.258	-.261	-.318	-.359	-.390	-.656	
50.00	-.160	-.187	-.256	.318	-.352	-.354	-.247	-.251	-.340	-.374	-.406	-.646	
55.00	-.143	-.184	-.248	.331	-.372	-.368	-.240	-.252	-.347	-.386	-.438	-.600	
60.00	-.124	-.188	-.297	.339	-.387	-.353	-.294	-.312	-.347	-.399	-.455	-.485	
65.00	-.230	-.248	-.300	.350	-.374	-.351	-.302	-.314	-.347	-.406	-.451	-.419	
70.00	-.245	-.250	-.303	.352	-.352	-.388	-.311	-.315	-.353	-.407	-.462	-.388	
75.00	-.245	-.264	-.312	.355	-.391	-.383	-.311	-.324	-.353	-.407	-.465	-.384	
80.00	-.269	-.282	-.316	.350	-.371	-.368	-.336	-.342	-.361	-.404	-.463	-.381	
85.00	-.295	-.282	-.316	.350	-.348	-.349	-.335	-.342	-.361	-.404	-.418	-.383	
90.00	-.266	-.280	-.305	.338	-.317	-.330	-.335	-.342	-.350	-.393	-.362	-.384	
95.00	-.181	-.249	-.287	.290	-.300	-.335	-.237	-.312	-.341	-.363	-.338	-.401	
Lower surface													
1.25	.351	.306	.267	.284	.337	.261	.469	.459	.445	.463	.504	.411	
2.50	.297	.218	.202	.213	.241	.204	.416	.357	.359	.375	.393	.341	
5.00	.253	.184	.149	.150	.163	.153	.364	.298	.295	.289	.300	.280	
7.50	.217	.139	.104	.113	.126	.102	.314	.246	.238	.234	.247	.215	
10.00	.176	.112	.074	.067	.086	.066	.269	.210	.202	.194	.196	.168	
15.00	.136	.086	.045	.036	.036	.000	.221	.176	.170	.153	.141	.085	
20.00	.098	.055	.017	.010	-.001	-.080	.174	.176	.128	.093	.104	.002	
25.00	.076	.044	.009	.028	-.027	-.154	.150	.131	.095	.065	.064	-.031	
30.00	.067	.021	-.011	.045	-.051	-.201	.133	.049	.070	.033	.032	.331	
35.00	.025	-.005	-.040	.078	-.079	-.16	.075	.063	.081	.010	.001	-.156	
40.00	.004	-.020	-.058	.100	-.098	-.260	.061	.040	.015	.018	.025	-.201	
45.00	.010	-.001	-.136	.136	-.133	-.000	.063	.011	-.019	-.053	-.055	-.258	
50.00	-.052	-.076	-.122	-.165	-.159	-.321	-.005	-.019	-.044	-.081	-.090	-.286	
55.00	-.074	-.098	-.142	-.166	-.159	-.324	-.026	-.047	-.066	-.093	-.129	-.312	
60.00	-.108	-.124	-.166	-.169	-.224	-.327	-.052	-.068	-.085	-.117	-.155	-.325	
65.00	-.115	-.137	-.172	-.221	-.252	-.325	-.060	-.080	-.094	-.135	-.183	-.340	
70.00	-.117	-.126	-.175	-.210	-.253	-.329	-.066	-.079	-.099	-.136	-.187	-.343	
75.00	-.179	-.162	-.191	-.228	-.277	-.321	-.130	-.116	-.127	-.157	-.214	-.343	
80.00	-.179	-.178	-.207	-.240	-.293	-.327	-.135	-.127	-.139	-.180	-.232	-.348	
85.00	-.195	-.178	-.207	-.244	-.308	-.275	-.149	-.127	-.137	-.185	-.249	-.297	
90.00	-.172	-.181	-.207	-.247	-.300	-.314	-.132	-.132	-.141	-.185	-.249	-.345	
95.00	-.130	-.159	-.198	-.259	-.277	-.273	-.108	-.122	-.137	-.198	-.239		

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:														
Percent		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
M = 0.98 $\alpha = 5.93^\circ$														
Upper surface														
0.00		+0.71	+472	+267	+208	+536		+0.75	+319	+162	+057	+059	+377	
1.25	-1.22	-1.010	-1.097	-1.142	-1.144	-1.944		-1.243	-1.171	-1.234	-1.269	-1.276	-1.100	
2.50	-1.188	-1.007	-0.992	-1.058	-1.079	-1.158		-1.320	-1.084	-1.132	-1.193	-1.223	-1.281	
5.00	-1.333	-1.638	-1.919	-1.979	-1.010	-1.105		-1.473	-1.813	-1.063	-1.118	-1.154	-1.227	
7.50	-1.316	-1.331	-1.848	-1.931	-1.962	-1.034		-1.445	-1.547	-1.993	-1.076	-1.101	-1.169	
10.00	-1.298	-1.312	-1.795	-1.902	-1.936	-1.008		-1.416	-1.463	-1.964	-1.034	-1.081	-1.139	
15.00	-1.216	-1.286	-1.383	-1.821	-1.908	-1.978		-1.325	-1.405	-1.877	-1.964	-1.043	-1.106	
20.00	-1.197	-1.285	-1.349	-1.788	-1.870	-1.950		-1.296	-1.376	-1.534	-1.931	-1.002	-1.082	
25.00	-1.257	-1.280	-1.340	-1.661	-1.827	-1.938		-1.327	-1.363	-1.452	-1.811	-1.961	-1.062	
30.00	-1.322	-1.291	-1.345	-1.459	-1.808	-1.897		-1.381	-1.397	-1.420	-1.883	-1.946	-1.102	
35.00	-1.281	-1.309	-1.358	-1.415	-1.804	-1.819		-1.356	-1.384	-1.420	-1.739	-1.935	-1.047	
45.00	-1.317	-1.324	-1.375	-1.423	-1.774	-1.839		-1.384	-1.393	-1.435	-1.613	-1.929	-1.054	
48.00	-1.324	-1.328	-1.384	-1.423	-1.800	-1.826		-1.384	-1.399	-1.449	-1.675	-1.928	-1.021	
55.00	-1.310	-1.330	-1.371	-1.441	-1.848	-1.809		-1.375	-1.403	-1.463	-1.558	-1.923	-1.030	
60.00	-1.328	-1.350	-1.371	-1.461	-1.823	-1.808		-1.345	-1.419	-1.474	-1.547	-1.917	-1.030	
65.00	-1.362	-1.377	-1.424	-1.468	-1.819	-1.793		-1.429	-1.444	-1.484	-1.540	-1.839	-1.023	
70.00	-1.368	-1.382	-1.422	-1.481	-1.806	-1.796		-1.432	-1.447	-1.483	-1.546	-1.717	-1.029	
75.00	-1.373	-1.381	-1.426	-1.482	-1.816	-1.800		-1.436	-1.451	-1.490	-1.545	-1.683	-1.034	
80.00	-1.364	-1.390	-1.433	-1.482	-1.821	-1.807		-1.416	-1.458	-1.497	-1.545	-1.644	-1.037	
85.00	-1.396	-1.408	-1.433	-1.482	-1.827	-1.801		-1.453	-1.477	-1.497	-1.545	-1.644	-1.037	
90.00	-1.417	-1.408	-1.435	-1.482	-1.809	-1.783		-1.473	-1.477	-1.499	-1.547	-1.599	-1.036	
95.00	-1.398	-1.410	-1.425	-1.476	-1.850	-1.787		-1.456	-1.477	-1.488	-1.540	-1.510	-1.040	
	-1.313	-1.384	-1.422	-1.455	-1.803	-1.773		-1.373	-1.454	-1.488	-1.524	-1.414	-1.050	
M = 0.98 $\alpha = 7.92^\circ$														
Upper surface														
0.00	+583	+589	+557	+571	+600	+501		+692	+683	+642	+642	+657	+554	
1.25	+539	+482	+473	+482	+497	+431		+652	+583	+567	+568	+571	+492	
5.00	+480	+406	+389	+390	+403	+372		+586	+493	+474	+465	+475	+425	
10.00	+420	+347	+330	+326	+344	+303		+514	+411	+419	+404	+414	+365	
15.00	+367	+313	+292	+284	+289	+250		+459	+398	+362	+363	+371	+311	
20.00	+255	+245	+245	+230	+235	+230		+391	+337	+321	+327	+329	+237	
25.00	+223	+196	+197	+172	+181	+174		+332	+310	+263	+243	+249	+134	
30.00	+199	+160	+129	+109	+108	+059		+293	+260	+226	+203	+204	+059	
35.00	+126	+127	+097	+072	+070	+070		+263	+222	+197	+173	+170	+003	
40.00	+121	+105	+071	+043	+043	+144		+184	+186	+164	+133	+127	+020	
45.00	+117	+072	+039	+012	+010	+201		+174	+124	+097	+070	+064	+155	
50.00	+050	+039	+008	+020	+024	+235		+105	+090	+070	+038	+029	+189	
55.00	+026	+011	+011	+039	+065	+260		+074	+063	+049	+020	+013	+217	
60.00	+010	+009	+035	+063	+094	+273		+066	+041	+019	+007	+042	+237	
65.00	+007	+024	+047	+084	+126	+301		+047	+023	+004	+032	+078	+274	
70.00	+016	+027	+059	+091	+129	+308		+039	+017	+009	+043	+085	+274	
75.00	+079	+062	+087	+125	+166	+310		+017	+015	+034	+069	+118	+276	
80.00	+082	+073	+095	+137	+182	+318		+027	+024	+042	+078	+130	+290	
85.00	+096	+076	+094	+137	+200	+272		+037	+031	+040	+079	+140	+248	
90.00	+083	+077	+097	+135	+194	+323		+037	+039	+046	+074	+132	+297	
95.00	+088	+085	+097	+144	+183	+290		+059	+055	+058	+097	+129	+262	
M = 0.98 $\alpha = 9.91^\circ$														
Upper surface														
0.00	+0.70	+1.47	+0.27	+1.95	+1.372	+1.154		+0.40	+2.29	+4.81	+7.06	+8.80	+4.02	
1.25	-1.357	-1.255	-1.287	-1.304	-1.311	-1.194		-1.584	-1.288	-1.257	-1.241	-1.278	-1.282	
2.50	-1.447	-1.179	-1.210	-1.266	-1.280	-1.320		-1.691	-1.254	-1.232	-1.242	-1.273	-1.319	
5.00	-1.601	-1.989	-1.158	-1.193	-1.224	-1.278		-1.828	-1.187	-1.267	-1.239	-1.277	-1.311	
7.50	-1.566	-1.760	-1.088	-1.149	-1.173	-1.244		-1.787	-1.142	-1.201	-1.235	-1.247	-1.305	
10.00	-1.531	-1.679	-1.066	-1.120	-1.152	-1.217		-1.745	-1.098	-1.171	-1.217	-1.234	-1.292	
15.00	-1.440	-1.592	-1.007	-1.056	-1.122	-1.183		-1.634	-1.008	-1.089	-1.170	-1.222	-1.277	
20.00	-1.391	-1.540	-1.028	-1.026	-1.092	-1.161		-1.559	-0.923	-1.024	-1.123	-1.193	-1.260	
25.00	-1.394	-1.484	-1.045	-1.009	-1.053	-1.142		-1.516	-0.651	-0.982	-1.097	-1.165	-1.245	
30.00	-1.440	-1.444	-1.058	-1.084	-1.038	-1.112		-1.546	-0.448	-0.942	-1.061	-1.140	-1.232	
35.00	-1.420	-1.442	-1.053	-1.066	-1.026	-1.024		-1.520	-0.505	-0.924	-1.030	-1.110	-1.174	
40.00	-1.446	-1.440	-1.053	-1.026	-1.016	-1.030		-1.540	-0.526	-0.906	-0.999	-1.141	-1.160	
45.00	-1.420	-1.442	-1.051	-1.074	-1.016	-1.093		-1.513	-0.532	-0.887	-0.981	-1.082	-1.141	
50.00	-1.434	-1.449	-1.059	-1.021	-1.012	-1.013		-1.540	-0.543	-0.861	-0.969	-1.061	-1.132	
55.00	-1.448	-1.469	-1.052	-1.008	-1.007	-1.007		-1.523	-0.553	-0.840	-0.948	-1.048	-1.117	
60.00	-1.490	-1.494	-1.054	-1.076	-1.080	-1.011		-1.596	-0.600	-1.716	-1.935	-1.968	-1.088	
65.00	-1.506	-1.538	-1.065	-1.082	-1.016	-1.016		-1.588	-0.608	-1.655	-1.931	-1.920	-1.064	
70.00	-1.475	-1.516	-1.049	-1.029	-1.029	-1.025		-1.586	-0.619	-1.616	-1.916	-1.873	-1.045	
75.00	-1.510	-1.536	-1.051	-1.029	-1.028	-1.025		-1.619	-0.641	-1.602	-1.895	-1.825	-1.032	
80.00	-1.526	-1.537	-1.054	-1.029	-1.028	-1.025		-1.625	-0.647	-1.604	-1.878	-1.775	-1.046	
85.00	-1.526	-1.537	-1.054	-1.029	-1.028	-1.025		-1.619	-0.644	-1.604	-1.757	-1.723	-1.069	
90.00	-1.514	-1.537	-1.054	-1.029	-1.028	-1.025		-1.534	-0.602	-1.535	-1.767	-1.711	-1.076	
95.00	-1.516	-1.520	-1.057	-1.029	-1.028	-1.025		-1.532	-0.625	-1.535	-1.766	-1.711	-1.076	
M = 0.98 $\alpha = 13.68^\circ$														
Upper surface														
0.00	+785	+761	+712	+702	+699	+599		+929	+874	+805	+768	+726	+639	
1.25	+759	+668	+645	+637	+632	+547		+939	+808	+766	+734	+712	+605	
5.00	+686	+580	+568	+542	+547	+491		+858	+724	+689	+666	+652	+572	
7.50	+611	+514	+501	+483	+490	+428		+768	+654	+631	+611	+600	+521	
10.00	+546	+478	+459	+436	+440	+379		+694	+614	+590	+566	+550	+475	
15.00	+468	+411	+388	+382	+375	+283		+604	+538	+520	+506	+49	+394	
20.00	+402	+378	+342	+312	+320	+201		+530	+504	+472	+442	+432	+307	
30.00	+359	+324	+296	+277	+271	+129		+416	+410	+379	+364	+346	+170	
35.00	+325	+281	+265	+247	+235	+164		+441	+392	+379	+364	+340	+139	
40.00	+245	+245	+226	+205	+192	+193		+352	+356	+340	+321	+303	+139	
45.00	+220	+183	+160	+132	+129	+109		+352	+325	+308	+286	+271	+076	
50.00</td														

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:													
	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent	c	M = 0.98	a = 15.84°				M = 0.98	a = 17.97°					
Upper surface													
0.00	.024	-.474	-.696	-.943	-1.065	-.716	.011	-.660	-.872	-1.078	-1.163	-.904	
1.25	-.712	-.1346	-.1283	-.1231	-.1123	-.1011	-.839	-.1326	-.1276	-.1133	-.1031	-.914	
2.50	-.823	-.1345	-.1263	-.1228	-.1128	-.1004	-.949	-.1306	-.1254	-.1122	-.1031	-.909	
5.00	-.946	-.1292	-.1293	-.1224	-.1124	-.1000	-.1045	-.1300	-.1275	-.1114	-.1038	-.904	
7.50	-.906	-.1253	-.1266	-.1224	-.1115	-.0994	-.1012	-.1291	-.1245	-.1114	-.1041	-.903	
10.00	-.866	-.1203	-.1266	-.1231	-.1123	-.0994	-.979	-.1266	-.1264	-.1114	-.1049	-.902	
12.50	-.744	-.1152	-.1207	-.1222	-.1120	-.0994	-.833	-.1223	-.1251	-.1109	-.1066	-.901	
20.00	-.632	-.1051	-.1160	-.1199	-.1110	-.0994	-.691	-.1184	-.1229	-.1091	-.1075	-.897	
25.00	-.589	-.901	-.1121	-.1189	-.1105	-.0994	-.660	-.1117	-.1200	-.1087	-.1072	-.894	
30.00	-.604	-.527	-.1085	-.1164	-.1094	-.0995	-.643	-.674	-.1188	-.1065	-.1056	-.892	
35.00	-.580	-.559	-.1069	-.1148	-.1081	-.0997	-.636	-.618	-.1177	-.1049	-.1047	-.888	
40.00	-.593	-.571	-.1056	-.1132	-.1067	-.0996	-.646	-.618	-.1167	-.1031	-.1037	-.890	
45.00	-.571	-.591	-.1044	-.1117	-.1056	-.0990	-.617	-.630	-.1156	-.1000	-.1033	-.886	
50.00	-.595	-.601	-.1035	-.1102	-.1040	-.0983	-.640	-.650	-.1144	-.979	-.1020	-.883	
55.00	-.626	-.629	-.1007	-.1083	-.1020	-.0971	-.657	-.671	-.1118	-.964	-.1006	-.881	
60.00	-.658	-.653	-.949	-.1045	-.1002	-.963	-.700	-.699	-.1033	-.948	-.996	-.877	
65.00	-.663	-.663	-.836	-.1028	-.981	-.956	-.701	-.710	-.891	-.943	-.975	-.871	
70.00	-.645	-.686	-.1009	-.966	-.950	-.673	-.721	-.780	-.934	-.957	-.872		
75.00	-.633	-.692	-.1024	-.948	-.949	-.657	-.708	-.723	-.922	-.950	-.871		
80.00	-.779	-.698	-.1003	-.942	-.932	-.670	-.684	-.713	-.918	-.929	-.886		
85.00	-.674	-.696	-.1617	-.911	-.898	-.952	-.675	-.660	-.707	-.914	-.904	-.885	
90.00	-.661	-.688	-.596	-.867	-.864	-.958	-.604	-.656	-.707	-.901	-.880	-.869	
95.00	-.568	-.584	-.571	-.821	-.869	-.954	-.512	-.611	-.707	-.890	-.894	-.866	
1.25	.977	.906	.828	.775	.719	.635	1.015	.936	.846	.778	.715	.641	
2.50	1.010	.859	.806	.767	.732	.618	1.073	.909	.843	.796	.756	.636	
5.00	.919	.780	.741	.712	.689	.597	.981	.841	.793	.758	.732	.627	
7.50	.830	.716	.688	.662	.647	.553	.887	.784	.743	.716	.698	.591	
10.00	.754	.671	.650	.624	.602	.512	.819	.739	.703	.680	.660	.553	
15.00	.663	.601	.579	.563	.540	.427	.725	.669	.636	.614	.593	.477	
20.00	.589	.567	.525	.496	.484	.351	.652	.617	.583	.557	.542	.407	
25.00	.542	.502	.475	.455	.443	.290	.601	.572	.536	.513	.499	.343	
30.00	.493	.457	.435	.420	.401	.225	.557	.523	.495	.473	.458	.274	
40.00	.407	.413	.396	.375	.358	.192	.468	.476	.456	.431	.411	.244	
45.00	.407	.379	.362	.338	.325	.128	.464	.442	.420	.393	.383	.180	
50.00	.384	.341	.327	.298	.289	.064	.440	.407	.383	.355	.343	.118	
55.00	.322	.306	.291	.263	.253	.032	.380	.365	.349	.319	.308	.085	
60.00	.281	.271	.263	.243	.209	-.002	.338	.331	.321	.300	.263	.055	
65.00	.276	.244	.230	.209	.173	-.027	.330	.299	.284	.268	.226	.029	
70.00	.232	.210	.208	.181	.137	-.054	.284	.267	.260	.237	.195	.004	
75.00	.194	.198	.194	.162	.106	-.16	.241	.232	.230	.217	.183	.137	
80.00	.173	.165	.159	.138	.101	-.085	.222	.215	.207	.187	.147	.033	
85.00	.150	.140	.140	.120	.080	-.101	.188	.191	.183	.164	.125	.053	
90.00	.117	.126	.125	.101	.056	-.071	.154	.165	.166	.144	.099	.037	
95.00	.095	.100	.097	.080	.041	-.123	.118	.135	.131	.115	.076	.084	
	.062	.056	.057	.023	-.001	-.110	.075	.084	.083	.051	.029	.084	
Lower surface													
0.00	M = 0.98	a = 20.13°					M = 0.98	a = 22.24°					
1.25	-.027	-.850	-.1047	-.1159	-.1047	-.931	-.104	-.987	-.1141	-.1055	-.988	-.974	
2.50	-.971	-.1333	-.1288	-.1106	-.1004	-.908	-.1052	-.1265	-.1190	-.1043	-.982	-.945	
5.00	-.1072	-.1315	-.1265	-.1108	-.1004	-.908	-.1133	-.1236	-.1195	-.1044	-.977	-.945	
7.50	-.1143	-.1314	-.1288	-.1102	-.1003	-.907	-.1182	-.1232	-.1195	-.1034	-.980	-.941	
10.00	-.1107	-.1309	-.1259	-.1101	-.1096	-.908	-.1159	-.1229	-.1168	-.1036	-.975	-.943	
15.00	-.1070	-.1299	-.1281	-.1099	-.997	-.908	-.1136	-.1223	-.1172	-.1039	-.972	-.942	
20.00	-.922	-.1274	-.1281	-.1089	-.999	-.909	-.991	-.1234	-.1173	-.1035	-.983	-.941	
25.00	-.752	-.1238	-.1270	-.1075	-.1000	-.908	-.786	-.1206	-.1168	-.1020	-.993	-.941	
30.00	-.709	-.1227	-.1231	-.1075	-.993	-.907	-.739	-.1189	-.1128	-.1031	-.989	-.937	
35.00	-.700	-.922	-.1212	-.1062	-.990	-.906	-.724	-.1176	-.1128	-.1021	-.992	-.930	
40.00	-.686	-.738	-.1181	-.1060	-.986	-.904	-.688	-.891	-.1122	-.1019	-.989	-.927	
45.00	-.705	-.699	-.1153	-.1048	-.987	-.907	-.694	-.1122	-.1021	-.984	-.935		
46.75	-.675	-.695	-.1104	-.1034	-.974	-.905	-.659	-.794	-.1044	-.1021	-.987	-.928	
50.00	-.673	-.681	-.1080	-.1026	-.974	-.904	-.659	-.805	-.1045	-.1021	-.987	-.929	
55.00	-.678	-.667	-.1055	-.1014	-.967	-.906	-.681	-.815	-.1077	-.1023	-.980	-.932	
60.00	-.678	-.666	-.1035	-.995	-.965	-.906	-.760	-.835	-.1063	-.1008	-.978	-.931	
65.00	-.672	-.708	-.1009	-.991	-.958	-.902	-.786	-.838	-.1046	-.1002	-.973	-.920	
70.00	-.645	.728	-.986	-.987	-.948	-.903	-.751	-.824	-.1030	-.998	-.963	-.923	
75.00	-.635	.746	-.952	-.981	-.946	-.906	-.756	-.822	-.1007	-.1000	-.956	-.929	
80.00	-.703	.777	-.916	-.978	-.942	-.904	-.817	-.827	-.991	-.996	-.951	-.924	
85.00	-.721	.782	-.888	-.977	-.924	-.900	-.790	-.814	-.992	-.993	-.919	-.915	
90.00	-.729	.782	-.857	-.967	-.909	-.902	-.780	-.805	-.954	-.979	-.919	-.921	
95.00	-.704	.769	-.836	-.961	-.930	-.902	-.717	-.790	-.935	-.972	-.936	-.921	
1.25	1.021	.947	.846	.764	.687	.621	1.002	.957	.844	.749	.667	.604	
2.50	1.101	.942	.865	.802	.754	.630	1.106	.971	.882	.804	.755	.625	
5.00	1.025	.888	.827	.780	.748	.633	1.053	.932	.861	.804	.769	.639	
7.50	.939	.832	.785	.746	.722	.606	.977	.884	.826	.773	.805	.625	
10.00	.870	.793	.747	.715	.688	.572	.913	.840	.791	.752	.747	.597	
15.00	.779	.722	.688	.658	.629	.504	.824	.774	.734	.704	.671	.534	
20.00	.712	.656	.633	.602	.583	.439	.756	.714	.681	.647	.626	.475	
25.00	.655	.622	.586	.561	.542	.379	.705	.669	.633	.602	.586	.418	
30.00	.610	.575	.540	.524	.499	.316	.662	.623	.592	.568	.543	.356	
35.00	.530	.531	.501	.478	.455	.280	.584	.555	.522	.503	.480	.319	
40.00	.522	.492	.466	.443	.426	.222	.571	.544	.518	.489	.471	.263	
45.00	.496	.457	.429	.403	.378	.159	.542	.508	.478	.451	.434	.201	
50.00	.428	.390	.353	.343	.305	.093	.484	.455	.441	.409	.398	.170	
55.00	.371	.346	.320	.306	.266	.066	.438	.427	.410	.386	.350	.137	
60.00	.382	.346	.319	.306	.261	.040	.425	.396	.372	.350	.311	.108	
65.00	.332	.309	.300	.270	.231	.040	.377	.359	.343	.314	.275	.081	
70.00	.283	.292	.273	.253	.219	.014	.323	.336	.316	.291	.243	.050	
75.00	.262	.253	.241	.223	.182	-.005	.299	.297	.282	.258	.226	.030	
80.00	.230	.230	.218	.195	.156	-.028	.263	.268	.251	.231	.194	.005	
85.00	.185	.201	.192	.172	.127	-.016	.218	.236	.226	.203	.163	.011	
90.00	.146	.16											

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:														
	Percent	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
	c	M = 0.98	a = 24.37°						M = 0.98	a = 26.48°				
Upper surface	0.00	-1.159	-1.095	-1.225	-1.100	-1.072	-1.001		-1.227	-1.164	-1.189	-1.132	-1.107	-1.058
	1.25	-1.131	-1.226	-1.171	-1.090	-1.055	-0.974		-1.169	-1.195	-1.167	-1.123	-1.095	-1.031
	2.50	-1.169	-1.208	-1.153	-1.089	-1.053	-0.973		-1.171	-1.184	-1.152	-1.122	-1.091	-1.030
	5.00	-1.256	-1.204	-1.170	-1.082	-1.050	-0.970		-1.214	-1.185	-1.169	-1.115	-1.089	-1.026
	7.50	-1.233	-1.205	-1.146	-1.082	-1.044	-0.970		-1.206	-1.181	-1.146	-1.115	-1.082	-1.015
	10.00	-1.210	-1.202	-1.157	-1.082	-1.042	-0.968		-1.177	-1.170	-1.147	-1.115	-1.078	-1.024
	15.00	-1.074	-1.207	-1.159	-1.074	-1.045	-0.968		-1.132	-1.149	-1.141	-1.111	-1.084	-1.026
	20.00	-0.887	-1.196	-1.152	-1.067	-1.045	-0.958		-0.954	-1.165	-1.163	-1.099	-1.089	-1.025
	25.00	-0.818	-1.187	-1.141	-1.072	-1.040	-0.953		-0.914	-1.173	-1.150	-1.109	-1.081	-1.020
	30.00	-0.810	-1.177	-1.131	-1.065	-1.037	-0.961		-0.860	-1.161	-1.155	-1.099	-1.081	-1.015
	35.00	-0.779	-1.126	-1.133	-1.065	-1.034	-0.959		-0.865	-1.140	-1.152	-1.099	-1.077	-1.011
	40.00	-0.777	-1.045	-1.140	-1.065	-1.028	-0.960		-0.849	-1.080	-1.154	-1.098	-1.073	-1.017
	45.00	-0.743	-0.974	-1.127	-1.064	-1.025	-0.957		-0.838	-1.015	-1.148	-1.095	-1.073	-1.013
	50.00	-0.750	-0.923	-1.113	-1.061	-1.021	-0.955		-0.829	-0.971	-1.134	-1.092	-1.068	-1.011
	55.00	-0.740	-0.891	-1.103	-1.054	-1.017	-0.955		-0.808	-0.936	-1.130	-1.088	-1.067	-1.011
	60.00	-0.805	-0.885	-1.095	-1.032	-1.014	-0.952		-0.850	-0.935	-1.126	-1.063	-1.065	-1.008
	65.00	-0.826	-0.869	-1.085	-1.032	-1.007	-0.945		-0.864	-0.919	-1.117	-1.065	-1.059	-1.000
	70.00	-0.786	-0.857	-1.079	-1.031	-1.001	-0.947		-0.826	-0.899	-1.111	-1.064	-1.052	-1.000
	75.00	-0.783	-0.852	-1.059	-1.025	-0.997	-0.947		-0.828	-0.886	-1.095	-1.064	-1.047	-1.005
	80.00	-0.843	-0.857	-1.049	-1.022	-0.991	-0.944		-0.854	-0.889	-1.086	-1.064	-1.042	-1.000
	85.00	-0.832	-0.854	-1.033	-1.022	-0.973	-0.940		-0.862	-0.886	-1.067	-1.063	-1.021	-0.992
	90.00	-0.824	-0.860	-1.011	-1.014	-0.956	-0.941		-0.868	-0.899	-1.046	-1.052	-1.003	-0.993
	95.00	-0.794	-0.845	-0.993	-1.002	-0.976	-0.938		-0.820	-0.884	-1.025	-1.029	-1.017	-0.994
Lower Surface	1.25	.968	.956	.839	.738	.639	.592		.932	.956	.828	.715	.608	.566
	2.50	1.100	.954	.894	.811	.751	.622		1.090	1.167	.895	.803	.739	.604
	5.00	1.070	.965	.890	.815	.735	.649		1.084	.990	.907	.840	.781	.643
	7.50	1.007	.919	.864	.712	.824	.642		1.031	.957	.889	.831	.789	.646
	10.00	.948	.834	.834	.790	.752	.622		.979	.926	.869	.816	.772	.632
	15.00	.863	.821	.783	.740	.705	.569		.897	.862	.818	.775	.733	.583
	20.00	.796	.766	.729	.692	.664	.511		.834	.813	.769	.729	.695	.532
	25.00	.749	.718	.686	.651	.625	.455		.789	.765	.727	.688	.656	.483
	30.00	.708	.673	.643	.614	.586	.398		.746	.720	.686	.656	.617	.428
	35.00	.632	.633	.602	.571	.542	.364		.673	.678	.646	.613	.577	.393
	40.00	.615	.589	.568	.535	.513	.307		.655	.639	.609	.576	.547	.335
	45.00	.587	.554	.530	.495	.478	.245		.629	.600	.573	.536	.511	.277
	50.00	.526	.513	.491	.460	.439	.213		.567	.555	.534	.498	.476	.243
	55.00	.482	.474	.460	.430	.396	.179		.527	.520	.503	.471	.428	.210
	60.00	.460	.439	.424	.393	.354	.147		.503	.483	.463	.435	.388	.178
	65.00	.416	.402	.389	.357	.320	.120		.456	.443	.432	.396	.353	.149
	70.00	.361	.376	.363	.333	.302	.088		.399	.417	.400	.372	.336	.114
	75.00	.336	.334	.325	.296	.263	.063		.366	.371	.359	.339	.294	.087
	80.00	.297	.304	.293	.268	.232	.038		.332	.339	.327	.302	.257	.058
	85.00	.252	.266	.264	.237	.196	.041		.280	.302	.294	.270	.219	.059
	90.00	.206	.224	.216	.196	.158	.017		.228	.252	.243	.225	.178	.003
	95.00	.119	.157	.154	.116	.091	.034		.131	.180	.176	.135	.107	.021

TABLE I - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:												
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent C	Upper surface	M = 1.00	a = -2.00°					M = 1.00	a = -0.04°					
		.074	.758	.708	.675	.616	.539	.067	.768	.722	.687	.724		
Lower surface	Upper surface	1.25	.374	.297	.322	.328	.306	.343	.260	.388	.379	.315	.322	.103
		2.50	.325	.220	.229	.220	.221	.217	.205	.492	.433	.013	.058	.002
		5.00	.273	.192	.179	.170	.150	.184	.151	.441	.3	.022	.068	.089
		7.50	.242	.162	.147	.131	.106	.130	.126	.441	.315	.015	.054	.099
		10.00	.211	.139	.114	.106	.076	.091	.100	.032	.008	.051	.094	.116
		15.00	.168	.107	.080	.070	.044	.014	.072	.014	.029	.059	.105	.140
		20.00	.104	.068	.048	.041	.034	.004	.044	.016	.055	.087	.113	.165
		25.00	.093	.057	.029	.011	-.017	-.151	.005	.030	.045	.100	.130	.232
		30.00	.058	.041	.019	-.010	-.030	-.182	-.055	.045	.086	.118	.138	.236
		35.00	.030	.012	-.008	-.030	-.060	-.204	-.045	.074	.102	.123	.164	.233
		40.00	.006	.003	-.030	-.066	-.083	-.265	-.072	.089	.113	.154	.184	.285
		45.00	-.001	-.013	-.051	-.087	-.112	-.262	-.087	.097	.126	.165	.202	.272
		50.00	.009	-.034	-.081	-.110	-.144	-.286	-.063	.097	.148	.189	.230	.295
		55.00	-.029	-.072	-.113	-.140	-.171	-.294	-.088	.133	.178	.211	.251	.306
		60.00	-.083	-.103	-.128	-.156	-.199	-.283	-.144	.169	.198	.228	.270	.293
		65.00	-.086	-.103	-.136	-.171	-.205	-.306	-.149	.169	.207	.250	.275	.322
		70.00	-.101	-.113	-.136	-.176	-.238	-.311	-.168	.178	.207	.259	.302	.326
		75.00	-.106	-.125	-.154	-.176	-.250	-.298	-.169	.192	.222	.255	.317	.317
		80.00	-.129	-.148	-.154	-.182	-.261	-.291	-.190	.211	.222	.251	.317	.305
		85.00	-.155	-.136	-.154	-.189	-.254	-.272	-.220	.203	.225	.248	.297	.287
		90.00	-.125	-.131	-.143	-.188	-.233	-.254	-.188	.200	.213	.248	.268	.269
		95.00	-.100	-.131	-.143	-.181	-.243	-.264	-.139	.189	.205	.233	.268	.276
Lower surface	Lower surface	1.25	.146	.129	-.301	-.567	-.707	-.765	.251	.127	.069	.031	.033	-.033
		2.50	.091	.102	-.154	-.423	-.588	-.709	.199	.057	.011	.008	.011	.035
		5.00	.066	.033	-.104	-.162	-.320	-.636	.164	.077	.036	.008	.026	.052
		7.50	.048	.044	-.113	-.174	-.204	-.569	.136	.053	.015	.039	.074	
		10.00	.012	.052	-.109	-.183	-.224	-.467	.102	.034	.001	.044	.054	-.084
		15.00	-.002	.052	-.111	-.167	-.220	-.315	.072	.020	.014	.054	.074	.112
		20.00	-.031	.053	-.115	-.187	-.241	-.310	.043	.004	.040	.077	.100	.164
		25.00	-.049	.062	-.106	-.168	-.221	-.310	.020	.003	.047	.080	.108	.213
		30.00	-.036	.072	-.120	-.177	-.227	-.257	.025	.023	.064	.098	.120	.227
		35.00	-.054	.110	-.149	-.204	-.246	-.233	-.011	.057	.075	.115	.149	.199
		40.00	-.107	.121	-.154	-.215	-.253	-.269	-.047	.058	.091	.137	.160	.243
		45.00	-.077	.118	-.167	-.227	-.272	-.299	-.023	.072	.118	.167	.187	.276
		50.00	-.125	-.155	-.198	-.251	-.287	-.322	-.082	.107	.153	.196	.214	.296
		55.00	-.150	-.176	-.212	-.266	-.314	-.341	-.104	.128	.172	.207	.248	.313
		60.00	-.180	-.202	-.233	-.288	-.334	-.364	-.138	.156	.189	.229	.269	.318
		65.00	-.193	-.211	-.244	-.305	-.354	-.344	-.147	.165	.199	.248	.291	.322
		70.00	-.200	-.201	-.244	-.292	-.347	-.340	-.155	.158	.199	.235	.287	.322
		75.00	-.253	-.234	-.253	-.306	-.358	-.327	-.210	.194	.205	.246	.308	
		80.00	-.257	-.254	-.264	-.314	-.342	-.338	-.215	.215	.217	.256	.314	.320
		85.00	-.271	-.262	-.266	-.305	-.341	-.308	-.228	.218	.222	.248	.318	.262
		90.00	-.258	-.266	-.271	-.293	-.327	-.319	-.214	.221	.222	.248	.303	.296
		95.00	-.179	-.232	-.253	-.278	-.291	-.288	-.157	.201	.206	.261	.285	.256
Lower surface	Lower surface	M = 1.00	a = 1.90°					M = 1.00	a = 3.93°					
		0.00	.093	.734	.646	.653	.630	.713	.089	.623	.482	.463	.668	
		1.25	.179	.097	-.183	-.572	-.678	-.536	.050	.784	.899	.973	.994	.746
		2.50	.118	.109	-.168	-.293	-.589	-.723	-.008	.417	.784	.871	.923	.981
		5.00	.054	.072	-.105	-.206	-.287	-.656	.121	.305	.639	.795	.848	.919
		7.50	.036	.043	-.100	-.196	-.254	-.584	.120	.176	.205	.741	.797	.858
		10.00	.017	.040	-.107	-.189	-.264	-.518	.118	.162	.215	.699	.785	.821
		15.00	.020	.043	-.112	-.159	-.249	-.352	-.072	.146	.208	.288	.745	.810
		20.00	.015	.073	-.122	-.183	-.242	-.293	-.065	.161	.232	.290	.684	.780
		25.00	-.047	.068	-.124	-.174	-.227	-.311	-.128	.156	.216	.270	.417	.779
		30.00	-.116	.092	-.138	-.188	-.233	-.256	-.197	.176	.222	.277	.310	.735
		35.00	-.089	.120	-.156	-.251	-.248	-.258	-.158	.197	.237	.284	.322	.669
		40.00	-.115	.126	-.171	-.227	-.268	-.292	-.191	.206	.258	.311	.340	.682
		45.00	-.136	.142	-.187	-.238	-.288	-.328	-.208	.218	.269	.322	.356	.647
		50.00	-.115	.143	-.194	-.250	-.307	-.321	-.191	.218	.279	.339	.380	.637
		55.00	-.126	.173	-.218	-.264	-.329	-.331	-.198	.242	.293	.355	.401	.572
		60.00	-.180	.204	-.232	-.275	-.337	-.314	-.251	.271	.309	.362	.419	.451
		65.00	-.185	.204	-.247	-.292	-.331	-.344	-.257	.272	.318	.373	.417	.405
		70.00	-.203	.208	-.241	-.292	-.344	-.344	-.268	.277	.312	.375	.428	.367
		75.00	-.229	.251	-.293	-.347	-.340	-.340	-.265	.285	.325	.374	.431	.393
		80.00	-.229	.252	-.294	-.330	-.325	-.306	-.290	.304	.345	.376	.431	.393
		85.00	-.257	.238	-.254	-.289	-.307	-.306	-.316	.306	.325	.371	.386	.365
		90.00	-.227	.237	-.246	-.276	-.281	-.289	-.296	.306	.316	.361	.335	.360
		95.00	-.151	.215	-.237	-.242	-.265	-.294	-.207	.279	.310	.333	.312	.373
Lower surface	Lower surface	1.25	.377	.340	.318	.330	.371	.293	.492	.502	.482	.499	.531	.438
		2.50	.329	.249	.248	.260	.278	.234	.451	.394	.401	.409	.425	.373
		5.00	.289	.216	.201	.204	.194	.189	.408	.337	.331	.321	.329	.313
		7.50	.253	.179	.161	.161	.160	.135	.359	.286	.265	.275	.246	
		10.00	.213	.153	.131	.124	.122	.100	.314	.253	.241	.230	.226	.201
		15.00	.176	.127	.102	.091	.073	.038	.265	.218	.205	.189	.170	.118
		20.00	.141	.099	.069	.047	.035	.043	.223	.216	.183	.134	.132	.037
		25.00	.120	.086	.061	.026	.006	.022	.195	.172	.132	.102	.095	.045
		30.00	.110	.062	.045	.012	-.012	-.166	.178	.134	.110	.080	.064	.094
		35.00	.066	.037	.020	-.020	-.049	-.158	.114	.102	.077	.045	.029	.125
		40.00	.042	.025	-.001	-.043	-.064	-.218	.105	.085	.054	.017	.006	.163
		45.00	.051	.001	-.032	-.078	-.095	-.257	.105	.058	.020	.017	.026	.218
		50.00	-.012	.032	.062	-.103	-.120	-.277	.039	.022	.010	.042	.053	.248
		55.00	-.034	-.055	-.082	-.120	-.157	-.290	.013	-.004	-.028	-.057	-.099	.272
		60.00	-.064	-.080	-.109	-.140	-.184	-.290	-.008	-.023	-.048	-.080	-.124	.288
		65.00	-.074	-.089	-.112	-.159	-.214	-.291	-.018	-.037	-.059	-.101	-.153	.304

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:											
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Upper surface	Percent C	M = 1.00	a = 5.90°					M = 1.00	a = 7.90°				
	0.00	.088	.504	.308	.253	.577	.062	.339	.191	.086	.036	.400	
	1.25	-.073	-.976	-1.062	-1.117	-1.137	-.897	-.210	-.149	-.197	-1.229	-1.253	
	2.50	-.139	-.886	-.943	-1.022	-1.073	-1.127	-.287	-.070	-.109	-1.168	-1.256	
	5.00	-.272	-.588	-.868	-.939	-.988	-1.062	-.436	-.798	-.019	-.078	-1.137	
	7.50	-.256	-.282	-.808	-.885	-.930	-.996	-.407	-.536	-.957	-.028	-1.076	
	10.00	-.240	-.265	-.761	-.853	-.917	-.963	-.377	-.444	-.928	-.995	-1.064	
	15.00	-.161	-.237	-.318	-.785	-.878	-.935	-.285	-.373	-.851	-.925	-1.019	
	20.00	-.144	-.237	-.297	-.760	-.839	-.907	-.255	-.346	-.849	-.897	-1.072	
	25.00	-.202	-.231	-.292	-.596	-.798	-.894	-.287	-.331	-.812	-.866	-1.034	
Lower surface	30.00	-.262	-.243	-.291	-.408	-.778	-.864	-.243	-.331	-.771	-.846	-1.047	
	35.00	-.229	-.266	-.304	-.367	-.757	-.789	-.313	-.340	-.379	-.907	-1.022	
	40.00	-.263	-.247	-.325	-.394	-.739	-.811	-.347	-.357	-.393	-.581	-1.024	
	45.00	-.272	-.284	-.346	-.373	-.618	-.769	-.336	-.363	-.403	-.519	-1.095	
	50.00	-.254	-.284	-.347	-.391	-.505	-.772	-.336	-.366	-.410	-.519	-1.093	
	55.00	-.264	-.307	-.358	-.410	-.482	-.772	-.346	-.385	-.428	-.511	-1.088	
	60.00	-.315	-.332	-.370	-.416	-.477	-.760	-.392	-.410	-.437	-.499	-1.027	
	65.00	-.320	-.335	-.377	-.431	-.465	-.772	-.398	-.414	-.445	-.506	-1.028	
	70.00	-.324	-.335	-.375	-.431	-.477	-.776	-.402	-.419	-.441	-.506	-1.029	
	75.00	-.311	-.347	-.384	-.430	-.482	-.773	-.381	-.427	-.455	-.496	-1.044	
Upper surface	80.00	-.347	-.367	-.385	-.434	-.487	-.770	-.420	-.445	-.453	-.498	-1.018	
	85.00	-.372	-.367	-.387	-.430	-.469	-.767	-.444	-.442	-.454	-.500	-1.073	
	90.00	-.353	-.367	-.376	-.422	-.411	-.760	-.424	-.444	-.444	-.495	-1.014	
	95.00	-.271	-.350	-.376	-.405	-.370	-.742	-.344	-.428	-.444	-.476	-1.029	
	1.25	.611	.617	.589	.603	.625	.520	.713	.713	.677	.673	.679	
	2.50	.570	.509	.508	.515	.526	.457	.680	.607	.603	.597	.516	
	5.00	.516	.438	.425	.422	.425	.394	.618	.525	.514	.503	.457	
	7.50	.460	.379	.362	.368	.328	.351	.551	.464	.453	.446	.389	
	10.00	.406	.346	.331	.322	.315	.277	.492	.422	.401	.390	.334	
	15.00	.347	.298	.282	.269	.258	.186	.426	.368	.356	.347	.325	
Lower surface	20.00	.276	.235	.212	.208	.205	.106	.326	.342	.326	.293	.210	
	25.00	.261	.230	.194	.176	.159	.029	.224	.291	.246	.228	.090	
	30.00	.239	.194	.172	.152	.134	.028	.296	.250	.231	.198	.028	
	35.00	.161	.161	.138	.113	.097	.036	.212	.215	.202	.173	.009	
	40.00	.161	.137	.111	.084	.072	.109	.215	.189	.172	.145	.063	
	45.00	.158	.107	.078	.052	.038	.149	.207	.159	.140	.111	.095	
	50.00	.092	.073	.049	.024	.006	.197	.137	.121	.107	.061	.154	
	55.00	.060	.045	.030	.006	.035	.127	.104	.094	.088	.065	.017	
	60.00	.047	.026	.005	.017	.062	.242	.103	.075	.063	.035	.020	
	65.00	.028	.008	.010	.040	.093	.267	.073	.053	.047	.011	.045	
Upper surface	70.00	.028	.005	.019	.044	.098	.277	.059	.046	.033	.001	.052	
	75.00	-.036	-.033	-.047	-.075	-.132	-.278	-.036	-.014	-.006	-.031	-.089	
	80.00	-.044	-.041	-.057	-.091	-.153	-.286	-.008	-.007	-.001	-.034	-.099	
	85.00	-.053	-.044	-.056	-.091	-.166	-.238	-.006	-.002	-.000	-.035	-.113	
	90.00	-.048	-.047	-.061	-.089	-.163	-.288	-.008	-.004	-.006	-.035	-.104	
	95.00	-.048	-.053	-.059	-.102	-.154	-.257	-.020	-.020	-.015	-.053	-.102	
	1.25	.179	.099	.153	.328	.191	.029	.191	.431	.652	.623	.356	
	2.50	-.321	-.212	-.125	-.126	-.143	-.143	.528	-.212	-.190	-.111	-.132	
	5.00	-.407	-.132	-.161	-.126	-.149	-.142	.645	-.182	-.170	-.159	-.166	
	7.50	-.559	-.140	-.141	-.153	-.191	-.141	.713	-.136	-.138	-.166	-.120	
Lower surface	10.00	-.424	-.723	-.104	-.147	-.147	-.104	.723	-.080	-.137	-.161	-.177	
	15.00	-.489	-.643	-.104	-.170	-.120	-.175	.695	-.128	-.109	-.149	-.160	
	20.00	-.391	-.550	-.195	-.106	-.105	-.185	.574	-.949	-.029	-.105	-.152	
	25.00	-.338	-.496	-.675	-.982	-.1049	-.1116	.499	-.864	-.968	-.1062	-.132	
	30.00	-.353	-.440	-.604	-.960	-.1006	-.1103	.480	-.603	-.923	-.1038	-.108	
	35.00	-.401	-.400	-.549	-.943	-.993	-.1074	.504	-.402	-.889	-.1002	-.1084	
	40.00	-.373	-.397	-.489	-.922	-.985	-.192	.473	-.450	-.870	-.978	-.1063	
	45.00	-.405	-.398	-.456	-.788	-.976	-.988	.492	-.475	-.852	-.946	-.1043	
	50.00	-.387	-.402	-.458	-.692	-.973	-.961	.485	-.497	-.834	-.924	-.1035	
	55.00	-.392	-.408	-.468	-.676	-.970	-.973	.504	-.503	-.808	-.914	-.1081	
Upper surface	60.00	-.410	-.428	-.481	-.670	-.969	-.972	.521	-.523	-.777	-.902	-.1098	
	65.00	-.450	-.455	-.491	-.649	-.967	-.965	.547	-.546	-.734	-.882	-.1064	
	70.00	-.454	-.459	-.489	-.636	-.949	-.972	.550	-.557	-.674	-.877	-.1043	
	75.00	-.460	-.465	-.495	-.617	-.862	-.977	.552	-.562	-.616	-.876	-.1022	
	80.00	-.439	-.476	-.507	-.596	-.772	-.985	.545	-.577	-.577	-.863	-.1007	
	85.00	-.474	-.494	-.510	-.583	-.702	-.985	.579	-.590	-.563	-.848	-.781	
	90.00	-.492	-.494	-.512	-.571	-.619	-.986	.589	-.595	-.568	-.834	-.726	
	95.00	-.482	-.497	-.503	-.555	-.555	-.993	.583	-.595	-.562	-.714	-.677	
	1.25	.799	.786	.736	.724	.719	.617	.944	.890	.824	.785	.657	
Lower surface	2.50	.774	.691	.672	.658	.657	.566	.927	.823	.784	.758	.624	
	5.00	.745	.608	.597	.571	.570	.516	.874	.740	.685	.670	.589	
	7.50	.630	.540	.525	.504	.512	.453	.767	.671	.653	.631	.535	
	10.00	.570	.487	.468	.459	.459	.396	.714	.632	.617	.593	.574	
	15.00	.492	.440	.422	.406	.397	.305	.625	.567	.544	.529	.510	
	20.00	.426	.405	.367	.340	.345	.229	.555	.527	.488	.464	.456	
	25.00	.382	.352	.327	.302	.300	.158	.500	.469	.444	.423	.411	
	30.00	.349	.312	.290	.271	.264	.088	.465	.425	.405	.386	.368	
	35.00	.263	.273	.254	.233	.221	.071	.374	.385	.368	.345	.324	
	40.00	.266	.244	.226	.197	.192	.003	.380	.353	.335	.311	.297	
Upper surface	45.00	.255	.212	.190	.166	.159	.062	.363	.310	.300	.277	.261	
	50.00	.183	.175	.162	.134	.123	.098	.290	.281	.270	.241	.227	
	55.00	.151	.147	.134	.114	.083	.125	.255	.251	.242	.222	.183	
	60.00	.150	.124	.111	.086	.045	.146	.255	.221	.211	.191	.145	
	65.00	.119	.102	.093	.061	.013	.184	.214	.194	.192	.159	.112	
	70.00	.091	.093	.076	.047	.007	.179	.175	.182	.174	.146	.110	
	75.00	.073	.063	.055	.025	.002	.195	.160	.151	.147	.125	.078	
	80.00	.057	.056	.049	.015	.032	.207	.140	.138	.134	.110	.065	
	85.00	.040	.049	.043	.015	.040	.160	.108	.123	.126	.100	.047	
	90.00	.029	.036	.034	.011	.037	.206	.087	.101	.099	.085	.041	
Lower surface	95.00	.014	.009	.015	.019	.048	.176	.067	.062	.069	.036	.007	

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

		Pressure coefficient at:												
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent	c	M = 1.00	a = 15.83°					M = 1.00	a = 18.03°					
Upper surface	0.00	-0.054	-0.423	-0.645	-0.888	-1.008	-1.663	-0.072	-0.613	-0.826	-1.042	-1.124	-0.879	
	1.25	-0.657	-1.280	-1.231	-1.171	-1.089	-0.983	-0.787	-1.299	-1.254	-1.111	-1.012	-0.905	
	2.50	-0.778	-1.271	-1.202	-1.172	-1.088	-0.979	-0.908	-1.287	-1.225	-1.105	-1.013	-0.902	
	5.00	-0.898	-1.232	-1.228	-1.172	-1.087	-0.969	-1.006	-1.275	-1.252	-1.095	-1.019	-0.895	
	7.50	-0.861	-1.186	-1.204	-1.172	-1.078	-0.964	-0.974	-1.263	-1.225	-1.096	-1.020	-0.896	
	10.00	-0.823	-1.145	-1.203	-1.181	-1.080	-0.964	-0.942	-1.236	-1.246	-1.094	-1.029	-0.895	
	15.00	-0.691	-1.079	-1.149	-1.170	-1.078	-0.964	-0.802	-1.185	-1.224	-1.087	-1.043	-0.892	
	20.00	-0.597	-1.039	-1.102	-1.145	-1.072	-0.964	-0.655	-1.138	-1.195	-1.075	-1.052	-0.890	
	25.00	-0.547	-0.851	-1.064	-1.135	-1.064	-0.963	-0.617	-1.085	-1.165	-1.070	-1.047	-0.885	
	30.00	-0.566	-0.477	-1.028	-1.113	-1.057	-0.966	-0.608	-0.634	-1.146	-1.056	-1.037	-0.882	
Lower surface	35.00	-0.539	-0.515	-1.012	-1.094	-1.047	-0.963	-0.599	-0.586	-1.133	-1.042	-1.026	-0.877	
	40.00	-0.546	-0.537	-0.998	-1.077	-1.033	-0.962	-0.615	-0.593	-1.120	-1.027	-1.017	-0.882	
	45.00	-0.542	-0.548	-0.991	-1.063	-1.024	-0.957	-0.596	-0.608	-1.110	-1.006	-1.012	-0.876	
	50.00	-0.572	-0.562	-0.981	-1.049	-1.018	-0.951	-0.618	-0.620	-1.106	-0.989	-1.000	-0.873	
	55.00	-0.593	-0.587	-0.956	-1.030	-0.977	-0.942	-0.645	-0.642	-1.091	-0.974	-0.988	-0.873	
	60.00	-0.609	-0.608	-0.904	-1.002	-0.977	-0.930	-0.665	-0.664	-1.047	-0.953	-0.975	-0.869	
	65.00	-0.617	-0.625	-0.857	-0.970	-0.940	-0.916	-0.673	-0.673	-0.932	-0.94	-0.953	-0.861	
	70.00	-0.604	-0.625	-0.857	-0.970	-0.940	-0.916	-0.673	-0.673	-0.932	-0.94	-0.953	-0.861	
	75.00	-0.593	-0.633	-0.582	-0.939	-0.921	-0.918	-0.637	-0.686	-0.901	-0.915	-0.922	-0.860	
	80.00	-0.641	-0.652	-0.572	-0.903	-0.901	-0.918	-0.682	-0.681	-0.887	-0.897	-0.905	-0.859	
Upper surface	85.00	-0.645	-0.649	-0.587	-0.875	-0.868	-0.921	-0.676	-0.643	-0.817	-0.896	-0.881	-0.856	
	90.00	-0.626	-0.645	-0.578	-0.820	-0.835	-0.926	-0.635	-0.619	-0.835	-0.881	-0.853	-0.859	
	95.00	-0.553	-0.552	-0.571	-0.765	-0.836	-0.924	-0.466	-0.557	-0.655	-0.871	-0.864	-0.859	
Lower surface	1.25	1.001	.927	.848	.791	.738	.659	1.027	.949	.859	.791	.731	.658	
	2.50	1.034	.875	.826	.783	.750	.640	1.082	.923	.858	.806	.771	.654	
	5.00	.948	.808	.763	.726	.705	.619	.991	.858	.805	.766	.744	.644	
	7.50	.848	.735	.708	.679	.665	.577	.903	.796	.758	.721	.713	.610	
	10.00	.780	.693	.672	.643	.622	.534	.830	.751	.718	.689	.674	.570	
	15.00	.684	.625	.603	.579	.560	.453	.741	.681	.657	.626	.610	.497	
	20.00	.614	.590	.546	.519	.507	.383	.666	.629	.598	.569	.558	.427	
	25.00	.567	.529	.502	.474	.462	.312	.619	.586	.553	.525	.517	.364	
	30.00	.523	.481	.460	.439	.421	.254	.575	.540	.514	.489	.475	.299	
	35.00	.433	.442	.418	.397	.377	.221	.488	.493	.473	.444	.432	.267	
Upper surface	40.00	.412	.407	.381	.348	.344	.154	.483	.458	.439	.410	.402	.203	
	45.00	.371	.350	.322	.300	.077		.462	.422	.402	.371	.365	.140	
	50.00	.347	.322	.314	.291	.275		.392	.382	.366	.356	.348	.098	
	55.00	.303	.299	.292	.247	.229		.354	.351	.349	.312	.384		
	60.00	.306	.274	.256	.234	.196		.348	.319	.306	.278	.247	.052	
	65.00	.259	.246	.233	.204	.161		.302	.288	.278	.246	.214	.028	
	70.00	.216	.230	.214	.187	.155		.255	.272	.255	.230	.204		
	75.00	.198	.201	.184	.159	.128		.237	.234	.226	.201	.172		
	80.00	.174	.180	.165	.142	.107		.209	.214	.205	.181	.148		
	85.00	.144	.155	.154	.130	.084		.169	.190	.186	.161	.124		
Lower surface	90.00	.118	.130	.126	.109	.068		.139	.160	.154	.134	.099		
	95.00	.081	.087	.088	.053	.033		.095	.109	.109	.071	.055		
Upper surface	1.25	M = 1.00	a = 20.15°					M = 1.00	a = 22.28°					
	0.00	-0.121	-0.786	-0.980	-1.113	-1.091	-0.909	-0.211	-0.935	-1.112	-1.084	-0.988	-0.932	
	1.25	-0.902	-1.289	-1.248	-1.080	-0.989	-0.880	-1.009	-1.284	-1.233	-1.062	-0.983	-0.915	
	2.50	-1.011	-1.274	-1.214	-1.083	-0.991	-0.878	-1.102	-1.267	-1.214	-1.063	-0.979	-0.916	
	5.00	-1.086	-1.273	-1.239	-1.081	-0.995	-0.874	-1.158	-1.264	-1.238	-1.058	-1.014	-0.914	
	7.50	-1.053	-1.270	-1.204	-1.081	-0.995	-0.875	-1.128	-1.261	-1.202	-1.024	-0.972	-0.914	
	10.00	-0.919	-1.228	-1.238	-1.080	-0.995	-0.875	-1.097	-1.255	-1.217	-1.056	-0.973	-0.915	
	15.00	-0.872	-1.222	-1.202	-1.073	-1.004	-0.875	-0.953	-1.241	-1.209	-1.051	-0.976	-0.916	
	20.00	-0.746	-1.177	-1.220	-1.058	-1.006	-0.873	-0.755	-1.216	-1.195	-1.044	-0.976	-0.916	
	25.00	-0.657	-1.182	-1.194	-1.051	-0.995	-0.870	-0.705	-1.211	-1.167	-1.050	-0.974	-0.914	
Upper surface	30.00	-0.642	-0.877	-1.178	-1.044	-0.992	-0.868	-0.689	-1.018	-1.148	-1.042	-0.971	-0.914	
	35.00	-0.635	-0.683	-1.163	-1.031	-0.987	-0.866	-0.678	-0.803	-1.129	-1.039	-0.969	-0.913	
	40.00	-0.652	-0.650	-1.161	-1.017	-0.979	-0.868	-0.686	-0.703	-1.111	-1.039	-0.964	-0.915	
	45.00	-0.626	-0.654	-1.129	-0.999	-0.975	-0.865	-0.647	-0.682	-1.093	-1.036	-0.964	-0.914	
	50.00	-0.635	-0.664	-1.099	-0.983	-0.967	-0.864	-0.639	-0.693	-1.073	-1.035	-0.959	-0.915	
	55.00	-0.643	-0.680	-1.046	-0.969	-0.960	-0.865	-0.628	-0.724	-1.058	-1.031	-0.957	-0.915	
	60.00	-0.688	-0.707	-0.997	-0.947	-0.954	-0.864	-0.673	-0.763	-1.042	-1.006	-0.956	-0.909	
	65.00	-0.705	-0.712	-0.962	-0.944	-0.942	-0.859	-0.700	-0.778	-1.024	-1.006	-0.952	-0.911	
	70.00	-0.675	-0.698	-0.931	-0.942	-0.929	-0.860	-0.703	-0.789	-1.008	-1.003	-0.948	-0.914	
	75.00	-0.668	-0.677	-0.891	-0.931	-0.923	-0.861	-0.718	-0.797	-0.988	-0.994	-0.944	-0.911	
Lower surface	80.00	-0.685	-0.687	-0.849	-0.929	-0.916	-0.860	-0.786	-0.807	-0.968	-0.992	-0.942	-0.908	
	85.00	-0.643	-0.697	-0.818	-0.929	-0.896	-0.858	-0.776	-0.800	-0.944	-0.991	-0.924	-0.910	
	90.00	-0.625	-0.703	-0.780	-0.917	-0.877	-0.858	-0.765	-0.791	-0.918	-0.983	-0.908	-0.910	
	95.00	-0.638	-0.707	-0.754	-0.907	-0.898	-0.858	-0.728	-0.778	-0.898	-0.971	-0.929	-0.910	
Upper surface	1.25	1.037	.971	.868	.786	.710	.645	1.020	.973	.862	.767	.685	.629	
	2.50	1.114	.963	.822	.776	.655	.577	1.119	.987	.896	.822	.774	.648	
	5.00	1.038	.909	.801	.769	.658	.546	1.065	.944	.879	.821	.787	.665	
	7.50	.934	.854	.808	.742	.682	.581	0.990	.895	.844	.792	.829	.648	
	10.00	.814	.771	.738	.708	.600	.529	.839	.790	.754	.714	.689	.561	
	20.00	.729	.683	.657	.628	.609	.469	.773	.728	.701	.662	.645	.501	
	25.00	.676	.642	.614	.587	.567	.408	.723	.688	.656	.619	.605	.446	
	30.00	.633	.601	.571	.550	.525	.348	.678	.647	.612	.584	.564	.384	
	35.00	.551	.556	.532	.506	.483	.310	.603	.602	.572	.541	.522	.351	
	40.00	.543	.521	.497	.470	.453	.255	.588	.566	.538	.504	.493	.291	
Lower surface	45.00	.519	.485	.460	.431	.415	.192	.562	.526	.500	.465	.445	.230	
	50.00	.454	.444	.425	.395	.381	.161	.500	.485	.462	.428	.419	.198	
	55.00	.413	.409	.396	.369	.334	.130	.457	.451	.432	.406	.374	.164	
	60.00	.404	.377	.360	.335	.296	.103	.445	.416	.395	.370	.337	.136	
	65.00	.357	.34											

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

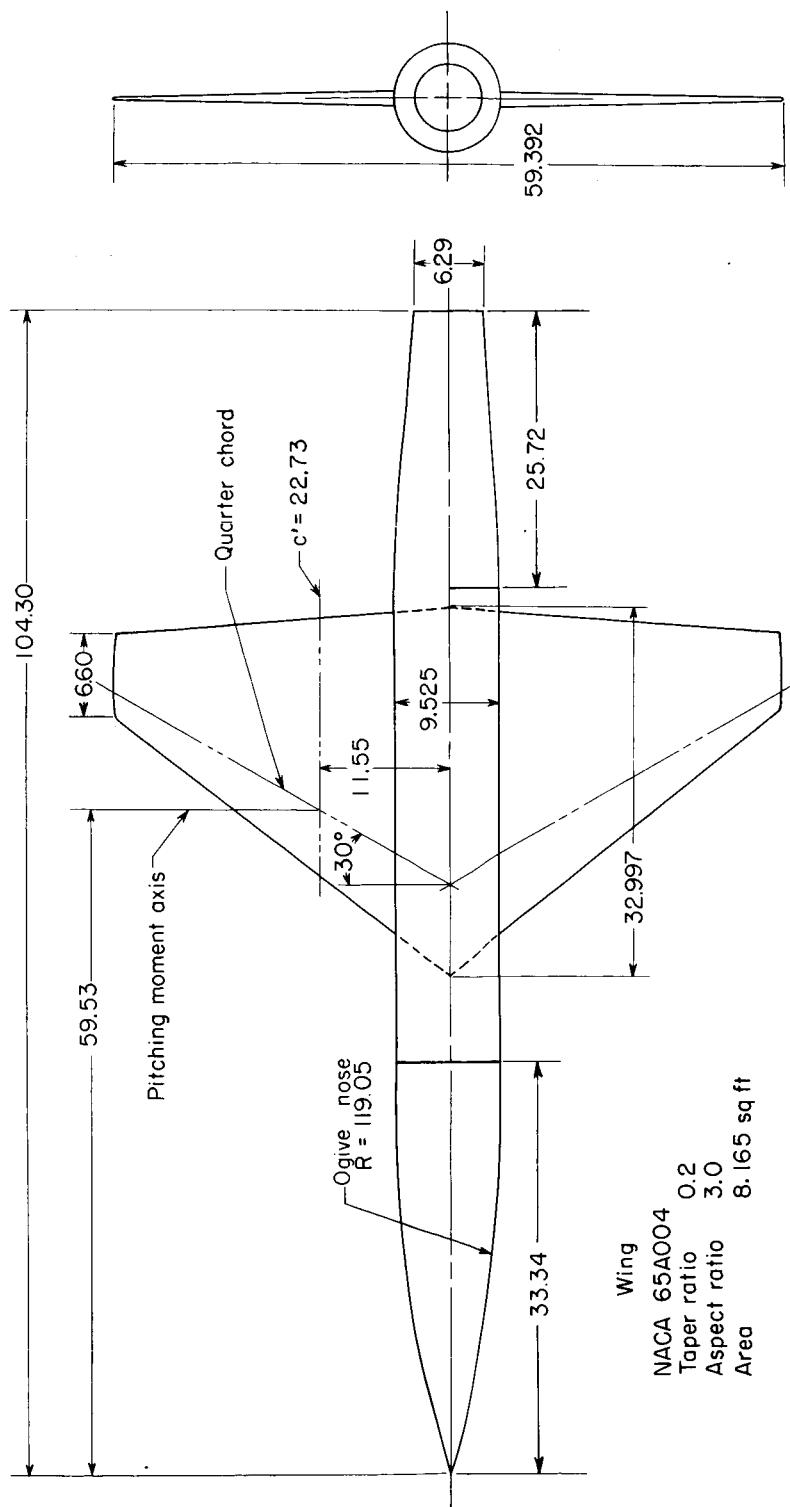
Percent C	Pressure coefficient at:											
	0.18b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Upper Surface												
0.00	-0.019	.737	.695	.667	.616	.560	-0.001	.758	.722	.725	.694	.739
1.25	.312	.245	.281	.303	.296	.357	.022	.065	.058	.064	.059	.147
2.50	.262	.173	.190	.204	.220	.234	.154	.023	.029	.013	.001	.043
3.75	.212	.148	.143	.141	.146	.195	.108	.025	.034	.005	.026	.051
5.00	.185	.120	.137	.133	.112	.153	.088	.025	.012	.016	.052	.059
6.25	.158	.105	.078	.072	.112		.067	.015	.005	.038	.053	.078
7.50	.124	.046	.046	.045	.039	.044	.050	.000	.030	.044	.076	.100
8.75	.096	.037	.015	.013	.011	.023	.007	.027	.059	.068	.095	.114
10.00	.055	.027	.003	.007	.009	.122	.008	.042	.057	.085	.111	.195
11.25	.023	.011	.012	.025	.023	.153	.031	.051	.073	.100	.121	.201
12.50	-.001	-.022	-.032	-.036	-.051	.176	.055	-.076	-.094	-.110	-.145	-.201
13.75	-.039	-.033	-.049	-.063	-.067	.239	-.086	-.098	-.117	-.146	-.163	-.251
15.00	-.016	-.033	-.058	-.080	-.095	.239	-.086	-.109	-.132	-.158	-.185	-.239
16.25	-.027	-.042	-.081	-.098	-.127	.269	-.065	-.097	-.137	-.177	-.210	-.265
17.50	-.042	-.082	-.109	-.127	-.150	.279	-.089	-.124	-.162	-.189	-.231	-.276
18.75	-.088	-.108	-.125	-.144	-.174	.263	-.132	-.159	-.180	-.202	-.246	-.264
20.00	-.090	-.103	-.128	-.158	-.178	.285	-.138	-.155	-.187	-.216	-.237	-.284
21.25	-.092	-.109	-.129	-.159	-.212	.288	-.144	-.161	-.188	-.222	-.255	-.296
22.50	-.098	-.116	-.140	-.159	-.223	.273	-.152	-.168	-.194	-.227	-.247	-.286
23.75	-.129	-.128	-.137	-.160	-.238	.263	-.180	-.184	-.214	-.242	-.263	-.293
25.00	-.138	-.116	-.134	-.162	-.230	.243	-.201	-.182	-.195	-.219	-.247	-.270
26.25	-.103	-.109	-.116	-.161	-.207	.227	-.165	-.179	-.185	-.210	-.242	-.230
27.50	-.077	-.107	-.112	-.152	-.220	.236	-.130	-.174	-.180	-.201	-.249	-.233
Lower Surface												
1.25	.086	-.180	-.128	-.587	-.741	-.787	.192	.067	.017	-.008	-.027	-.080
2.50	.019	-.156	-.189	-.492	-.618	-.722	.131	.012	.002	-.031	-.060	-.073
3.75	-.007	-.093	-.147	-.183	-.454	-.646	.098	.033	.008	-.014	-.042	-.082
5.00	-.022	-.101	-.158	-.205	-.263	-.593	.074	.007	-.017	-.038	-.052	-.097
6.25	-.050	-.111	-.156	-.223	-.250	-.540	.044	-.009	-.036	-.056	-.063	-.096
7.50	-.066	-.107	-.150	-.210	-.239	-.419	.024	-.009	-.046	-.063	-.078	-.109
8.75	-.083	-.112	-.169	-.234	-.269	-.319	-.001	-.040	-.061	-.096	-.107	-.139
10.00	-.105	-.111	-.149	-.198	-.243	-.306	.013	-.030	-.057	-.091	-.111	-.184
11.25	-.085	-.115	-.152	-.196	-.233	-.272	.003	-.040	-.070	-.101	-.120	-.203
12.50	-.100	-.141	-.172	-.214	-.247	-.213	.036	-.067	-.095	-.124	-.144	-.172
13.75	-.147	-.169	-.187	-.233	-.254	-.237	.073	-.095	-.114	-.145	-.157	-.213
15.00	-.119	-.157	-.201	-.254	-.274	-.268	.046	-.084	-.122	-.160	-.178	-.243
16.25	-.158	-.185	-.218	-.275	-.296	-.286	.093	-.114	-.142	-.172	-.192	-.279
17.50	-.184	-.206	-.232	-.281	-.328	-.307	.114	-.161	-.167	-.196	-.223	-.283
18.75	-.209	-.226	-.256	-.319	-.346	-.319	.144	-.161	-.181	-.219	-.242	-.283
20.00	-.220	-.224	-.250	-.315	-.347	-.323	.149	-.169	-.191	-.236	-.262	-.283
21.25	-.224	-.224	-.263	-.303	-.339	-.330	.149	-.157	-.195	-.228	-.254	-.284
22.50	-.248	-.252	-.269	-.309	-.352	-.317	.200	-.182	-.197	-.237	-.272	-.269
23.75	-.266	-.273	-.313	-.342	-.328		.203	-.199	-.203	-.246	-.287	-.278
25.00	-.279	-.266	-.311	-.328	-.328		.233	-.201	-.206	-.237	-.289	-.221
26.25	-.262	-.249	-.272	-.297	-.315		.203	-.206	-.203	-.223	-.280	-.262
27.50	-.166	-.229	-.248	-.277	-.282		.151	-.192	-.198	-.229	-.258	-.225
Upper surface												
0.00	-.009	.722	.645	.666	.654	.727	-.025	.652	.540	.523	.514	.692
1.25	.119	-.108	-.256	-.473	-.555	-.459	.036	-.685	-.779	-.841	-.877	-.885
2.50	.058	-.158	-.184	-.329	-.476	-.628	-.032	-.421	-.692	-.764	-.806	-.903
3.75	-.008	-.125	-.138	-.190	-.321	-.575	.142	-.314	-.607	-.693	-.750	-.853
5.00	-.025	-.130	-.191	-.241	-.241	-.524	.149	-.362	-.486	-.524	-.620	-.740
6.25	-.041	-.130	-.190	-.234	-.234	-.490	.155	-.326	-.420	-.527	-.681	-.761
7.50	-.040	-.091	-.135	-.274	-.292	-.410	.114	-.261	-.313	-.423	-.563	-.746
8.75	-.047	-.110	-.156	-.200	-.250	-.423	.116	-.244	-.327	-.425	-.554	-.725
10.00	-.088	-.108	-.150	-.199	-.219	-.323	.106	-.244	-.327	-.424	-.554	-.711
11.25	-.084	-.132	-.172	-.222	-.250	-.323	.160	-.237	-.327	-.427	-.554	-.666
12.50	-.134	-.172	-.196	-.229	-.229	-.270	.215	-.233	-.323	-.427	-.554	-.601
13.75	-.147	-.173	-.203	-.245	-.245	-.234	.185	-.214	-.327	-.427	-.554	-.624
15.00	-.134	-.161	-.198	-.232	-.261	-.271	.219	-.229	-.328	-.428	-.557	-.587
16.25	-.174	-.174	-.209	-.243	-.279	-.260	.201	-.233	-.327	-.428	-.557	-.590
17.50	-.136	-.169	-.219	-.258	-.300	-.287	.214	-.257	-.327	-.434	-.557	-.590
18.75	-.152	-.194	-.234	-.276	-.320	-.300	.260	-.278	-.347	-.434	-.557	-.590
20.00	-.198	-.223	-.248	-.282	-.336	-.285	.214	-.257	-.327	-.434	-.557	-.590
21.25	-.201	-.222	-.253	-.289	-.330	-.316	.263	-.280	-.361	-.439	-.548	-.590
22.50	-.211	-.221	-.252	-.290	-.341	-.325	.272	-.281	-.313	-.358	-.409	-.436
23.75	-.215	-.228	-.257	-.294	-.342	-.319	.270	-.285	-.320	-.357	-.413	-.354
25.00	-.245	-.243	-.257	-.291	-.336	-.308	.298	-.299	-.316	-.356	-.414	-.332
26.25	-.244	-.257	-.290	-.303	-.303	-.291	.314	-.299	-.316	-.356	-.383	-.323
27.50	-.241	-.243	-.248	-.275	-.277	-.280	.293	-.295	-.302	-.344	-.323	-.317
28.75	-.165	-.233	-.243	-.254	-.276	-.289	.202	-.275	-.299	-.319	-.307	-.338
Lower Surface												
1.25	.291	.261	.262	.291	.332	.285	.420	.439	.440	.478	.526	.455
2.50	.245	.175	.155	.223	.240	.237	.386	.339	.361	.394	.422	.390
3.75	.048	.153	.155	.111	.172	.117	.347	.288	.296	.311	.330	.332
5.00	.174	.117	.082	.124	.141	.143	.306	.237	.246	.259	.279	.270
6.25	.140	.092	.082	.088	.108	.110	.263	.207	.210	.224	.231	.222
7.50	.074	.062	.058	.061	.052	.052	.222	.184	.181	.187	.181	.145
8.75	.081	.042	.038	.018	.027	.019	.180	.183	.146	.133	.145	.065
10.00	.066	.045	.023	.004	.004	.008	.162	.147	.121	.109	.112	.006
11.25	.066	.023	.006	.003	.012	.041	.153	.116	.102	.090	.082	.062
12.50	.008	-.010	-.012	-.026	-.043	-.134	.080	.089	.075	.056	.053	.092
13.75	-.004	-.010	-.012	-.047	-.057	-.192	.090	.076	.055	.034	.031	-.130
15.00	-.018	-.018	-.046	-.081	-.086	-.235	.096	.050	.025	-.001	-.002	-.184
16.25	-.037	-.053	-.075	-.110	-.117	-.257	.028	.019	-.003	-.023	-.037	-.213
17.50	-.065	-.075	-.090	-.122	-.147	-.277	-.003	-.008	-.017	-.036	-.041	-.239
18.75	-.080	-.097	-.117	-.143	-.168	-.279	.002	-.022	-.034	-.053	-.091	-.242
20.00	-.090	-.108	-.123	-.163	-.192	-.278	.015	-.031	-.038	-.072	-.120	-.244
21.25	-.083	-.097	-.123	-.155	-.193	-.279	.028	-.032	-.044	-.071	-.122	-.274
22.50	-.135	-.122	-.131	-.162	-.217	-.266	.042	-.052	-.062	-.092	-.148	-.271
23.75	-.138	-.135	-.140	-.171	-.235	-.269	.051	-.058	-.070	-.105	-.170	-.275
25.00	-.151	-.134	-.137	-.166	-.245	-.213	.066	-.059	-.067	-.109	-.183	-.220
26.25	-.133	-.134	-.131	-.163	-.242	-.251	.058	-.065	-.066	-.106	-.178	-.271
27.50	-.089	-.115	-.125	-.175	-.229	-.213	.049	-.06				

TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Continued

Pressure coefficient at:													
	0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2
Percent c	M = 1.03	a = 5.95°	M = 1.03	a = 7.92°									
Upper surface													
0.00	-0.93	+495	+399	+342	+290	+601	-0.58	+386	+236	+128	+0.31	+448	
1.25	-1.00	+948	+968	-1.008	-1.036	+834	-1.136	-1.030	-1.081	-1.113	-1.123	-0.963	
2.50	-1.182	+891	+873	+932	+976	-1.049	-2.222	-2.946	-0.994	-1.051	-1.072	-1.134	
5.00	-1.313	+625	+808	+855	+908	+993	-3.367	-7.716	-9.932	-9.777	-1.012	-1.079	
7.50	-1.314	+352	+746	+855	+862	+927	-3.357	-4.519	-8.871	-9.933	-0.966	-1.031	
10.00	-1.315	+338	+716	+791	+838	+900	-3.347	-4.386	-8.846	-9.906	-0.942	-1.005	
15.00	-1.241	+314	+350	+730	+814	+874	-2.253	-4.338	-7.777	-8.852	-0.916	-0.977	
20.00	-1.223	+304	+296	+697	+782	+851	-2.217	-4.310	-8.488	-8.818	-0.885	-0.953	
25.00	-1.279	+303	+299	+673	+747	+845	-2.265	-4.299	-8.01	-7.799	-0.847	-0.935	
30.00	-1.336	+306	+297	+453	+728	+799	-3.318	-4.299	-8.355	-7.767	-0.832	-0.900	
40.00	-1.296	+334	+294	+367	+721	+723	-2.277	-4.316	-8.346	-7.734	-0.824	-0.823	
45.00	-1.331	+344	+310	+349	+714	+744	-3.315	-3.329	-8.357	-5.65	-0.815	-0.838	
50.00	-1.338	+347	+325	+349	+704	+709	-3.314	-3.328	-8.370	-5.509	-0.815	-0.805	
55.00	-1.311	+348	+331	+361	+578	+713	-2.290	-3.330	-3.380	-4.487	-0.809	-0.813	
60.00	-1.322	+369	+352	+380	+444	+716	-3.303	-3.346	-4.497	-4.475	-0.817	-0.814	
65.00	-1.324	+364	+354	+387	+464	+705	-3.306	-3.361	-4.400	-4.460	-0.803	-0.807	
70.00	-1.371	+389	+352	+399	+444	+714	-3.345	-3.366	-3.399	-4.556	-0.706	-0.811	
75.00	-1.376	+385	+354	+397	+445	+714	-3.345	-3.364	-3.399	-4.553	-0.625	-0.819	
80.00	-1.373	+391	+361	+397	+445	+716	-3.342	-3.367	-4.405	-4.552	-0.587	-0.823	
85.00	-1.414	+403	+353	+395	+435	+701	-3.377	-3.375	-4.400	-4.451	-0.513	-0.815	
90.00	-1.385	+398	+340	+386	+381	+704	-3.355	-3.375	-3.385	-4.443	-0.425	-0.822	
95.00	-1.271	+369	+334	+367	+324	+710	-2.256	-3.364	-3.383	-4.246	-0.333	-0.833	
Lower surface													
0.00	+535	+562	+593	+619	+642	+555	+705	+714	+687	+693	+703	+611	
1.25	+518	+511	+532	+545	+490	+696	+614	+613	+618	+621	+548		
5.00	+472	+383	+435	+440	+453	+433	+638	+535	+528	+525	+532	+489	
7.50	+413	+327	+377	+384	+395	+363	+575	+442	+436	+426	+421	+375	
10.00	+361	+298	+345	+347	+345	+316	+511	+442	+436	+426	+421	+375	
15.00	+300	+249	+294	+297	+286	+225	+441	+381	+373	+368	+359	+284	
20.00	+250	+229	+249	+236	+240	+145	+383	+360	+325	+306	+309	+204	
25.00	+216	+187	+221	+205	+203	+078	+352	+313	+291	+270	+270	+11	
30.00	+195	+152	+194	+180	+171	+016	+317	+276	+260	+242	+235	+074	
35.00	+109	+124	+159	+144	+149	+010	+227	+249	+225	+203	+193	+059	
40.00	+121	+105	+139	+139	+110	+066	+243	+221	+199	+172	+171	+015	
45.00	+124	+106	+136	+108	+076	+124	+235	+186	+166	+136	+131	+075	
50.00	+057	+037	+060	+057	+044	+153	+170	+149	+135	+109	+100	+105	
55.00	+021	+012	+063	+041	+004	+182	+136	+127	+118	+091	+061	+136	
60.00	+025	+006	+041	+018	+022	+197	+138	+106	+091	+066	+028	+154	
65.00	+004	+023	+026	+002	+051	+215	+106	+085	+078	+043	+003	+186	
70.00	+025	+027	+021	+006	+052	+230	+075	+079	+064	+032	+009	+190	
75.00	+039	+056	+004	+034	+089	+228	+065	+052	+041	+004	+004	+208	
80.00	+054	+063	+013	+050	+109	+238	+048	+041	+031	+004	+006	+056	
85.00	+075	+067	+013	+050	+120	+192	+028	+036	+031	+004	+006	+165	
90.00	+082	+073	+014	+048	+120	+238	+022	+030	+031	+002	+006	+212	
95.00	+066	+081	+019	+062	+111	+210	+024	+017	+018	+022	+057	+182	
Upper surface													
0.00	M = 1.03	a = 9.89°	M = 1.03	a = 13.68°									
1.25	-0.91	+206	+044	+108	+270	+239	-1.121	-1.159	-1.406	-1.598	-1.760	-0.290	
2.50	-1.260	+1136	+1163	+1165	+1813	+1074	-1.183	-1.133	-1.087	-1.046	-1.065	-1.102	
5.00	-1.358	+1068	+1084	+1136	+1155	+1198	-1.154	-1.092	-1.073	-1.052	-1.044	-1.120	
7.50	-1.513	+1036	+1052	+1072	+1091	+1161	-1.171	-1.053	-1.056	-1.036	-1.045	-1.104	
10.00	-1.496	+974	+974	+1028	+1058	+1128	-1.180	-1.094	-1.040	-1.040	-1.045	-1.101	
15.00	-1.479	+611	+956	+1003	+1036	+1040	-1.190	-1.046	-1.023	-1.008	-1.024	-1.091	
20.00	-1.359	+518	+878	+946	+946	+1069	-1.196	-0.880	-1.063	-1.008	-1.008	-1.010	
25.00	-1.322	+463	+703	+911	+982	+1046	-1.201	-0.805	-0.907	-0.962	-1.020	-1.080	
30.00	-1.373	+387	+532	+872	+929	+1001	-1.215	-0.537	-0.860	-0.958	-0.997	-1.056	
35.00	-1.333	+371	+478	+857	+921	+922	-1.227	-0.344	-0.828	-0.922	-0.978	-1.028	
40.00	-1.364	+371	+430	+808	+912	+924	-1.227	-0.395	-0.810	-0.902	-0.960	-0.975	
45.00	-1.369	+371	+414	+661	+912	+899	-1.235	-0.444	-0.774	-0.868	-0.934	-0.959	
50.00	-1.355	+373	+419	+626	+909	+899	-1.244	-0.447	-0.748	-0.858	-0.918	-0.950	
55.00	-1.366	+391	+431	+620	+909	+898	-1.256	-0.456	-0.715	-0.846	-0.902	-0.944	
60.00	-1.403	+419	+442	+603	+910	+903	-1.283	-0.483	-0.672	-0.827	-0.883	-0.931	
65.00	-1.407	+417	+440	+590	+897	+908	-1.288	-0.488	-0.607	-0.812	-0.839	-0.903	
70.00	-1.407	+418	+445	+577	+861	+914	-1.298	-0.498	-0.504	-0.803	-0.798	-0.889	
75.00	-1.399	+424	+454	+557	+745	+922	-1.307	-0.487	-0.508	-0.808	-0.752	-0.895	
80.00	-1.424	+437	+454	+540	+664	+922	-1.321	-0.521	-0.500	-0.793	-0.714	-0.885	
85.00	-1.441	+438	+454	+527	+559	+922	-1.330	-0.530	-0.505	-0.777	-0.666	-0.877	
90.00	-1.424	+438	+443	+505	+507	+927	-1.318	-0.518	-0.504	-0.657	-0.618	-0.907	
95.00	-1.325	+426	+443	+472	+467	+946	-1.443	-0.499	-0.510	-0.548	-0.597	-0.908	
Lower surface													
0.00	.805	.803	.757	.749	.741	.646	.958	.914	.844	.807	.771	.685	
1.25	.803	.716	.694	.689	.678	.595	.979	.850	.808	.777	.754	.657	
5.00	.742	.622	.611	.596	.594	.541	.902	.767	.735	.708	.693	.616	
7.50	.663	.562	.553	.542	.540	.481	.818	.764	.677	.657	.646	.567	
10.00	.598	.526	.511	.499	.490	.427	.741	.663	.640	.644	.602	.520	
15.00	.516	.463	.448	.438	.437	.335	.657	.595	.570	.556	.541	.438	
20.00	.449	.429	.394	.376	.373	.260	.586	.557	.515	.492	.488	.366	
25.00	.410	.378	.359	.340	.333	.195	.538	.501	.475	.455	.445	.301	
30.00	.376	.323	.308	.292	.292	.125	.496	.458	.435	.417	.405	.236	
35.00	.281	.303	.287	.268	.252	.112	.403	.416	.397	.378	.360	.204	
40.00	.292	.272	.258	.237	.227	.037	.409	.386	.365	.345	.331	.139	
45.00	.284	.241	.222	.195	.187	.024	.393	.353	.329	.305	.294	.078	
50.00	.218	.203	.193	.170	.156	.057	.327	.310	.299	.273	.258	.045	
55.00	.176	.178	.173	.151	.113	.086	.294	.279	.275	.252	.217	.022	
60.00	.185	.158	.146	.123	.084	.109	.291	.257	.240	.223	.181	.004	
65.00	.147	.133	.128	.099	.048	.141	.250	.227	.221	.192	.149	.037	
70.00	.113	.126	.114	.086	.047	.141	.205	.218	.204	.181	.144	.044	
75.00	.102	.096	.090	.062	.014	.149	.194	.186	.180	.157	.117	.056	
80.00	.083	.085	.080	.055	.001	.167	.173	.172	.166	.146	.103	.069	
85.00	.062	.078	.080	.054	-.005	.125	.140	.158	.155	.134	.086	.041	
90.00	.050	.066	.068	.050	-.005	.164	.120	.136	.134	.123	.075	.047	
95.00	.041	.044</											

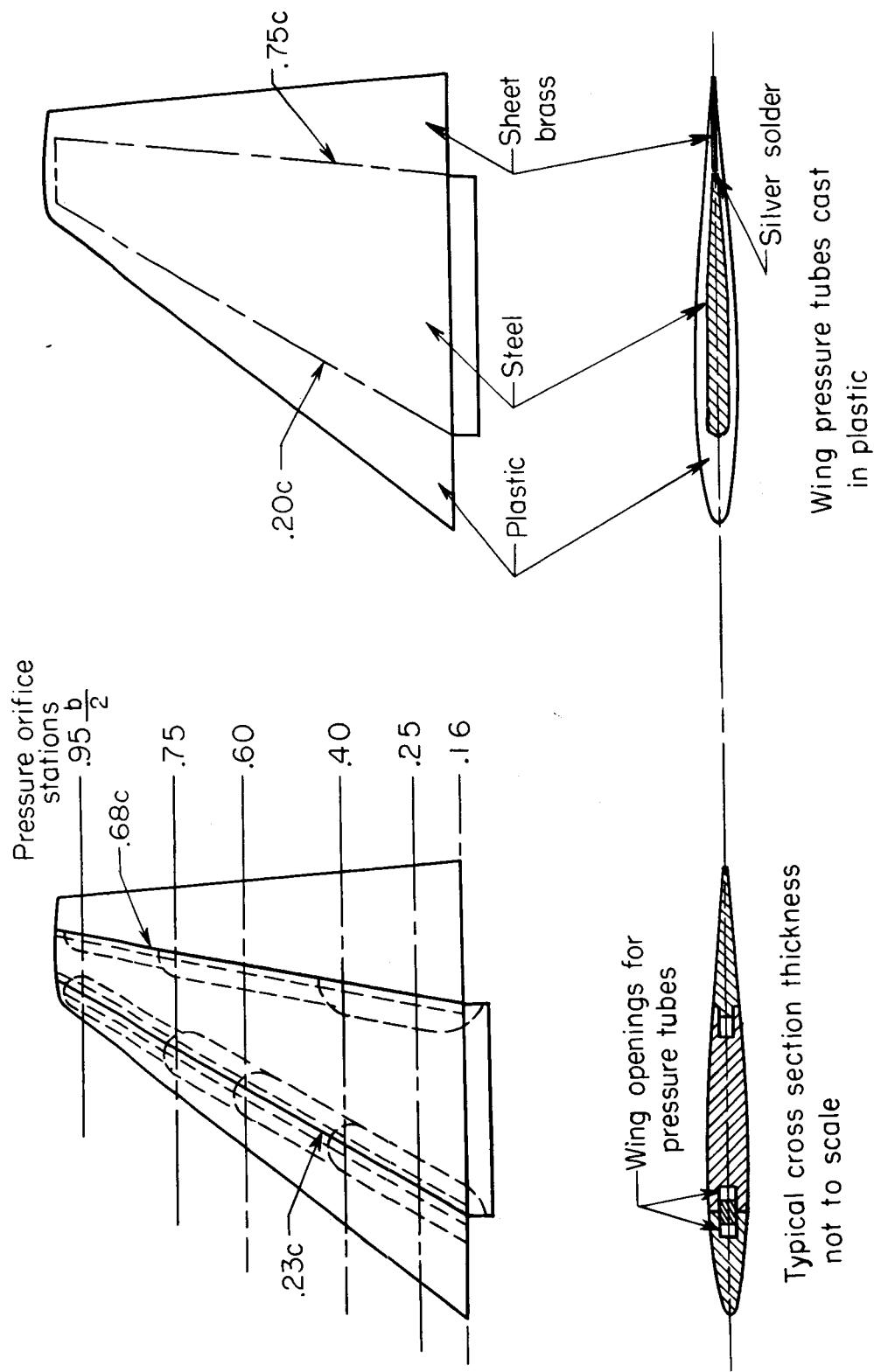
TABLE I. - STEEL WING PRESSURE COEFFICIENT DATA FOR THE TEST
RANGE OF ANGLE OF ATTACK AND MACH NUMBER - Concluded

		Pressure coefficient at:														
		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		0.16b/2	0.25b/2	0.40b/2	0.60b/2	0.75b/2	0.95b/2		
Percent C	M = 1.03	$\alpha = 15.85^\circ$						$\alpha = 1.03^\circ$						$\alpha = 17.97^\circ$		
		-1.152	-1.378	-1.588	-1.818	-1.932	-1.599	-1.172	-1.559	-1.765	-1.965	-1.062	-1.830			
Upper surface	0.00	-1.152	-1.378	-1.588	-1.818	-1.932	-1.599	-1.172	-1.559	-1.765	-1.965	-1.062	-1.830			
	1.25	-1.604	-1.188	-1.129	-1.072	-1.003	-0.918	-1.709	-1.245	-1.193	-1.047	-0.973	-0.870			
	2.50	-1.715	-1.179	-1.108	-1.076	-1.003	-0.907	-1.833	-1.233	-1.166	-1.042	-0.973	-0.866			
	5.00	-1.827	-1.144	-1.132	-1.068	-1.002	-0.901	-1.936	-1.213	-1.196	-1.037	-0.979	-0.861			
	7.50	-1.794	-1.107	-1.107	-1.072	-0.990	-0.894	-1.952	-1.184	-1.152	-1.036	-0.977	-0.861			
	10.00	-1.761	-1.064	-1.103	-1.080	-0.985	-0.894	-1.868	-1.176	-1.190	-1.033	-0.989	-0.850			
	15.00	-1.602	-1.016	-1.064	-1.073	-0.992	-0.894	-1.733	-1.115	-1.159	-1.026	-1.002	-0.859			
	20.00	-1.517	-0.977	-1.023	-1.049	-0.990	-0.894	-1.611	-1.073	-1.125	-1.018	-1.007	-0.856			
	25.00	-1.493	-0.743	-0.984	-1.049	-0.981	-0.891	-1.561	-1.021	-1.098	-1.015	-1.004	-0.853			
	30.00	-1.506	-0.449	-0.956	-1.022	-0.980	-0.889	-1.565	-1.073	-1.074	-1.003	-0.994	-0.851			
	35.00	-1.476	-0.454	-0.939	-1.005	-0.970	-0.884	-1.545	-1.029	-1.061	-0.995	-0.984	-0.850			
	40.00	-1.486	-0.478	-0.929	-0.992	-0.960	-0.888	-1.552	-1.048	-1.048	-0.983	-0.977	-0.849			
	45.00	-1.497	-0.493	-0.920	-0.974	-0.953	-0.879	-1.553	-1.060	-1.039	-0.965	-0.971	-0.844			
	50.00	-1.513	-0.505	-0.909	-0.966	-0.940	-0.872	-1.574	-1.071	-1.035	-0.950	-0.959	-0.841			
	55.00	-1.527	-0.523	-0.925	-0.976	-0.866	-0.858	-1.587	-1.092	-1.025	-0.935	-0.948	-0.837			
Lower surface	60.00	-1.551	-0.552	-0.830	-0.927	-0.914	-0.858	-1.607	-1.115	-1.099	-0.913	-0.934	-0.835			
	65.00	-1.555	-0.561	-0.721	-0.910	-0.896	-0.847	-1.613	-1.120	-1.011	-0.899	-0.914	-0.828			
	70.00	-1.553	-0.566	-0.580	-0.894	-0.872	-0.843	-1.601	-1.124	-1.073	-0.886	-0.896	-0.828			
	75.00	-1.542	-0.573	-0.517	-0.873	-0.855	-0.843	-1.594	-1.132	-1.059	-0.866	-0.880	-0.828			
	80.00	-1.587	-0.585	-0.513	-0.844	-0.839	-0.843	-1.625	-1.143	-1.066	-0.855	-0.866	-0.825			
	85.00	-1.593	-0.589	-0.526	-0.812	-0.804	-0.843	-1.641	-1.161	-1.057	-0.843	-0.837	-0.824			
	90.00	-1.579	-0.587	-0.522	-0.754	-0.772	-0.852	-1.618	-1.075	-1.049	-0.827	-0.811	-0.826			
	95.00	-1.507	-0.509	-0.518	-0.696	-0.773	-0.851	-1.431	-1.084	-1.080	-0.813	-0.820	-0.826			
	1.25	1.013	.950	.876	.822	.769	.688	1.047	.974	.882	.818	.755	.682			
	2.50	1.048	.908	.855	.815	.781	.674	1.103	.913	.862	.836	.792	.678			
	5.00	.967	.830	.795	.761	.741	.650	1.019	.885	.832	.798	.768	.670			
	7.50	.877	.767	.742	.713	.698	.667	.928	.823	.785	.754	.735	.635			
	10.00	.804	.727	.706	.671	.655	.566	.861	.778	.746	.718	.699	.596			
	15.00	.720	.650	.629	.613	.599	.487	.772	.710	.685	.657	.634	.525			
	20.00	.645	.591	.556	.543	.418	.397	.697	.660	.626	.599	.584	.456			
	30.00	.595	.559	.537	.515	.500	.355	.647	.617	.577	.559	.541	.396			
	35.00	.557	.514	.497	.480	.463	.292	.604	.567	.543	.525	.501	.329			
	40.00	.462	.475	.457	.437	.417	.259	.515	.526	.503	.483	.459	.299			
	45.00	.465	.444	.425	.402	.388	.195	.515	.489	.469	.443	.429	.236			
	50.00	.448	.404	.390	.363	.352	.136	.494	.455	.434	.407	.393	.176			
	55.00	.380	.366	.354	.330	.318	.102	.431	.412	.398	.374	.358	.142			
	60.00	.342	.334	.331	.308	.278	.074	.388	.382	.370	.352	.314	.114			
	65.00	.339	.309	.297	.279	.242	.047	.382	.352	.337	.320	.277	.089			
	70.00	.295	.280	.278	.247	.205	.022	.339	.319	.313	.286	.245	.062			
	75.00	.250	.264	.255	.232	.200	.003	.289	.306	.291	.272	.216	.077			
	80.00	.209	.214	.210	.191	.153	.022	.271	.269	.244	.242	.204	.025			
	85.00	.175	.197	.197	.179	.133	.004	.246	.248	.241	.223	.179	.006			
	90.00	.151	.173	.173	.170	.156	.115	.104	.107	.129	.125	.106	.023			
	95.00	.110	.126	.135	.105	.081	.032	.125	.150	.150	.118	.092	.019			



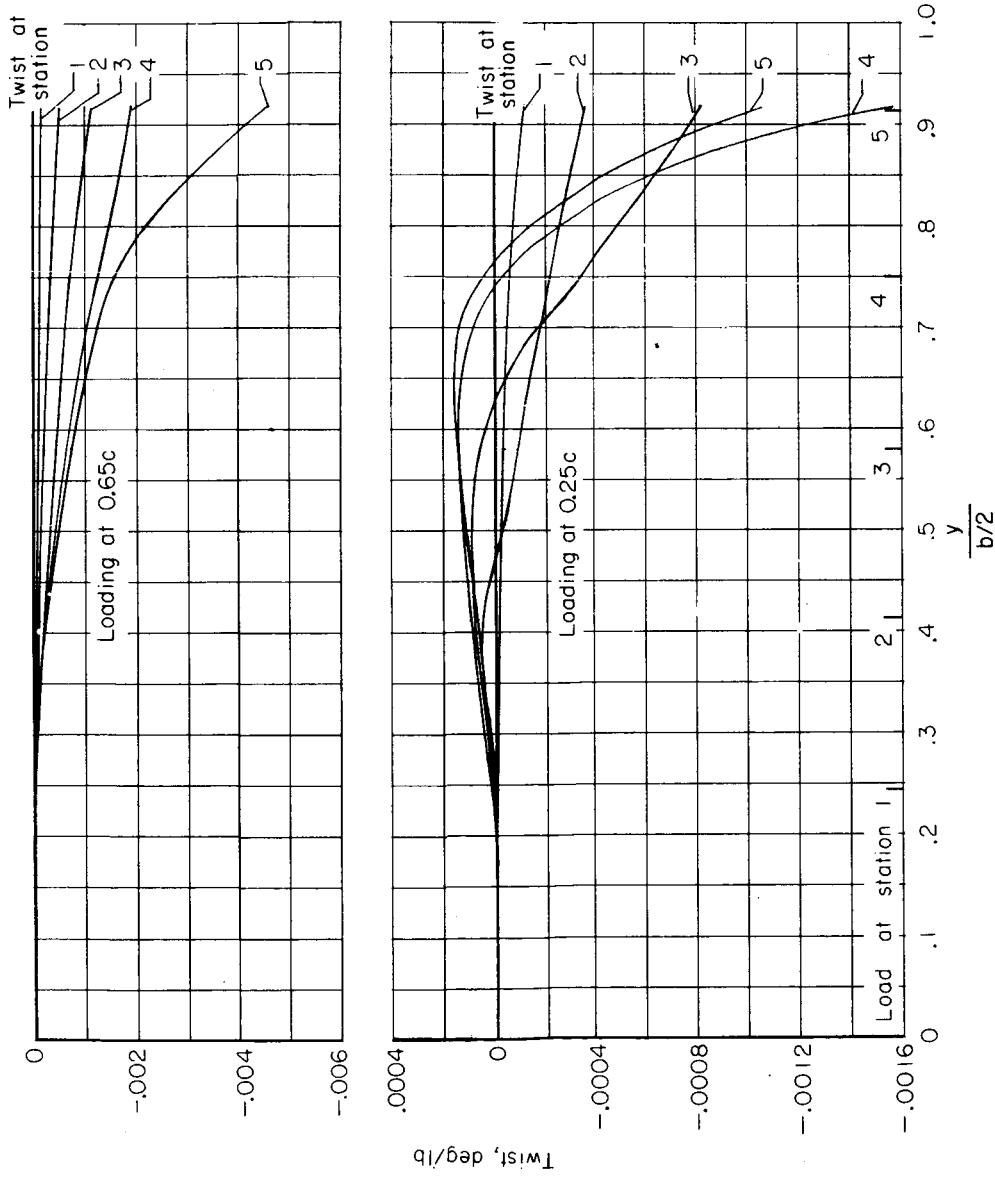
(a) Complete model.

Figure 1.- General model arrangement. All dimensions in inches.



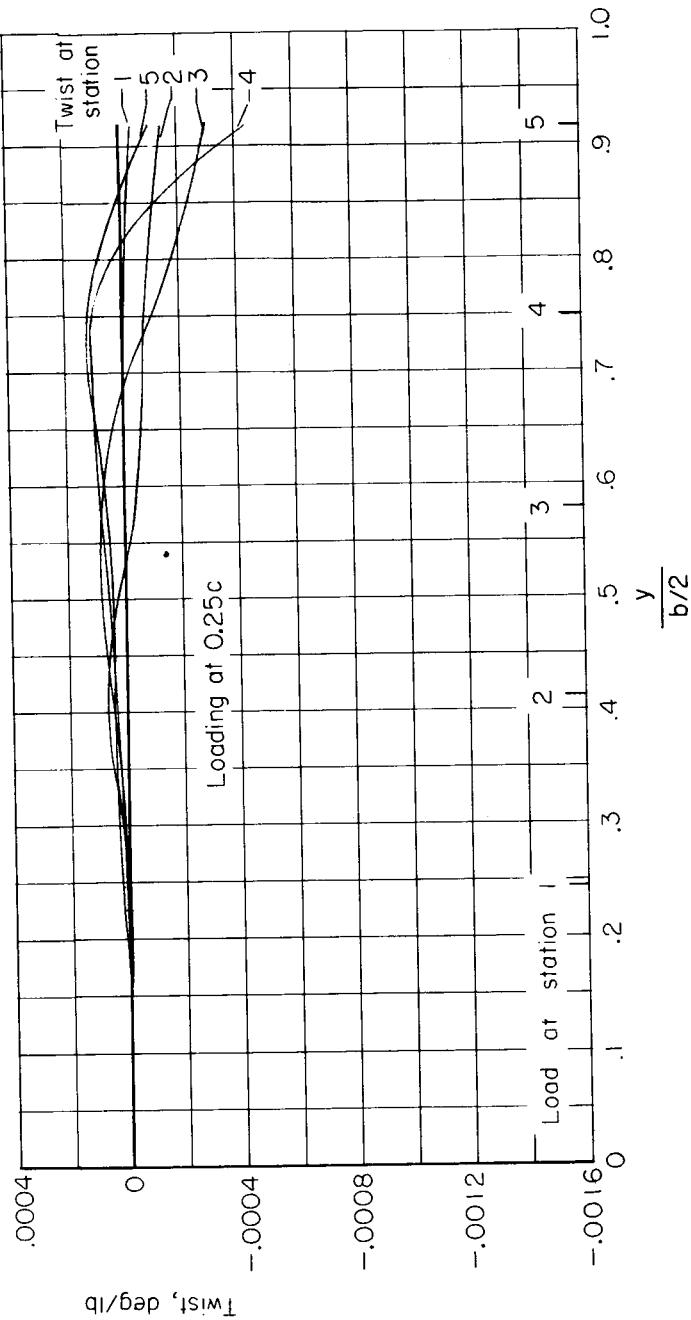
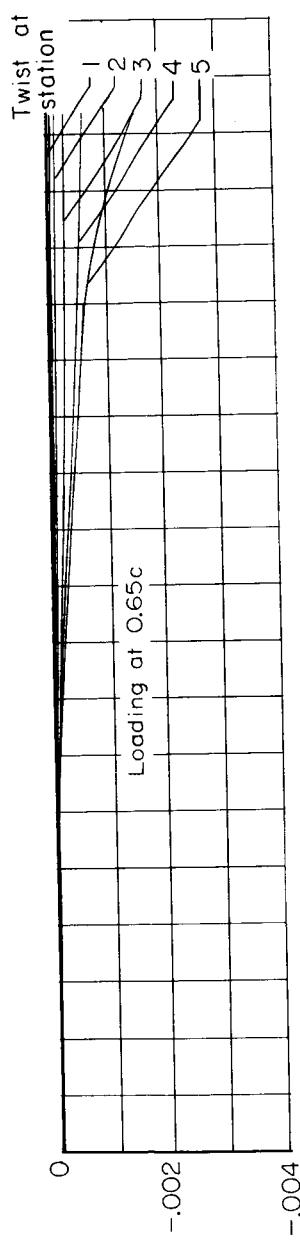
(b) Wings.

Figure 1.- Concluded.



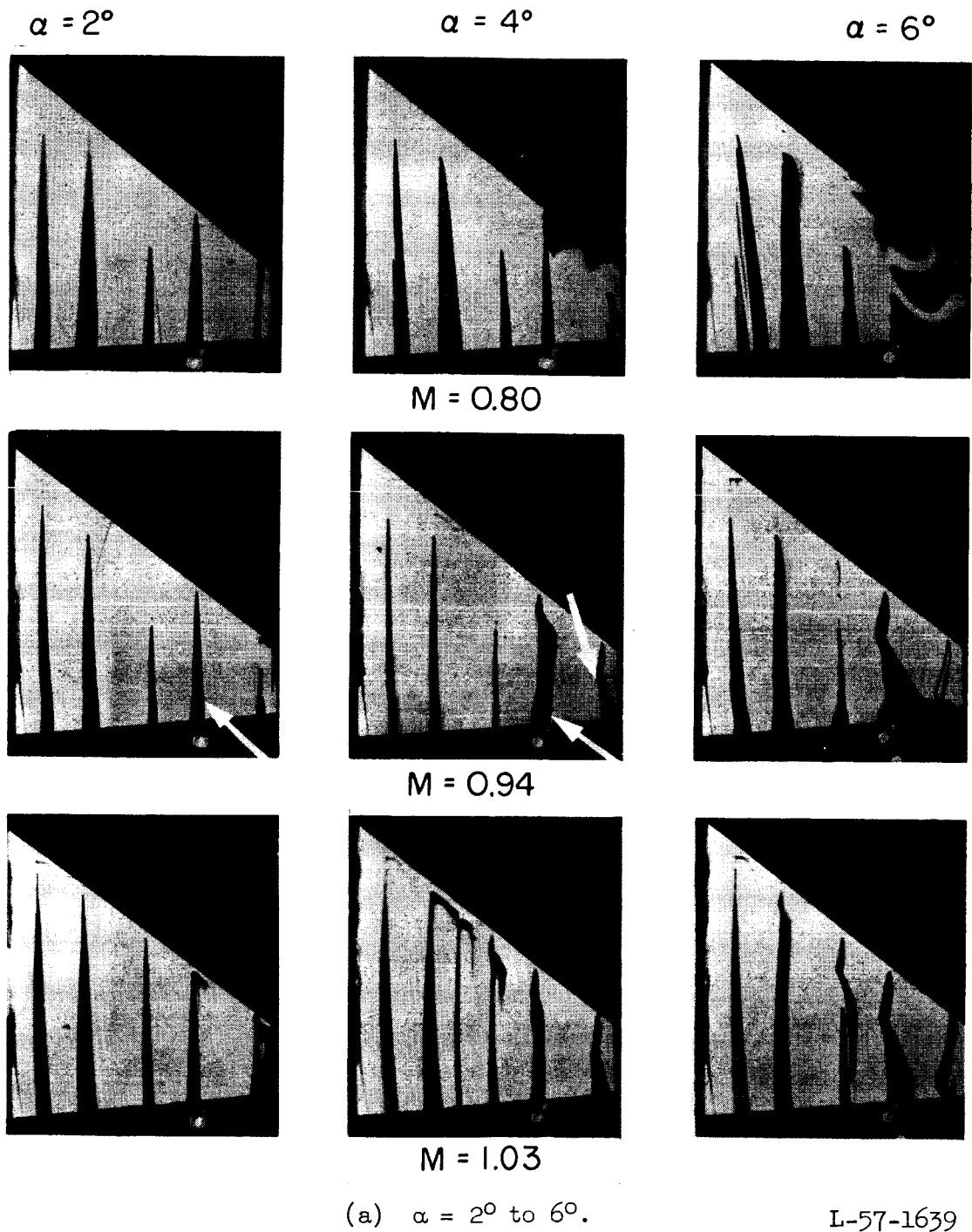
(a) Plastic wing.

Figure 2.- Wing elastic characteristics obtained experimentally, from which the influence coefficients were determined for twist in the angle-of-attack plane about $0.25c$.



(b) Steel wing.

Figure 2.- Concluded.

(a) $\alpha = 2^\circ$ to 6° .

L-57-1639

Figure 3.- Typical flow study photographs for a range of Mach number and angle of attack, plastic wing.

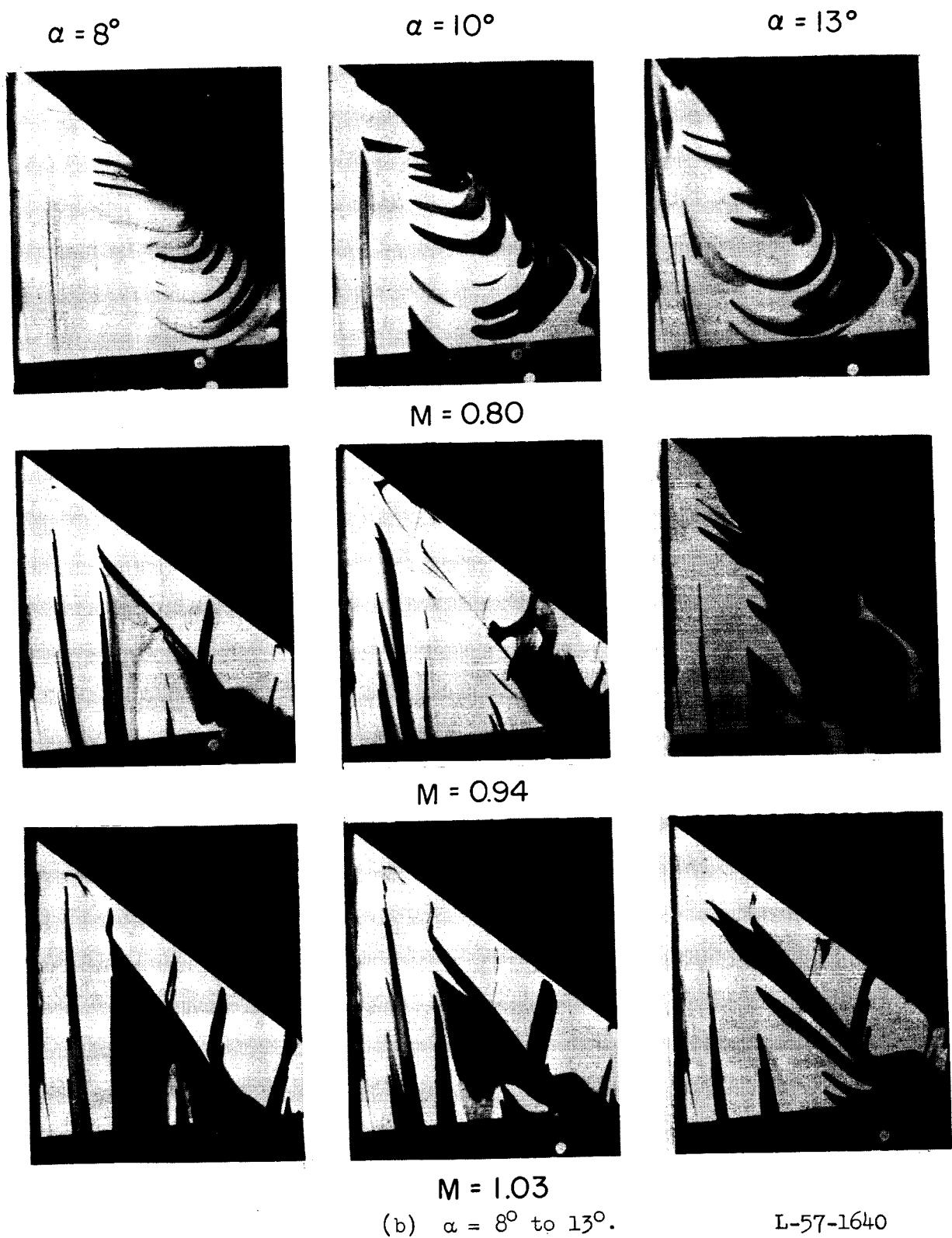


Figure 3.- Continued.

(b) $\alpha = 8^\circ$ to 13° .

L-57-1640

$\alpha = 15^\circ$  $\alpha = 17^\circ$  $\alpha = 19^\circ$  $M = 0.80$ $\alpha = 15^\circ$  $\alpha = 17^\circ$  $M = 0.94$ $\alpha = 15^\circ$  $M = 1.03$ (c) $\alpha = 15^\circ$ to 19° .

L-57-1641

Figure 3.- Concluded.

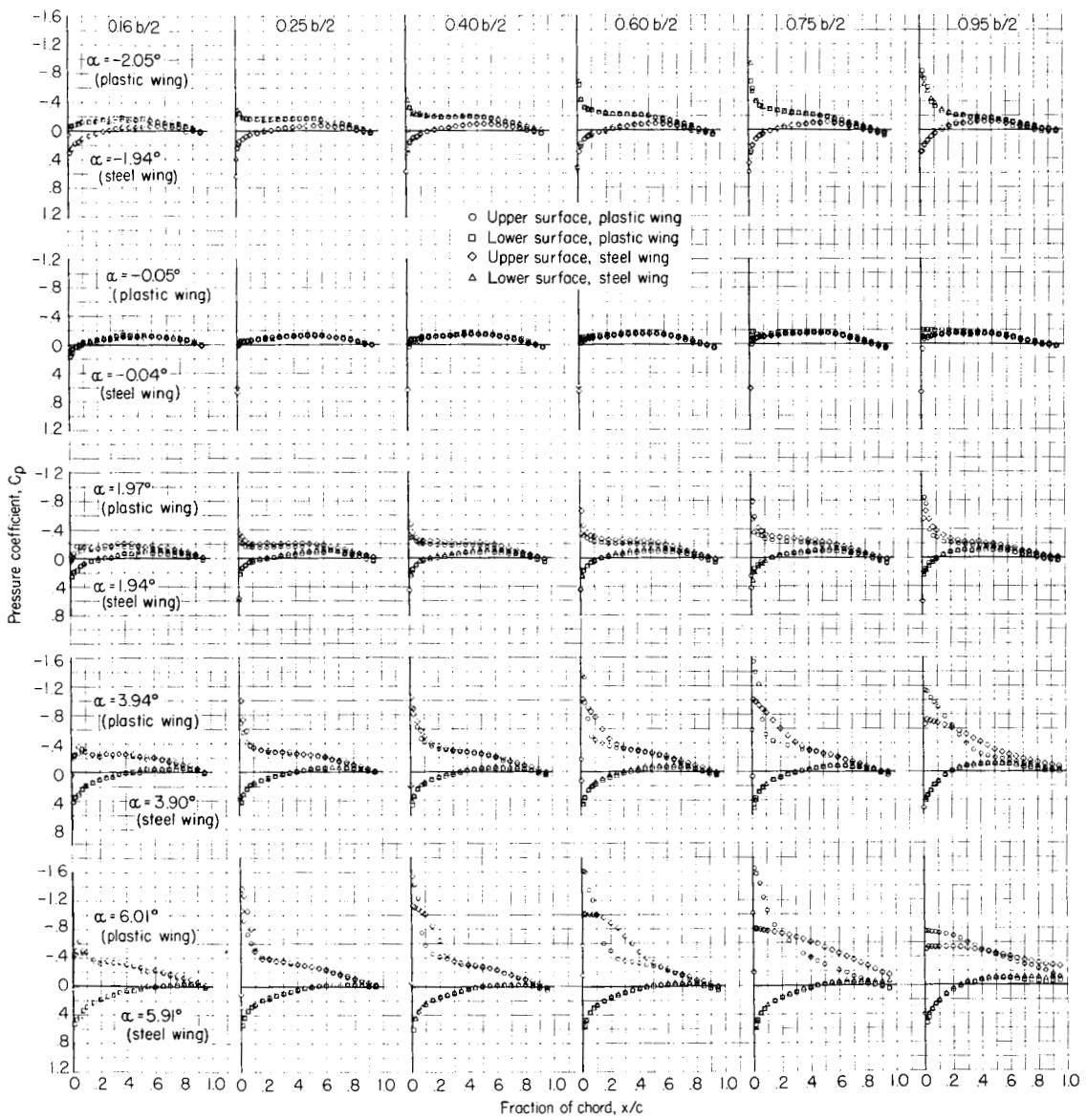
(a) $M = 0.80$.

Figure 4.- Comparison of chordwise pressure distributions for steel and plastic wings.

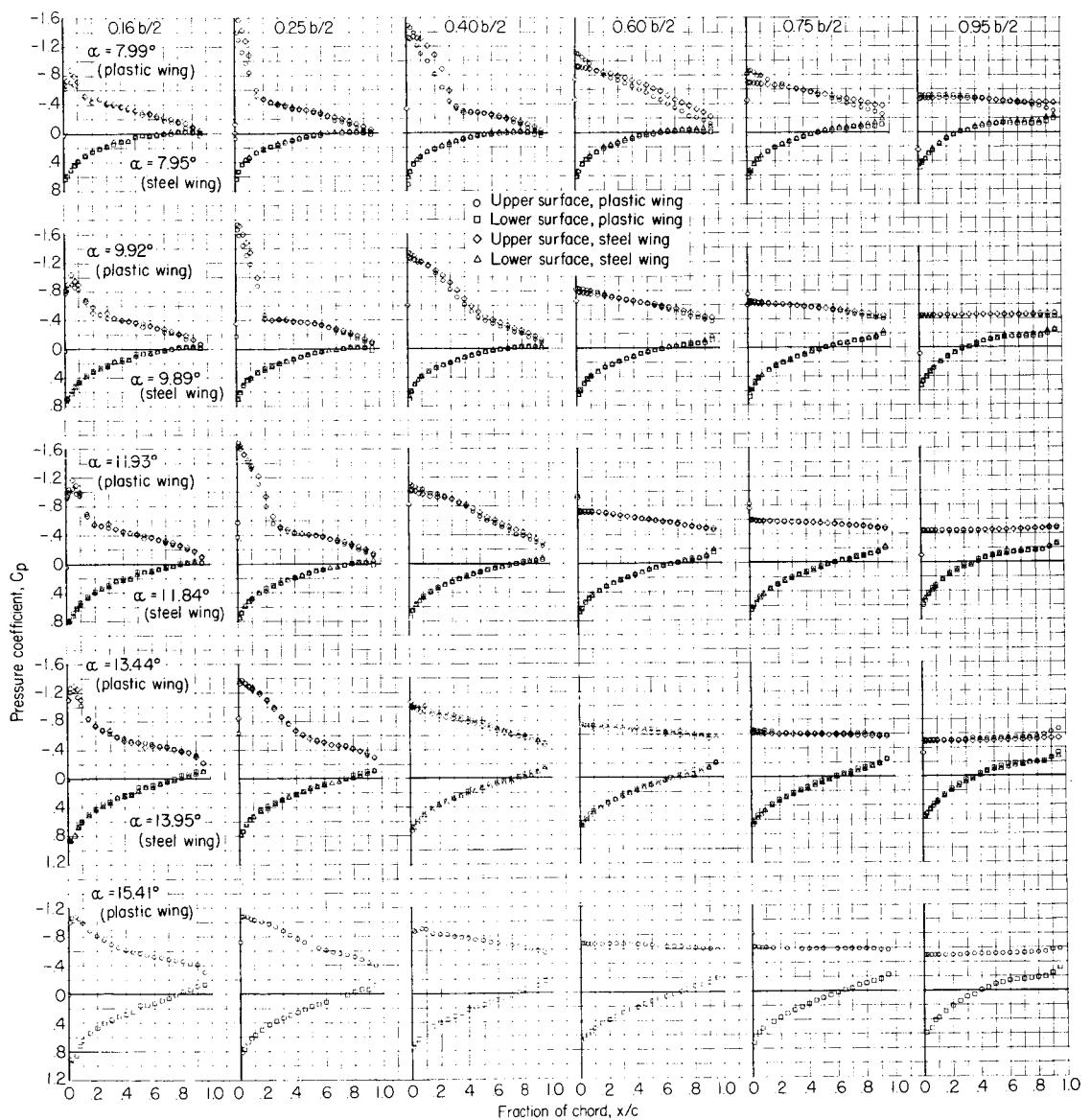
(a) $M = 0.80$, continued.

Figure 4.- Continued.

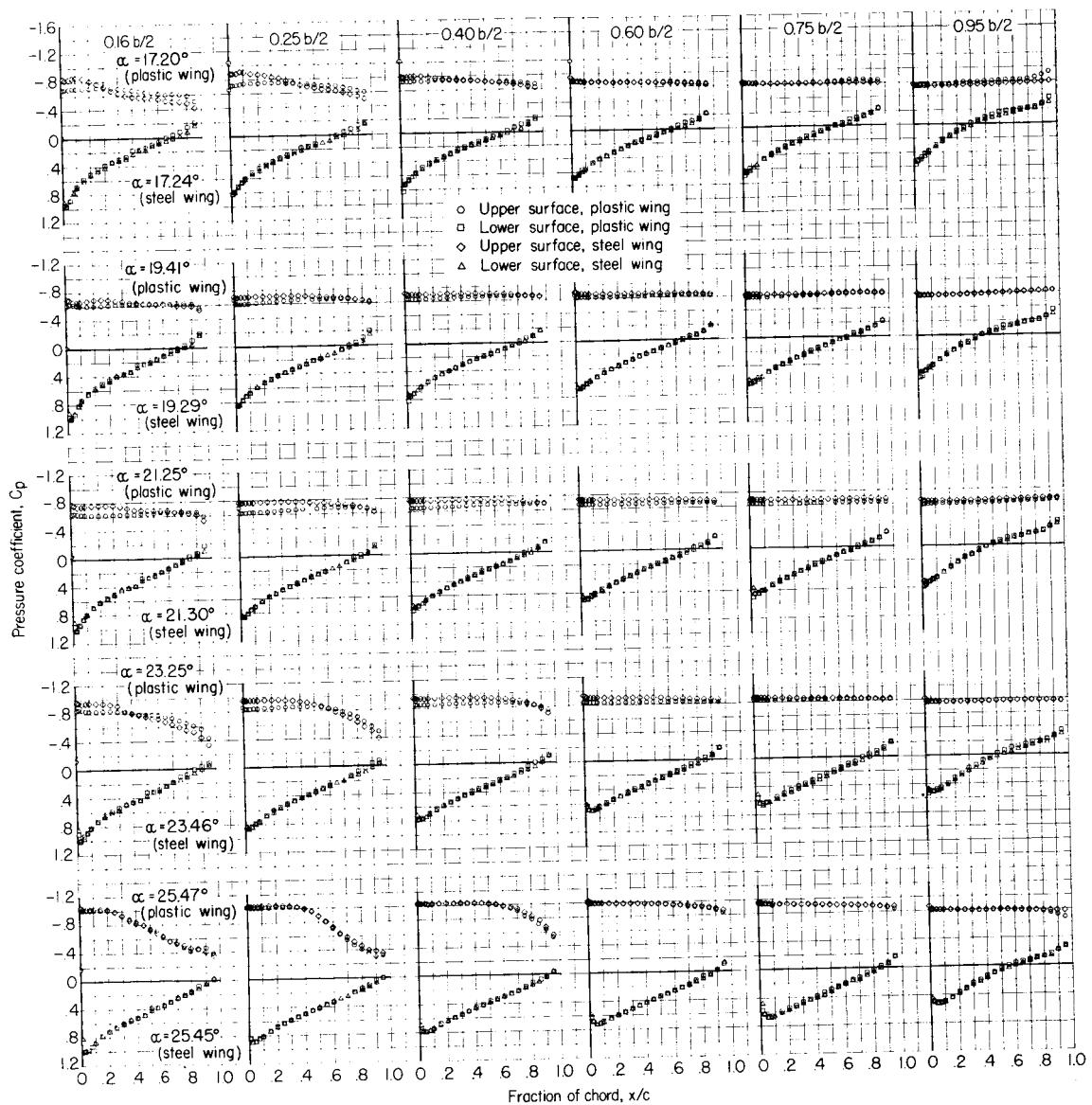
(a) $M = 0.80$, concluded.

Figure 4.- Continued.

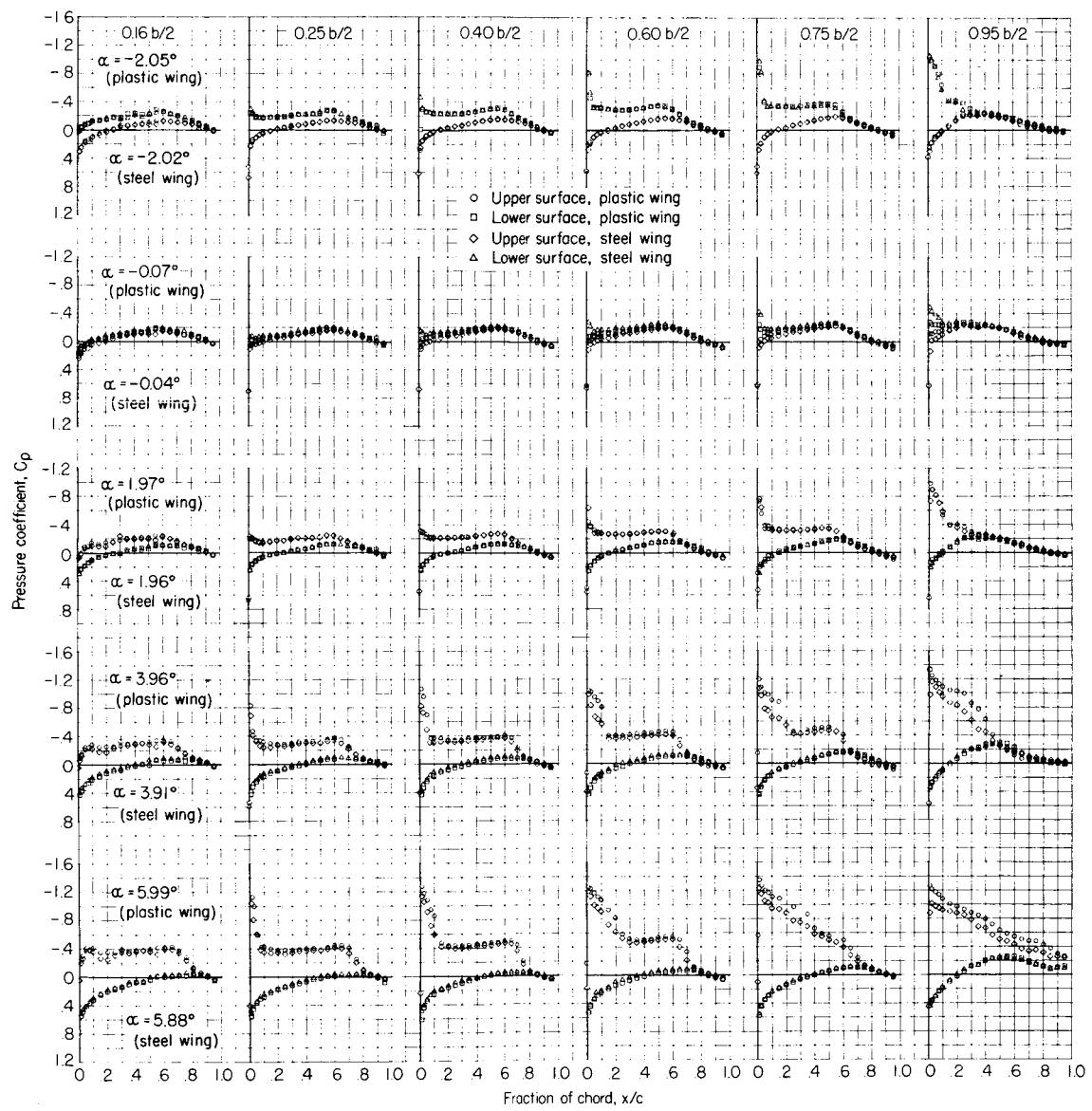
(b) $M = 0.90.$

Figure 4.- Continued.

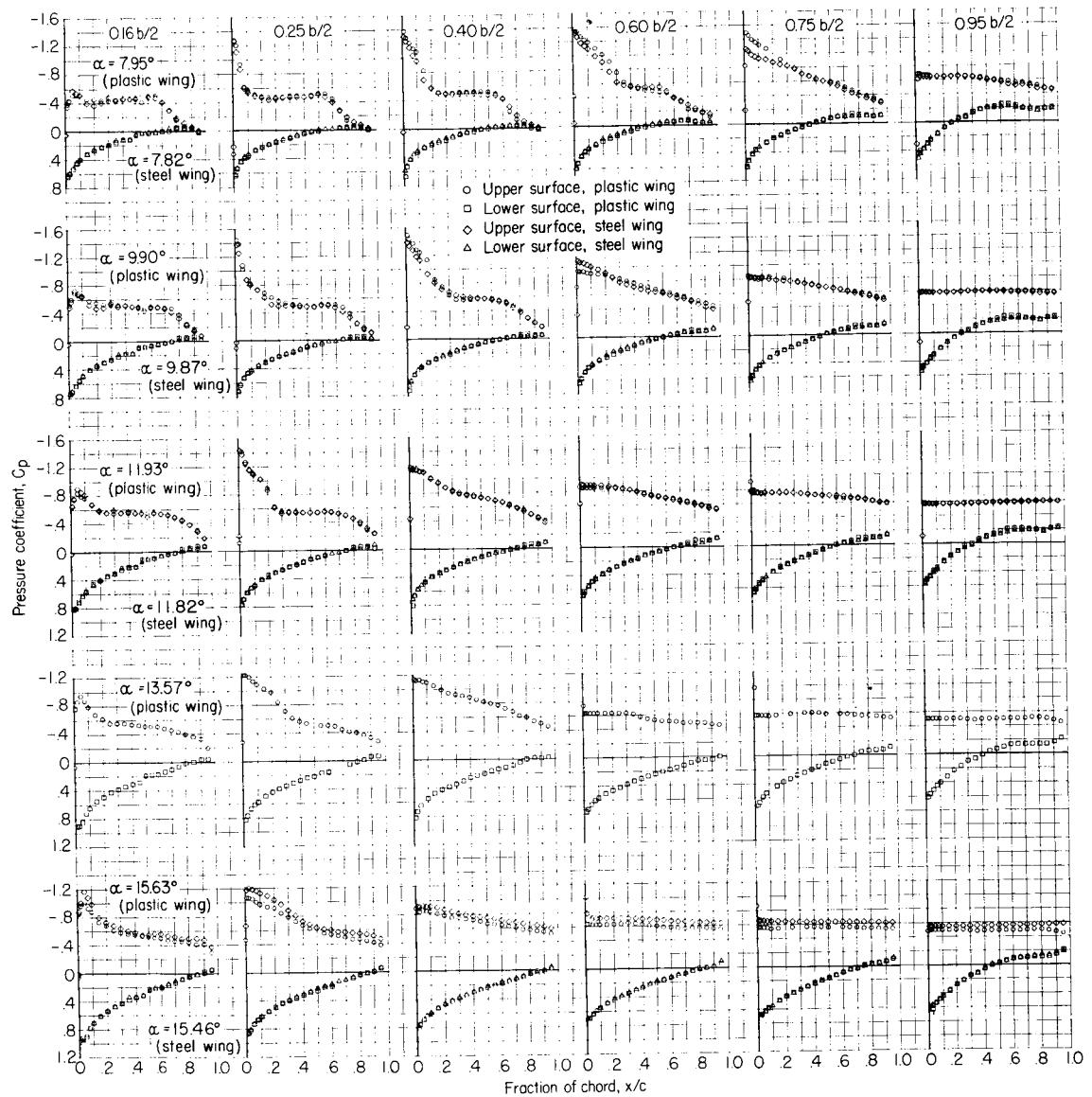


Figure 4.- Continued.

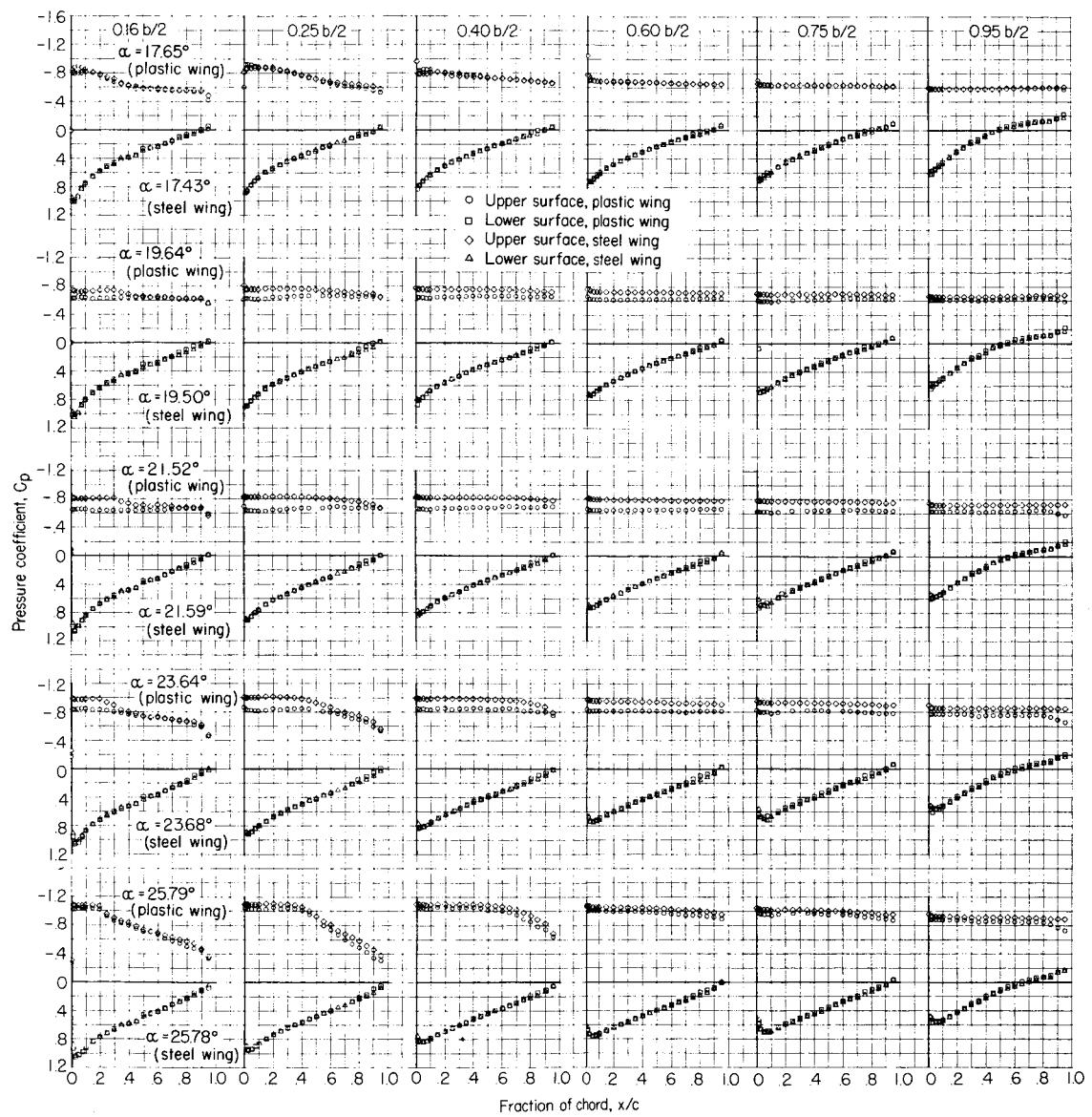
(b) $M = 0.90$, concluded.

Figure 4.- Continued.

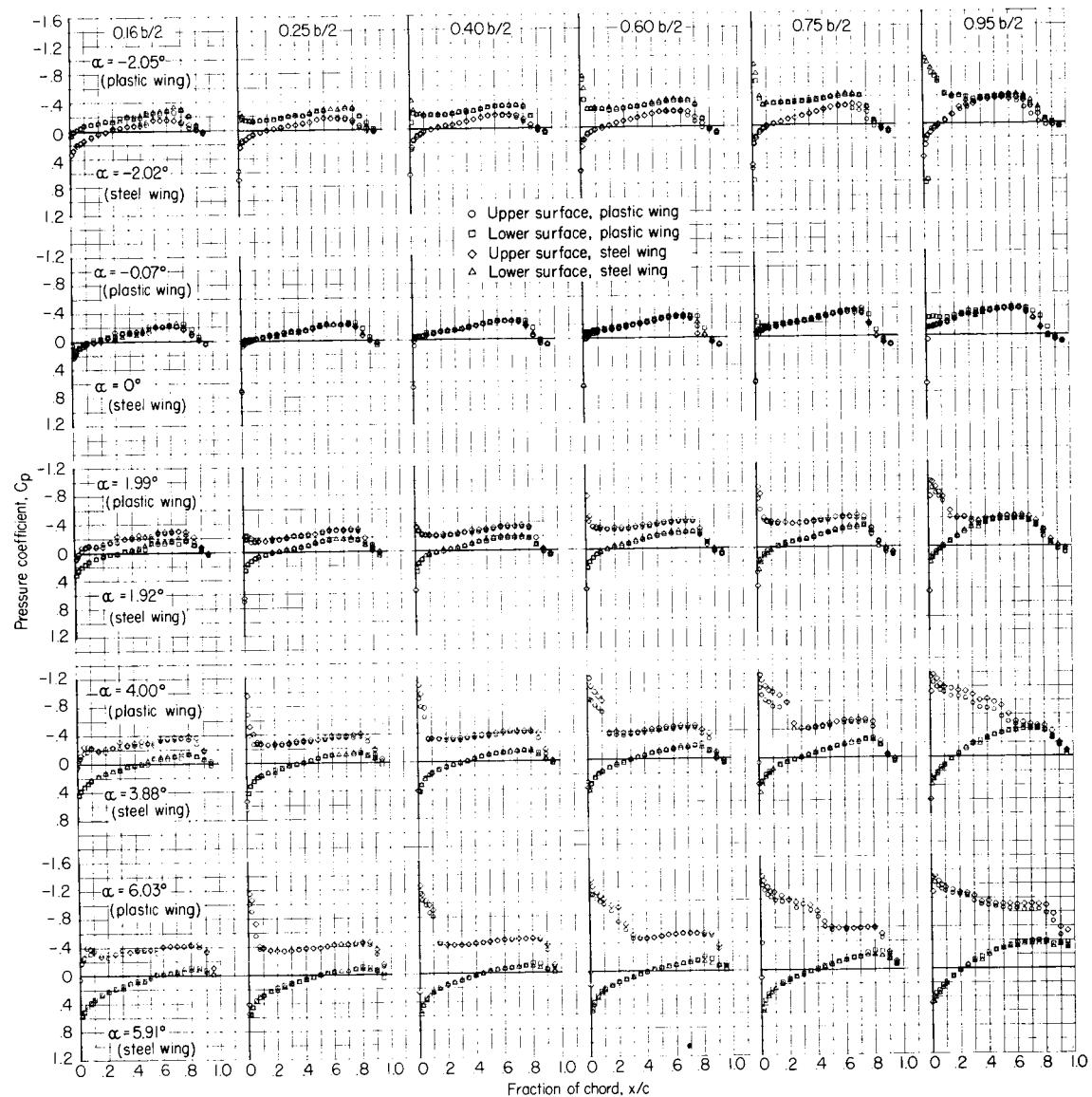
(c) $M = 0.94$.

Figure 4.- Continued.

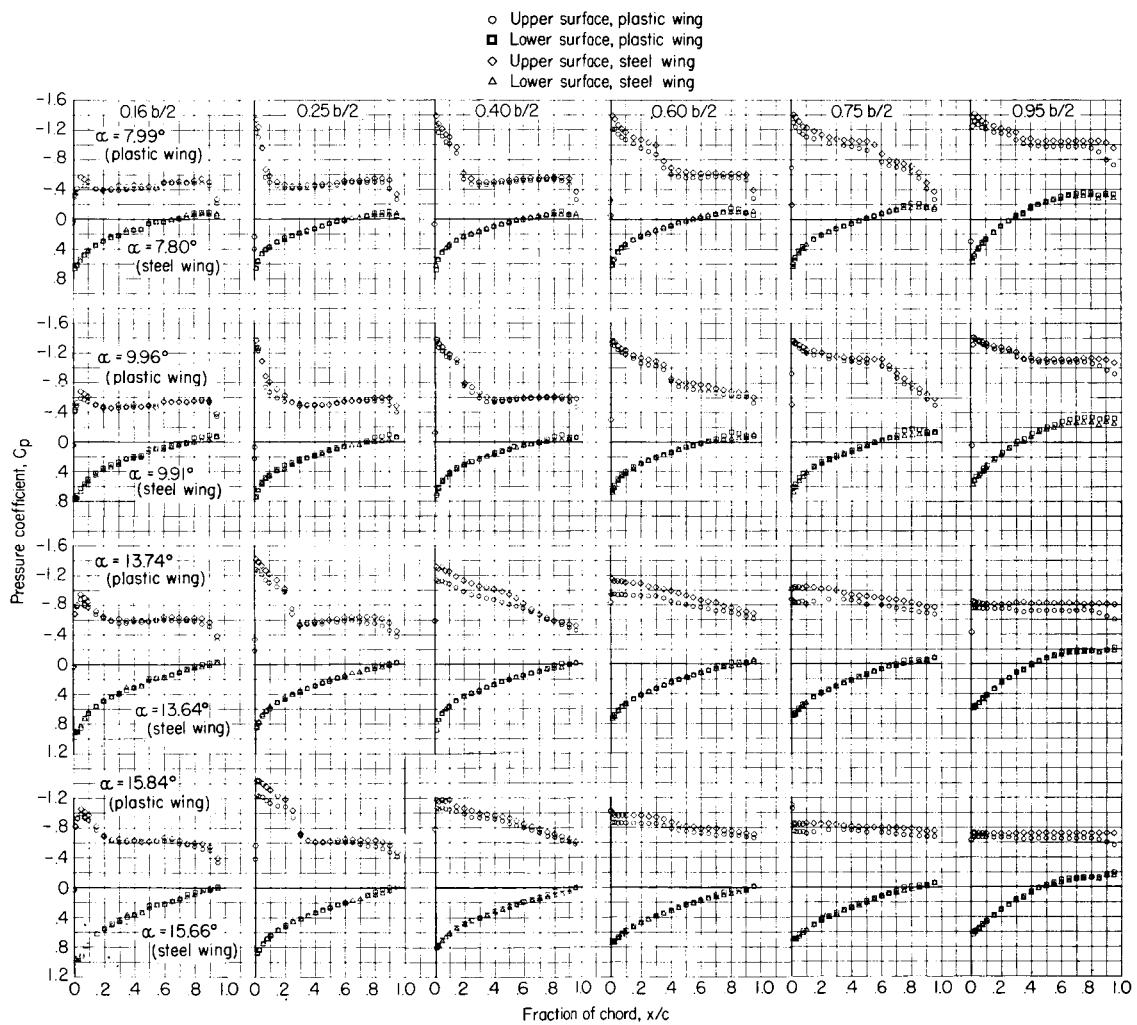
(c) $M = 0.94$, continued.

Figure 4.- Continued.

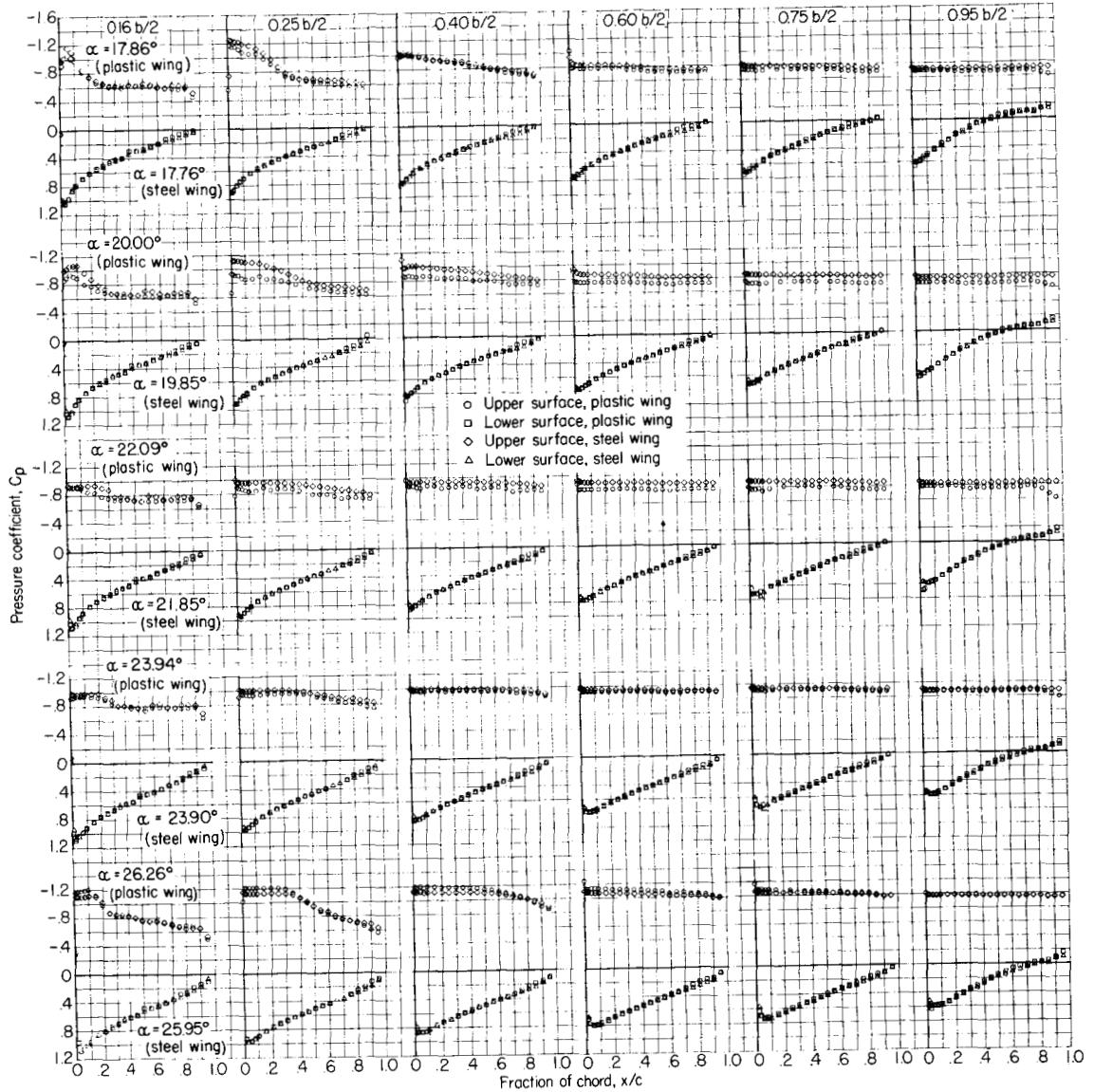
(c) $M = 0.94$, concluded.

Figure 4.- Continued.

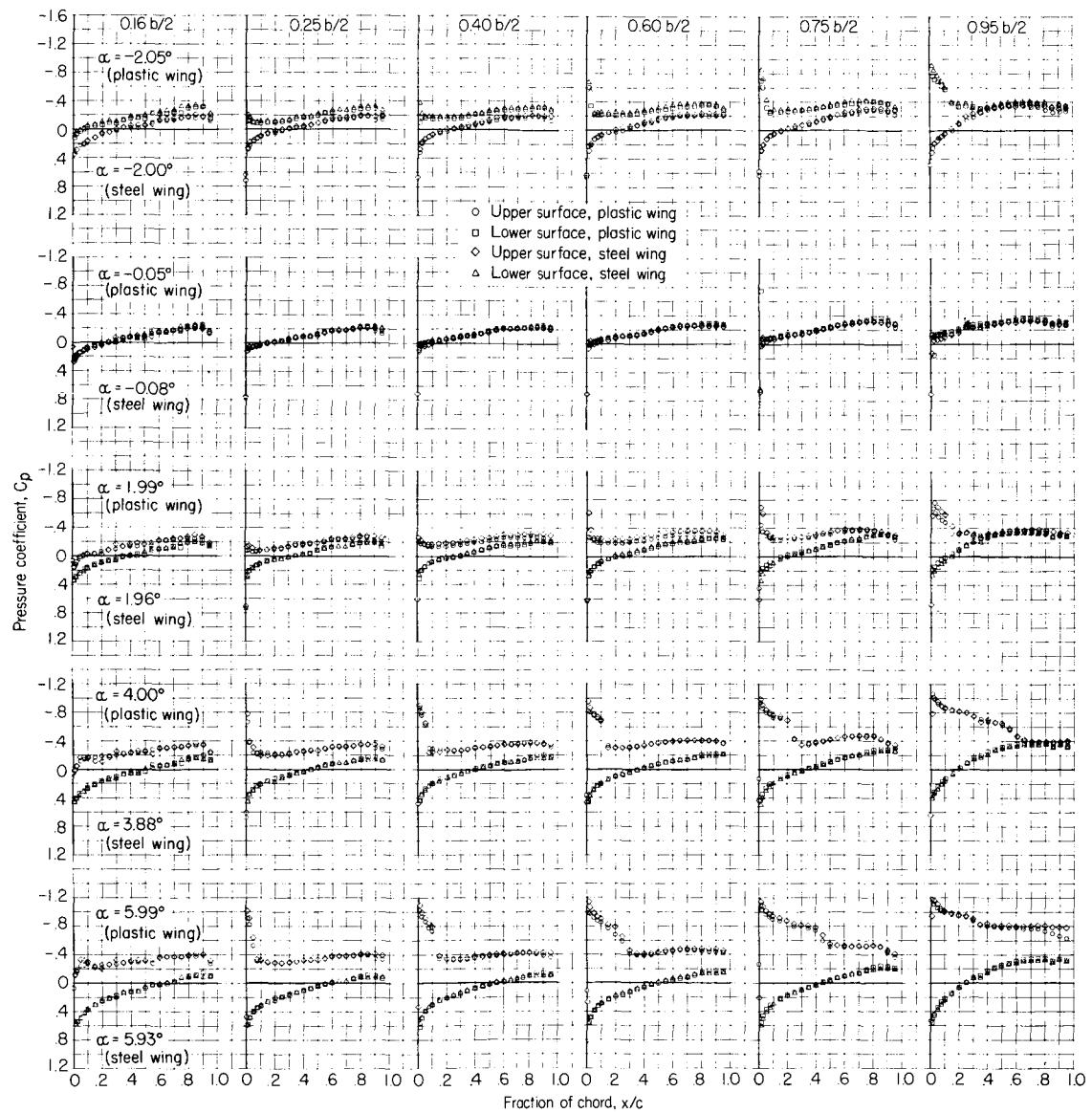
(d) $M = 0.98$.

Figure 4.- Continued.

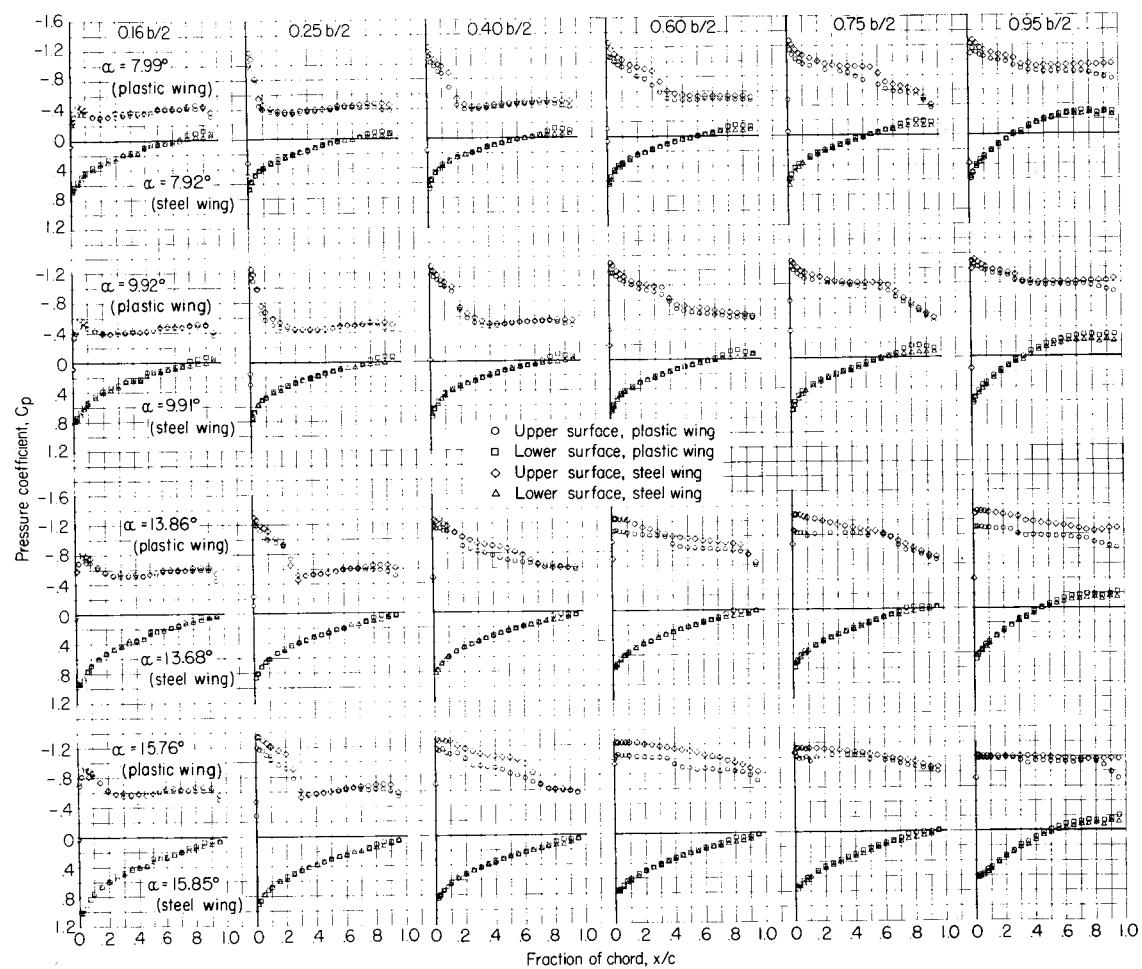
(d) $M = 0.98$, continued.

Figure 4.- Continued.

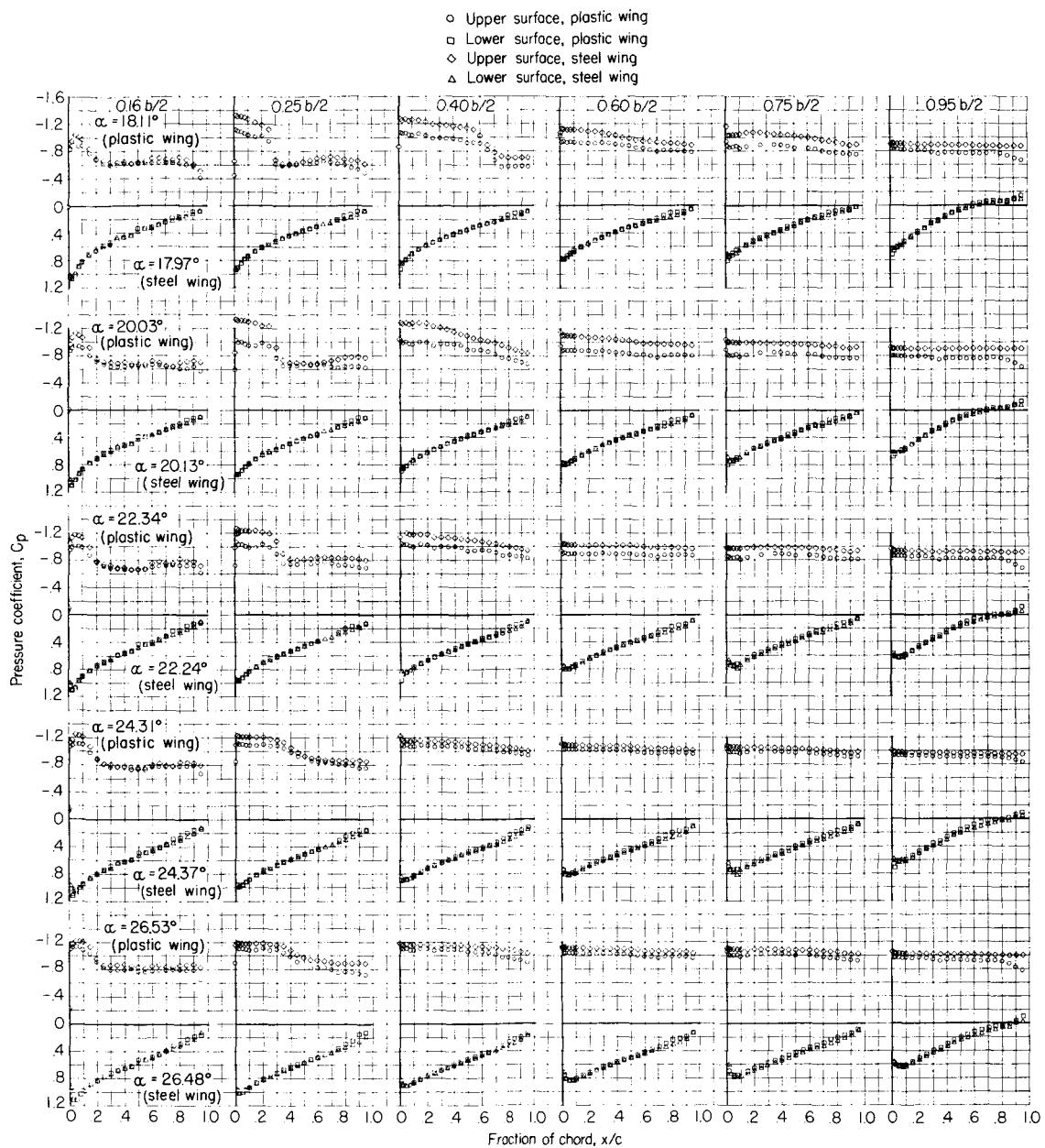
(d) $M = 0.98$, concluded.

Figure 4.- Continued.

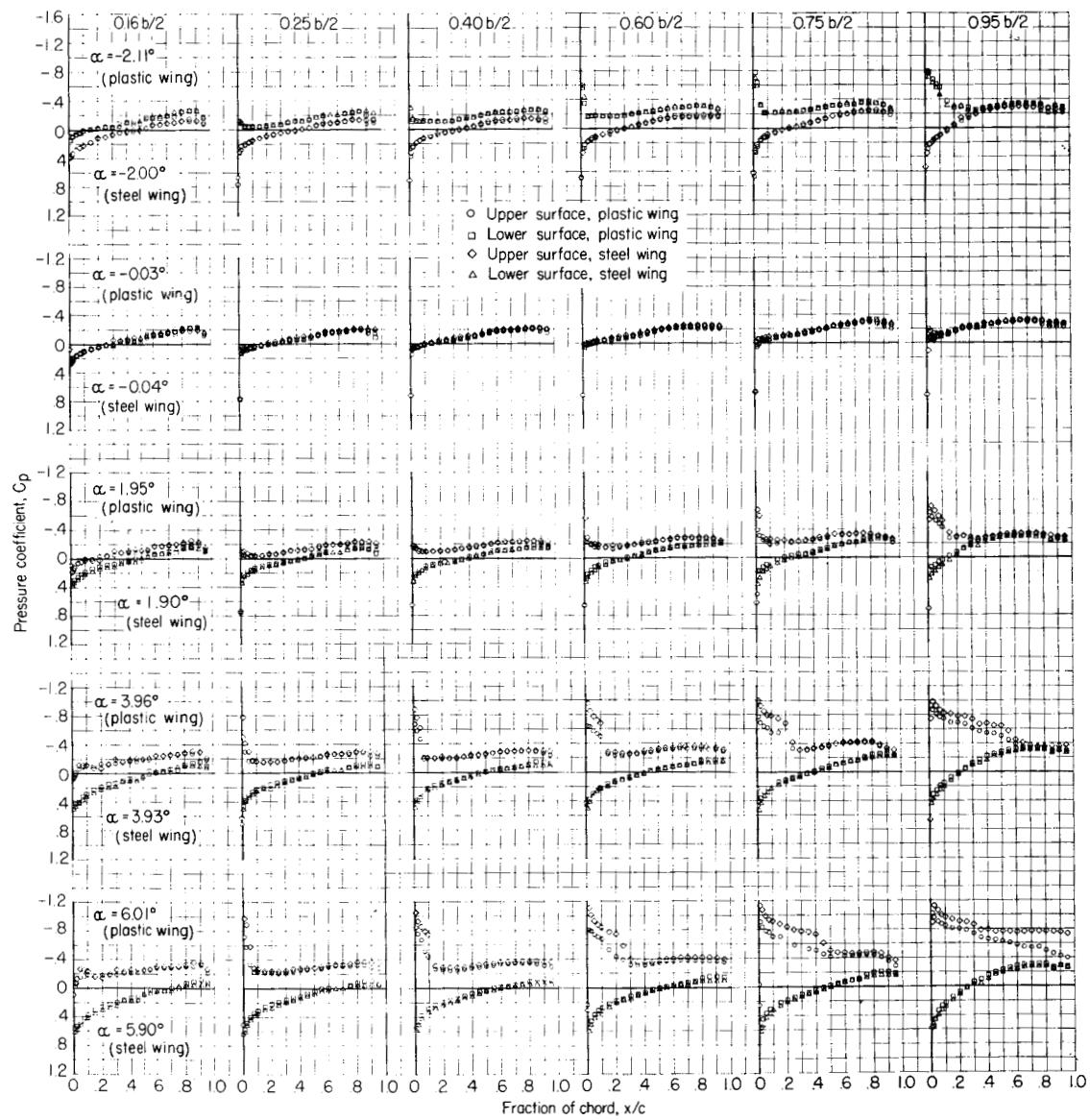
(e) $M = 1.00$.

Figure 4.- Continued.

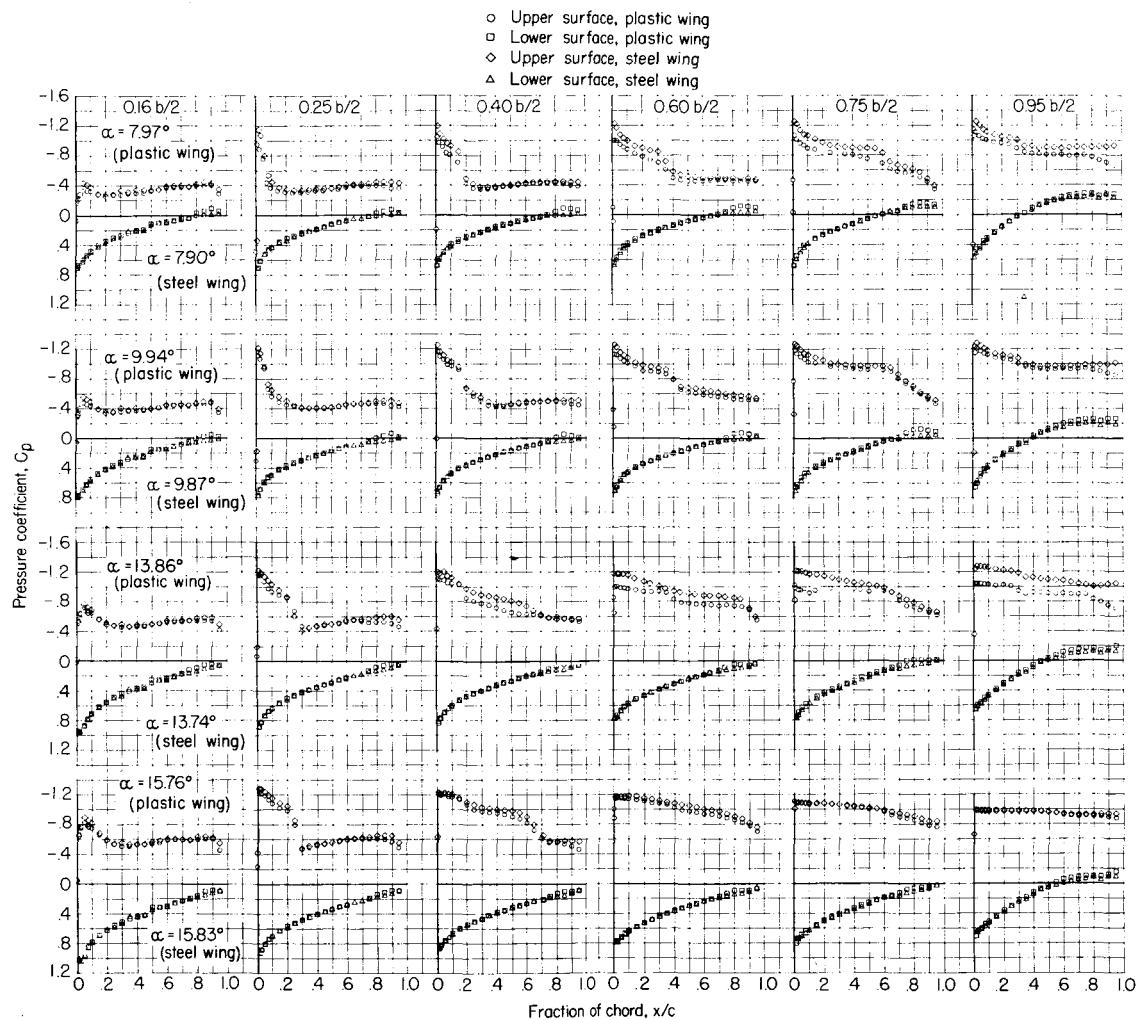
(e) $M = 1.00$, continued.

Figure 4.- Continued.

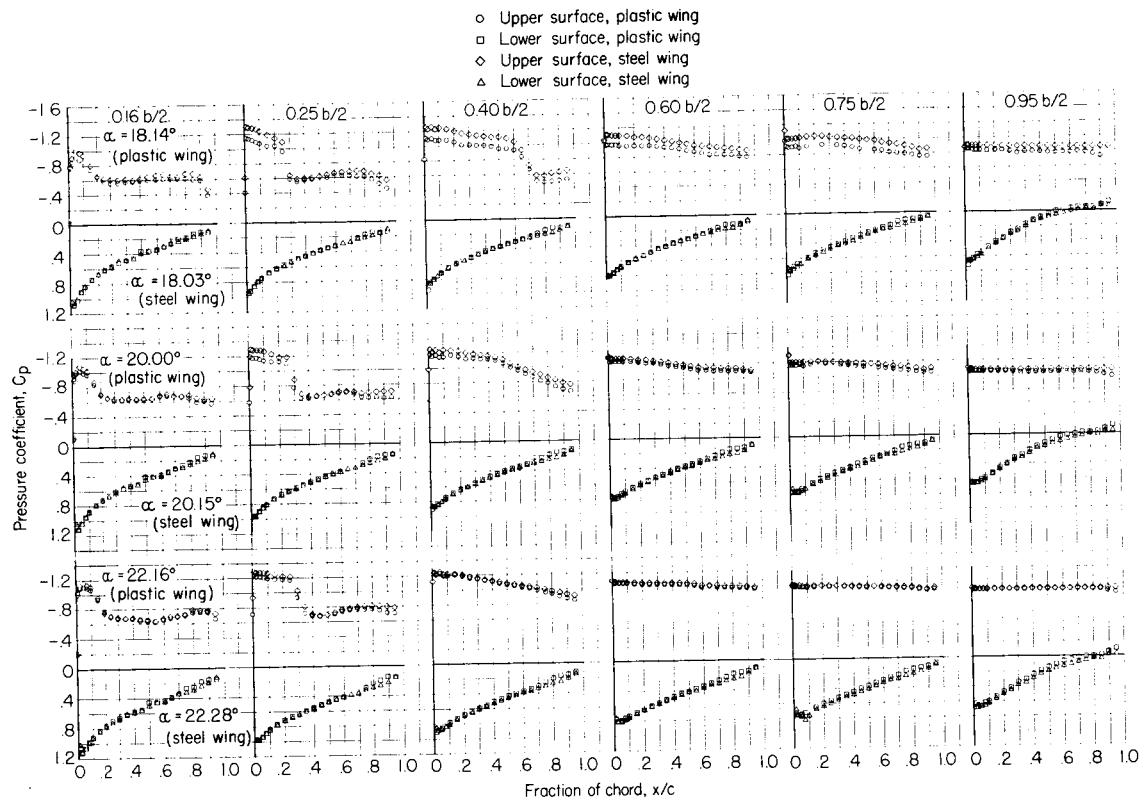
(e) $M = 1.00$, concluded.

Figure 4.-- Continued.

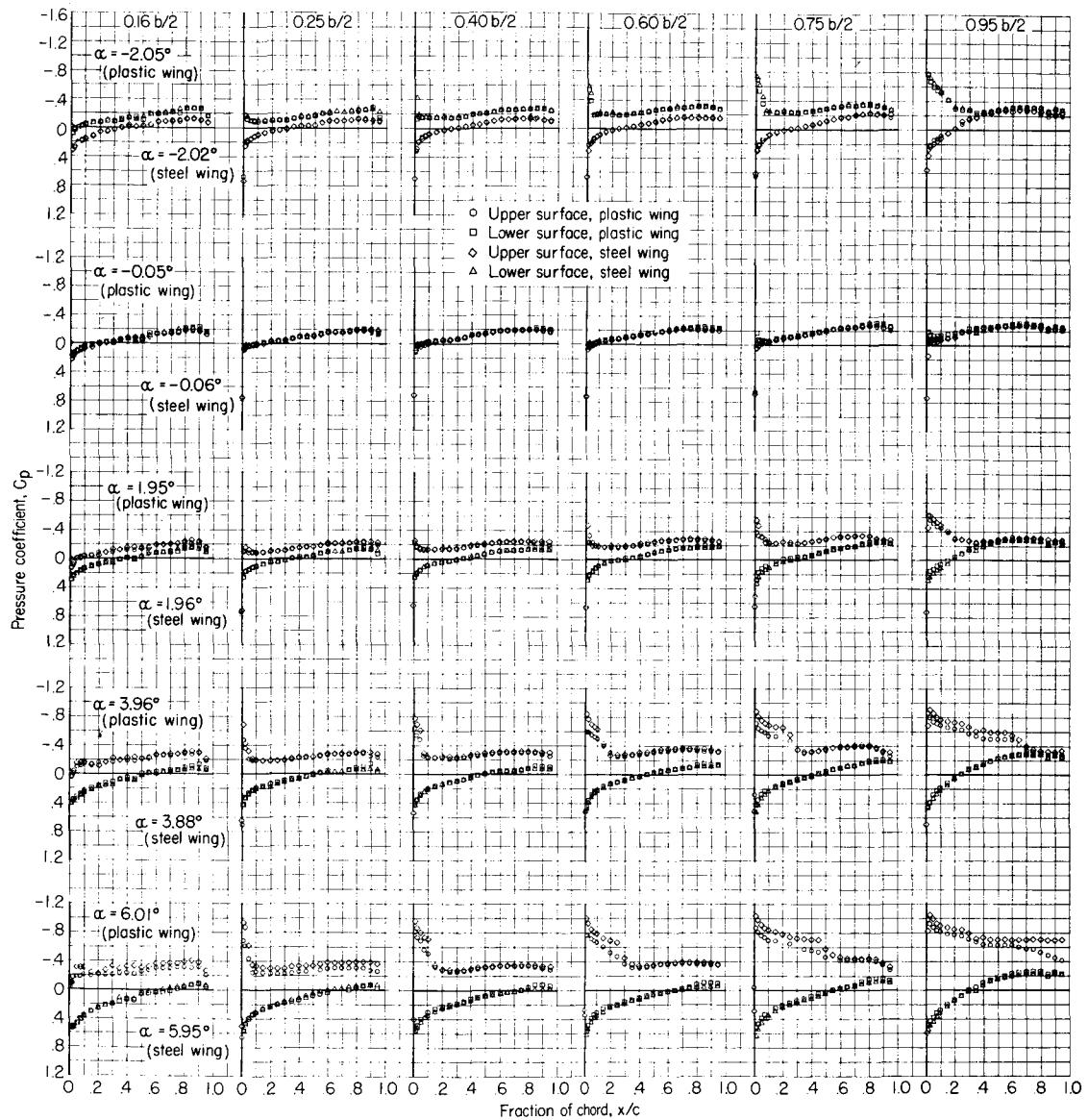
(f) $M = 1.03$.

Figure 4.- Continued.

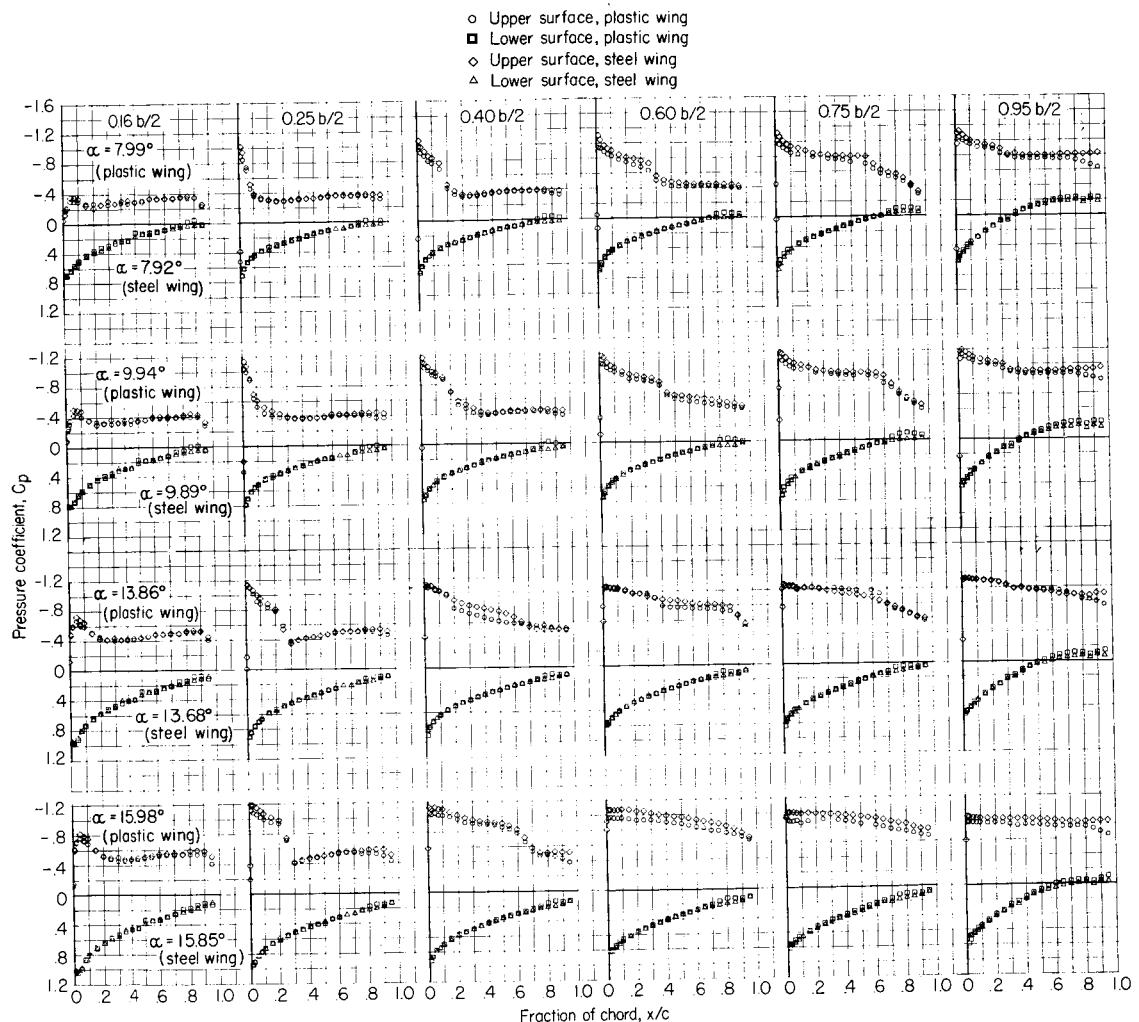
(f) $M = 1.03$, continued.

Figure 4.- Continued.

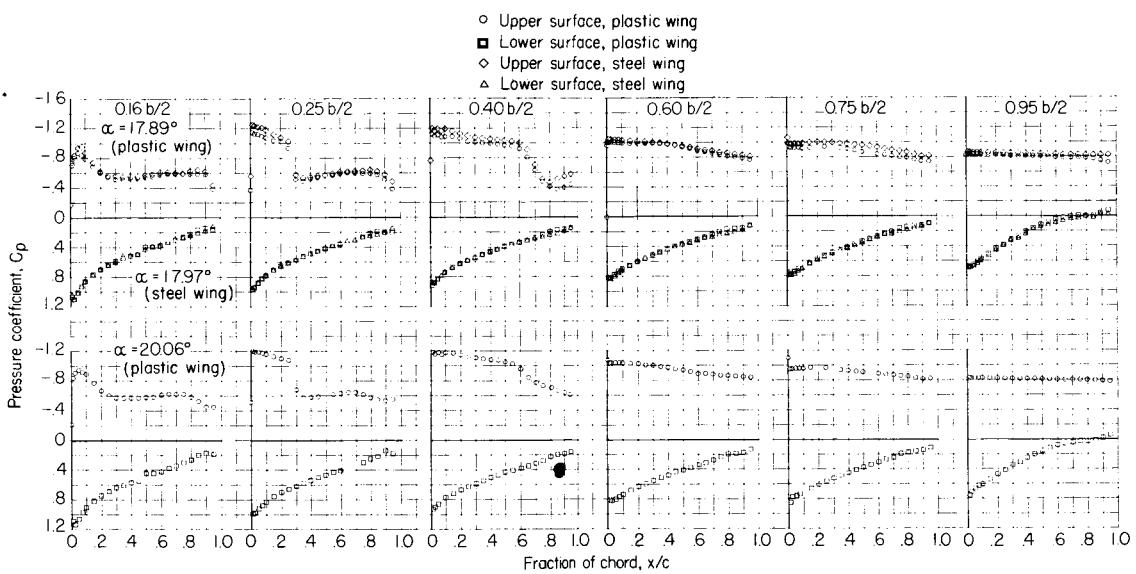
(f) $M = 1.03$, concluded.

Figure 4.- Concluded.

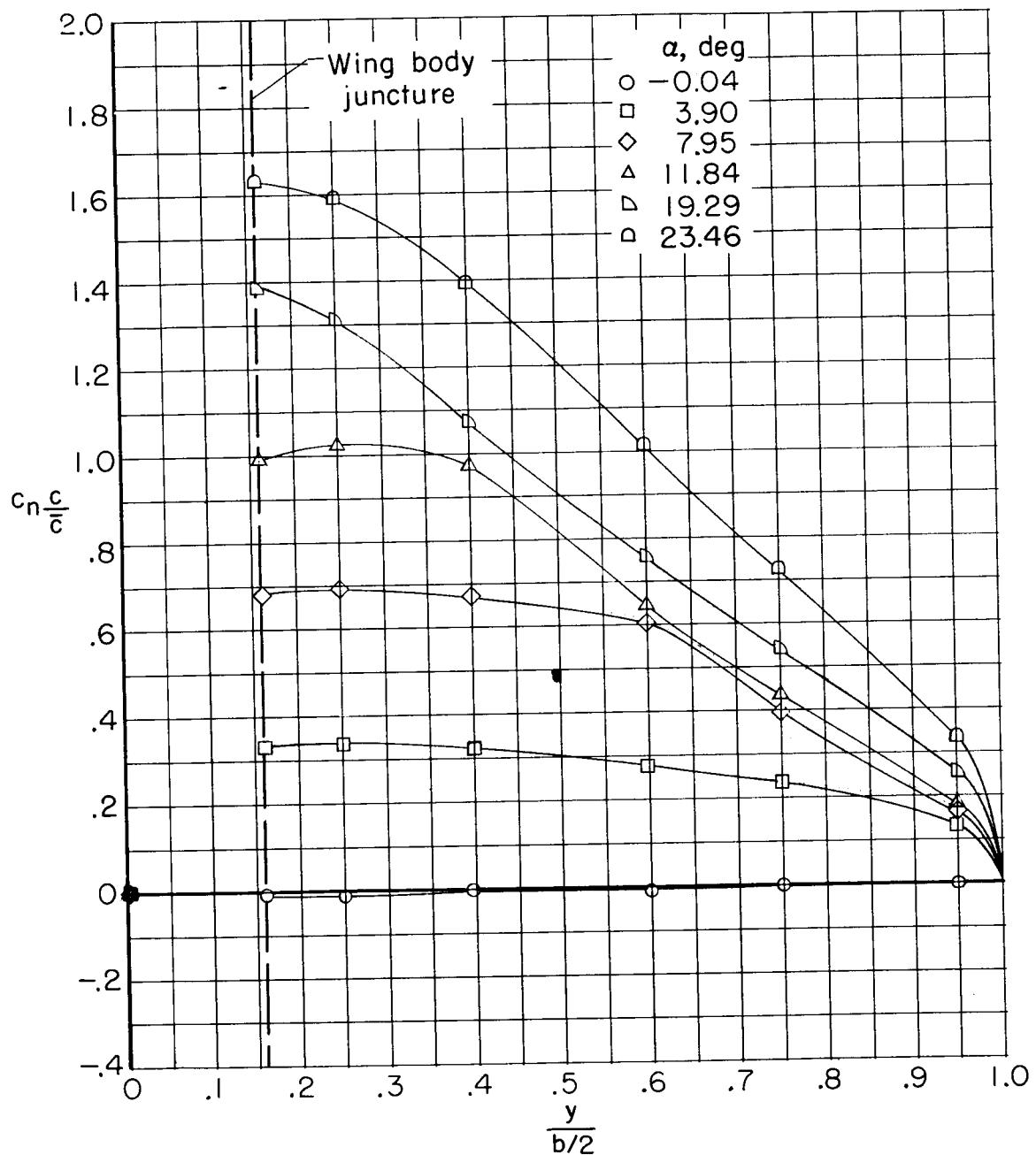
(a) $M = 0.80$.

Figure 5.- Spanwise variation of normal-load parameter for steel wing at various angles of attack and Mach numbers.

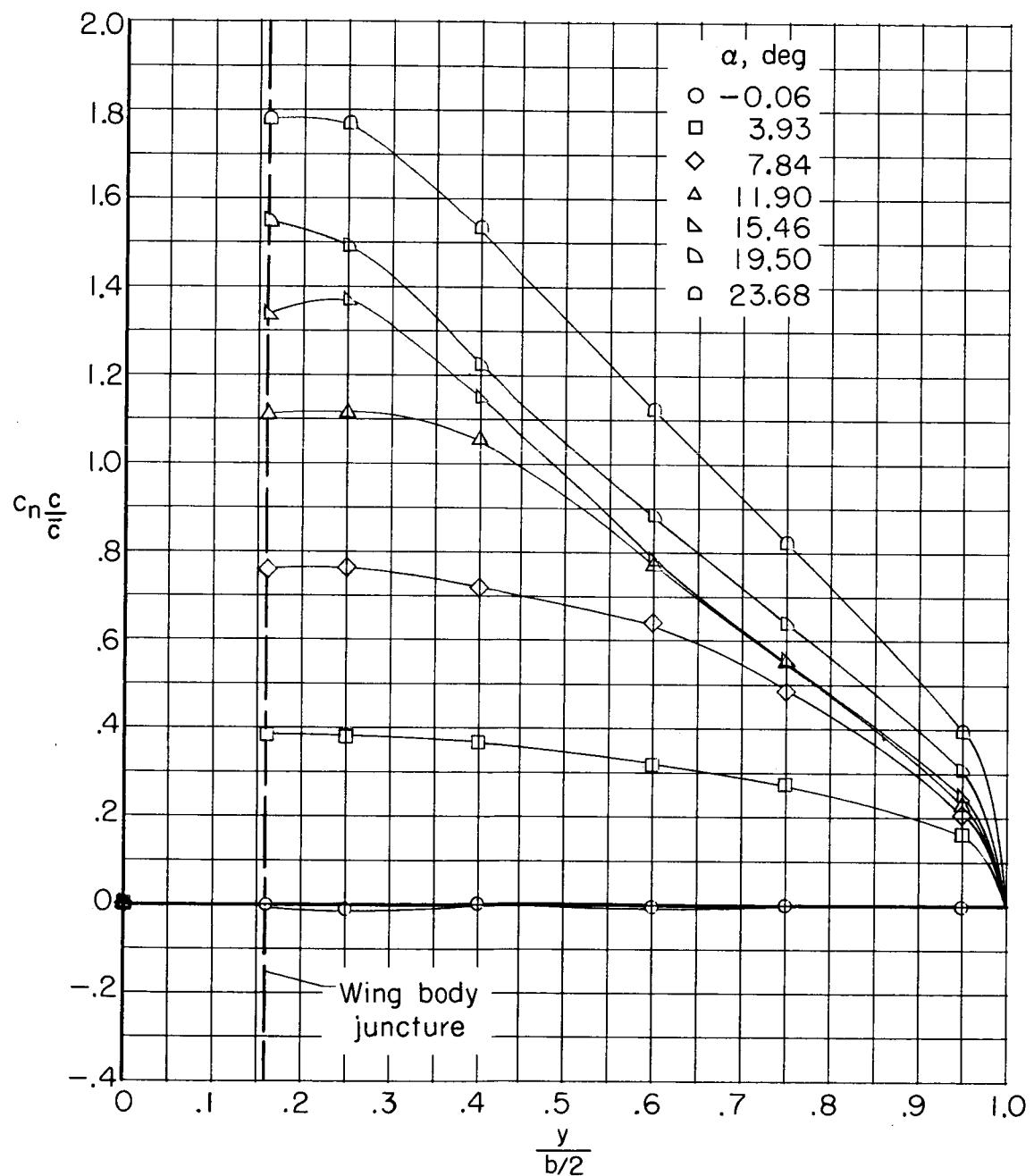
(b) $M = 0.90$.

Figure 5.- Continued.

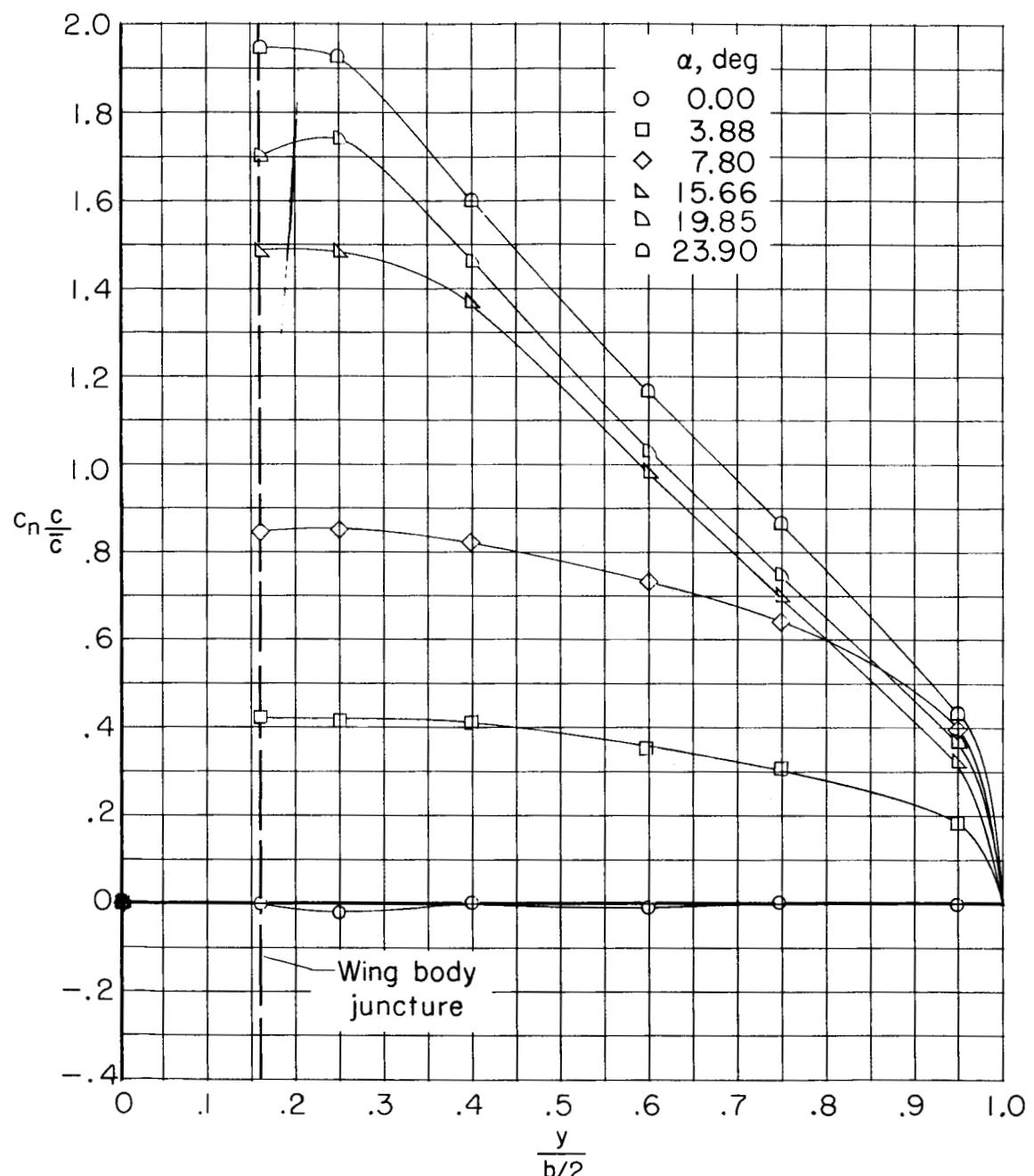
(c) $M = 0.94$.

Figure 5.- Continued.

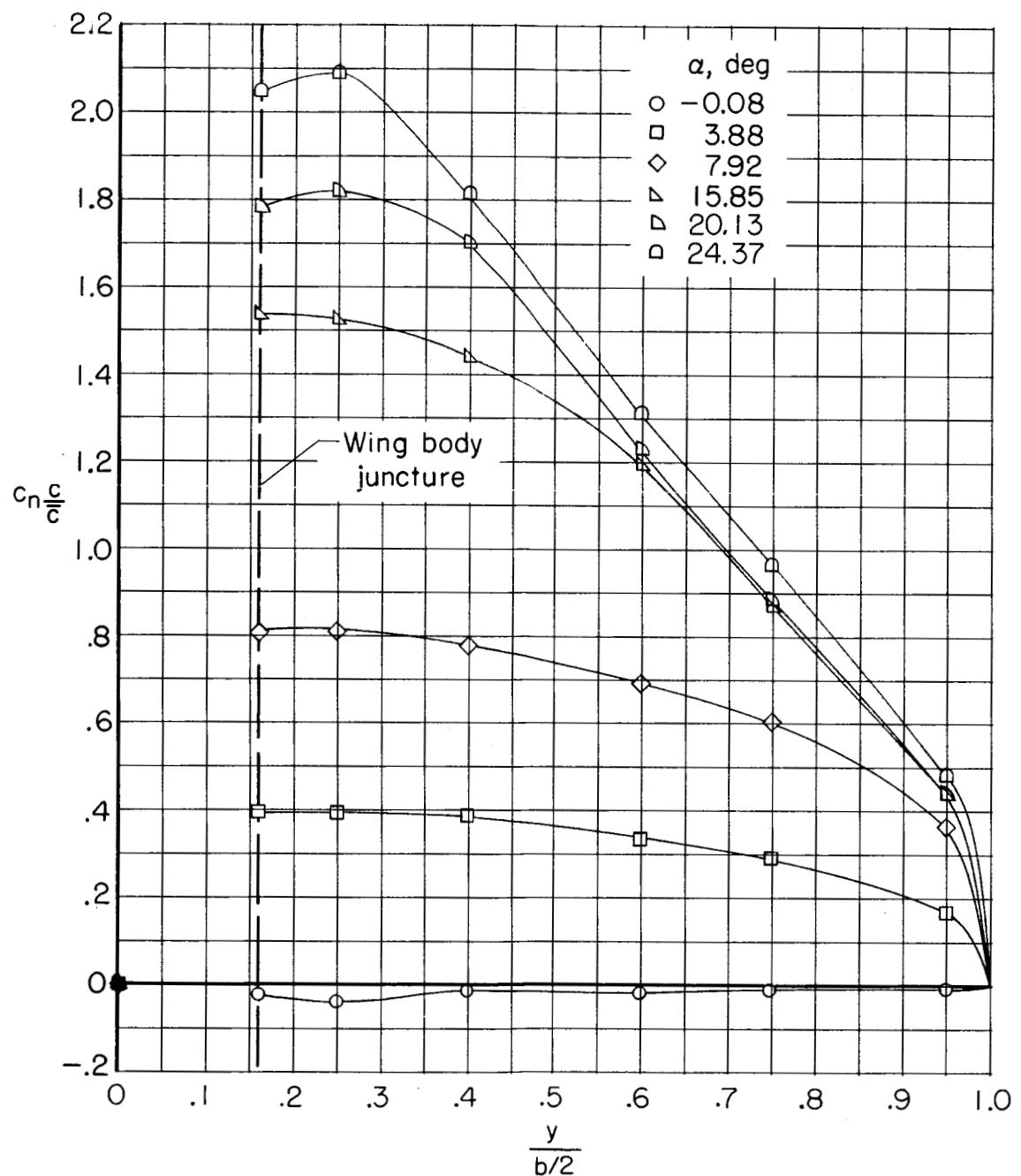
(d) $M = 0.98$.

Figure 5.- Continued.

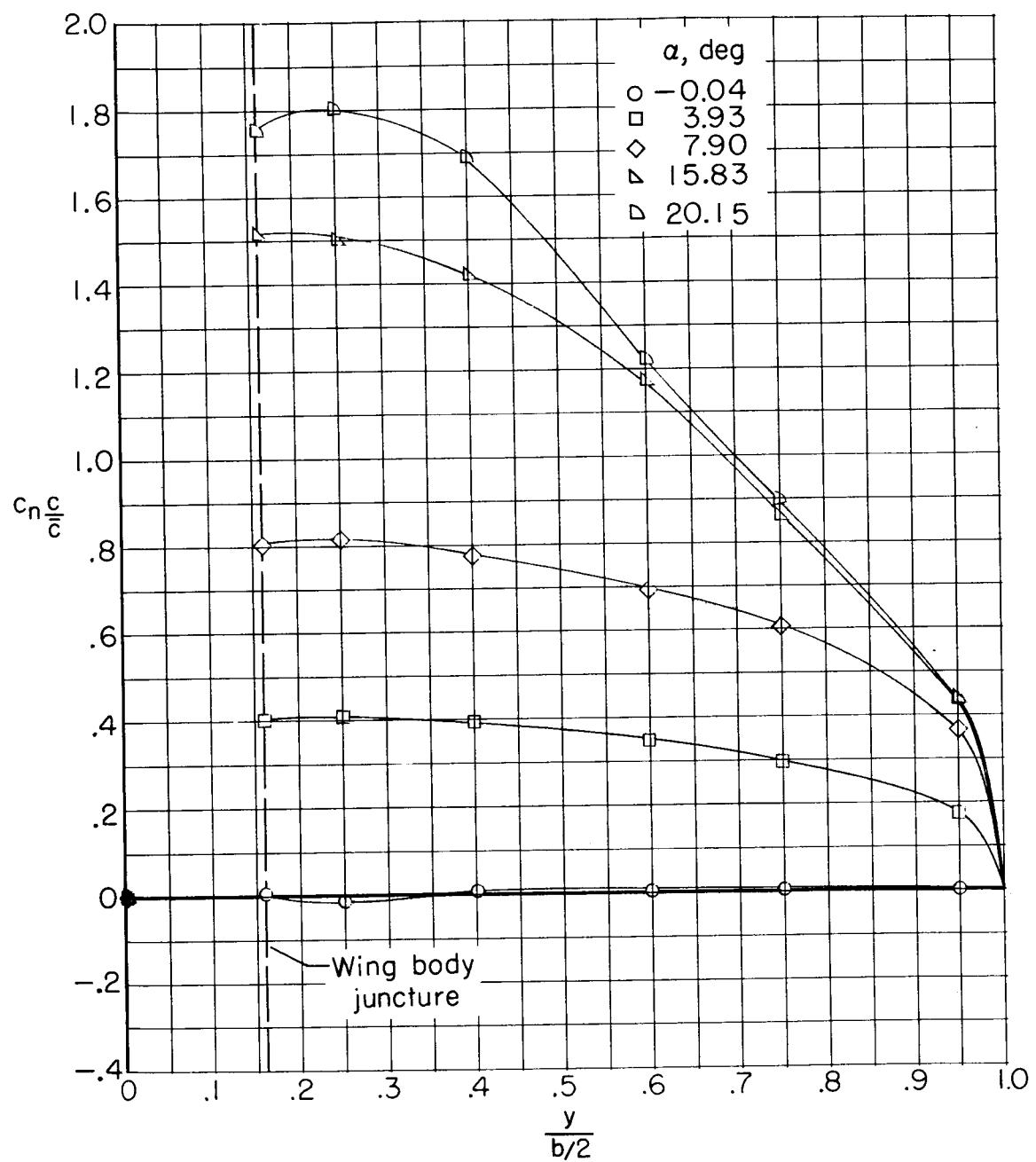
(e) $M = 1.00.$

Figure 5.- Continued.

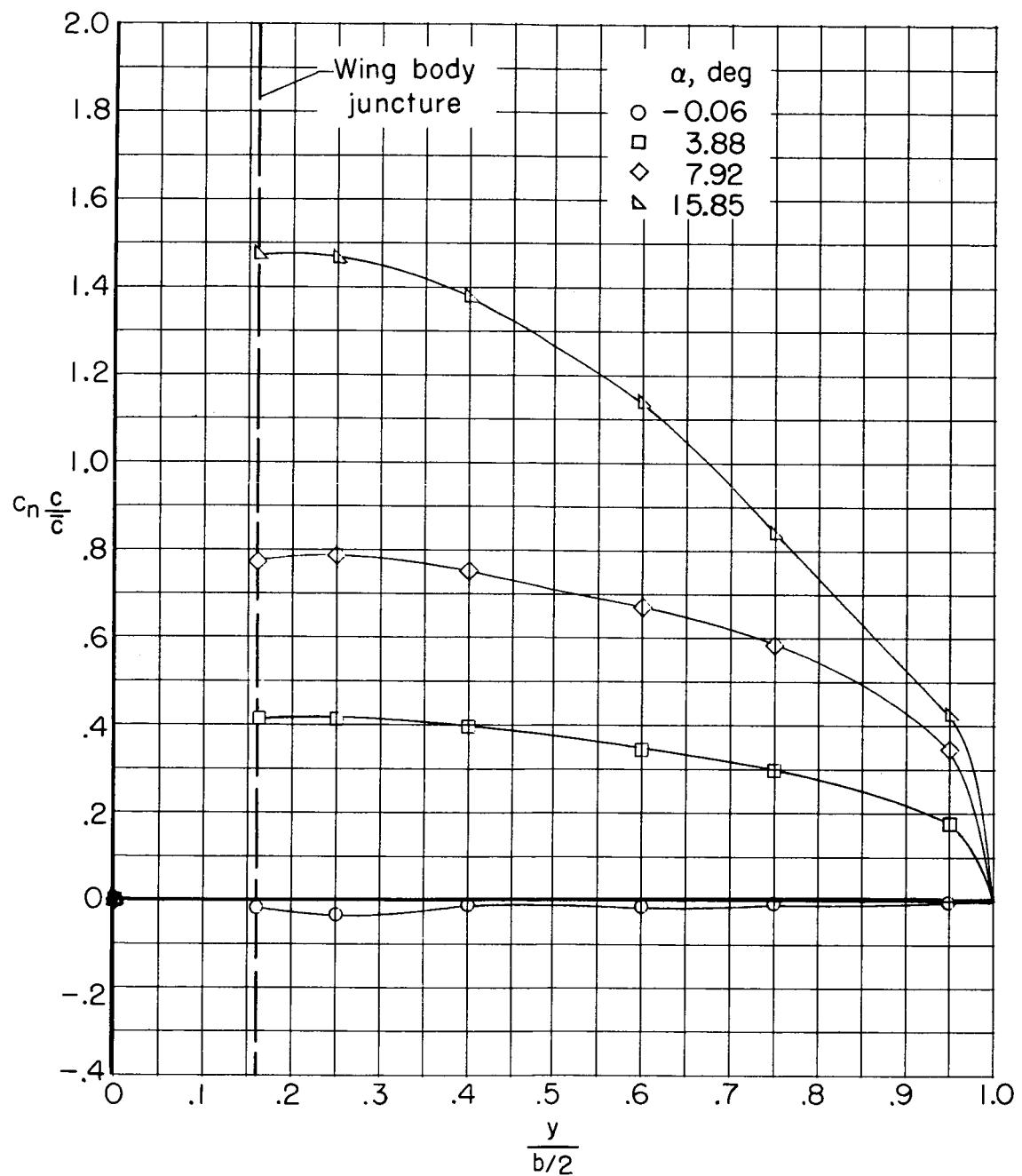
(f) $M = 1.03$.

Figure 5.- Concluded.

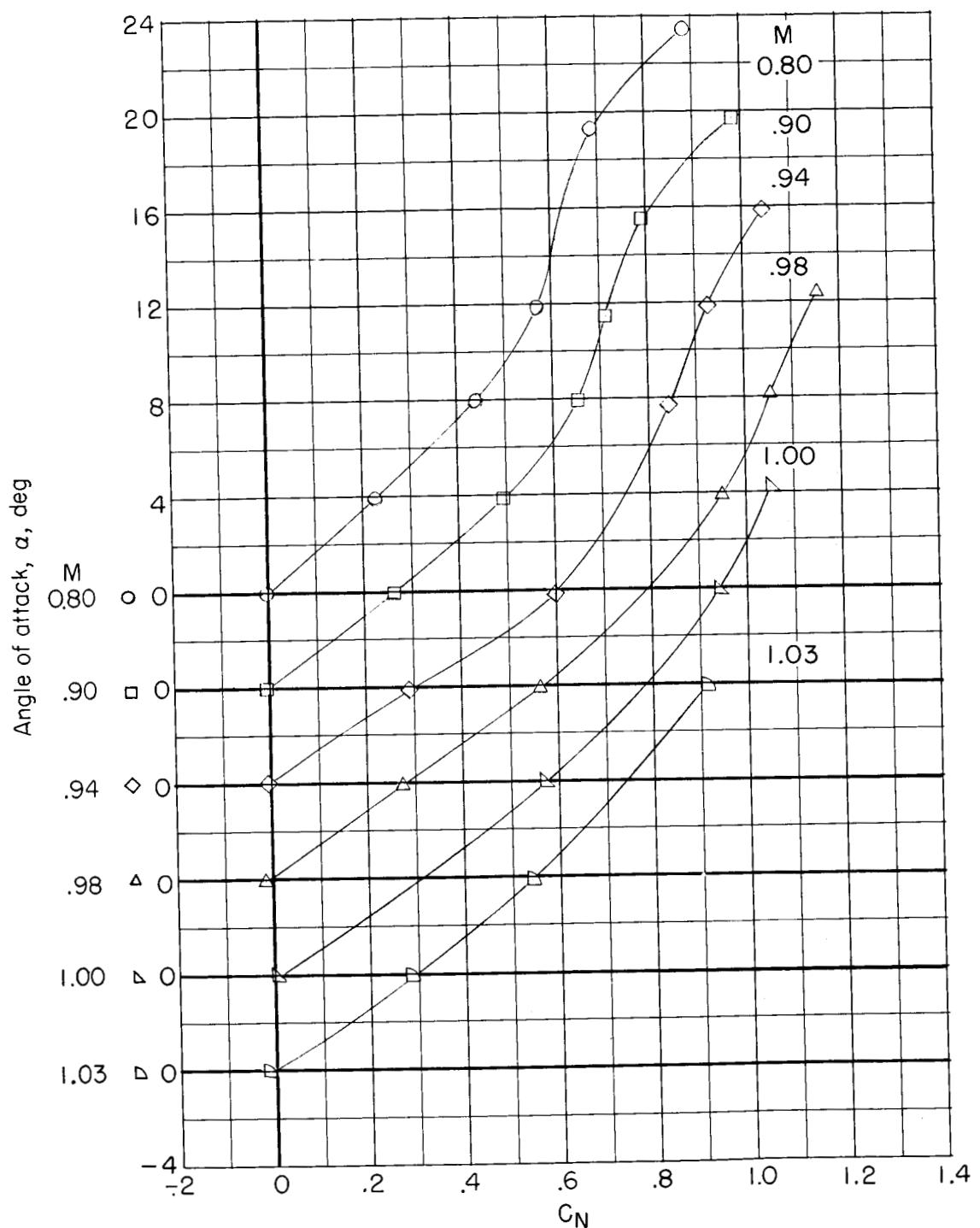


Figure 6.- Variation of angle of attack with wing normal-force coefficient for several Mach numbers. Steel wing.

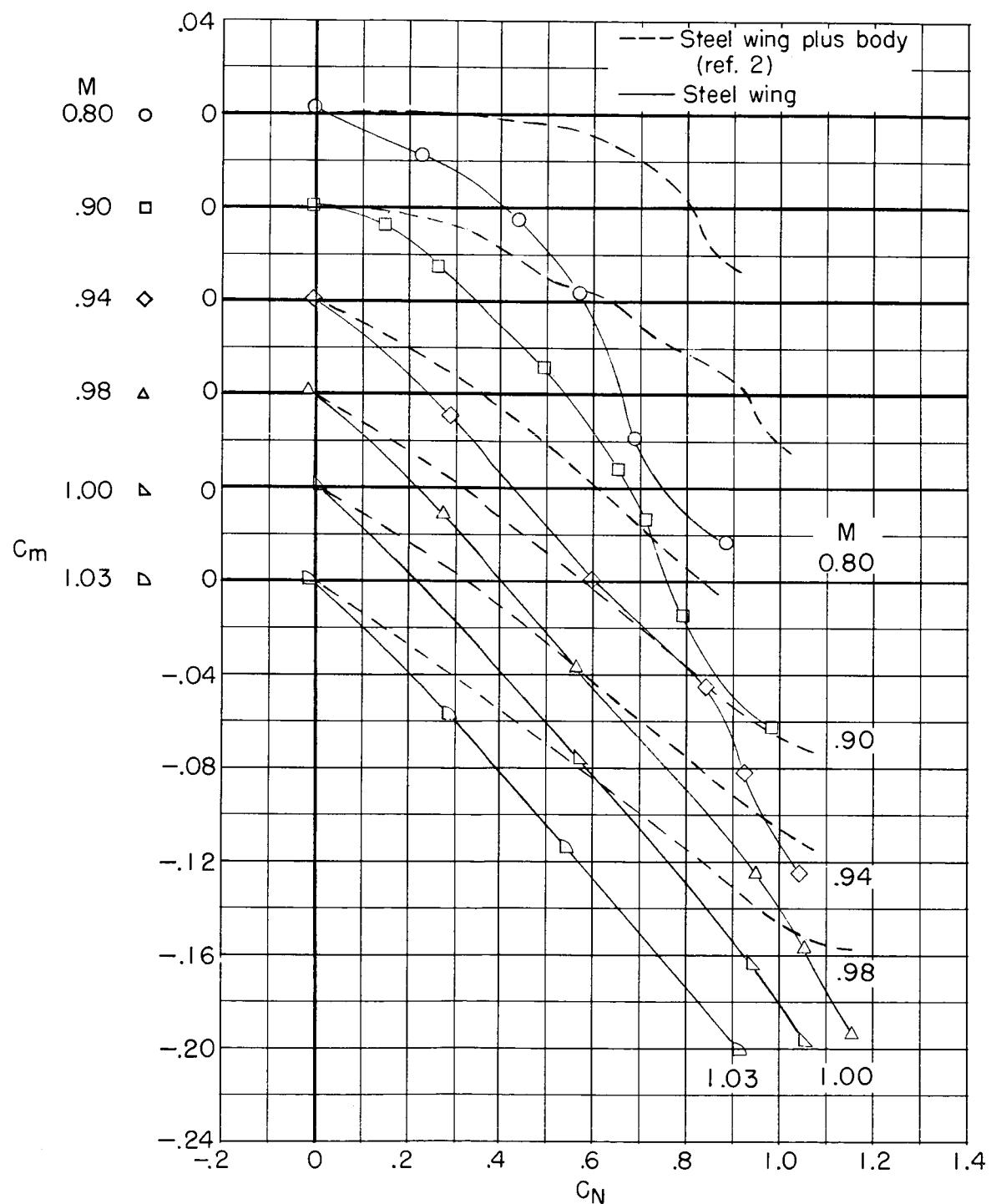


Figure 7.- Variation of wing pitching-moment coefficient with wing normal-force coefficient for several Mach numbers. Steel wing.

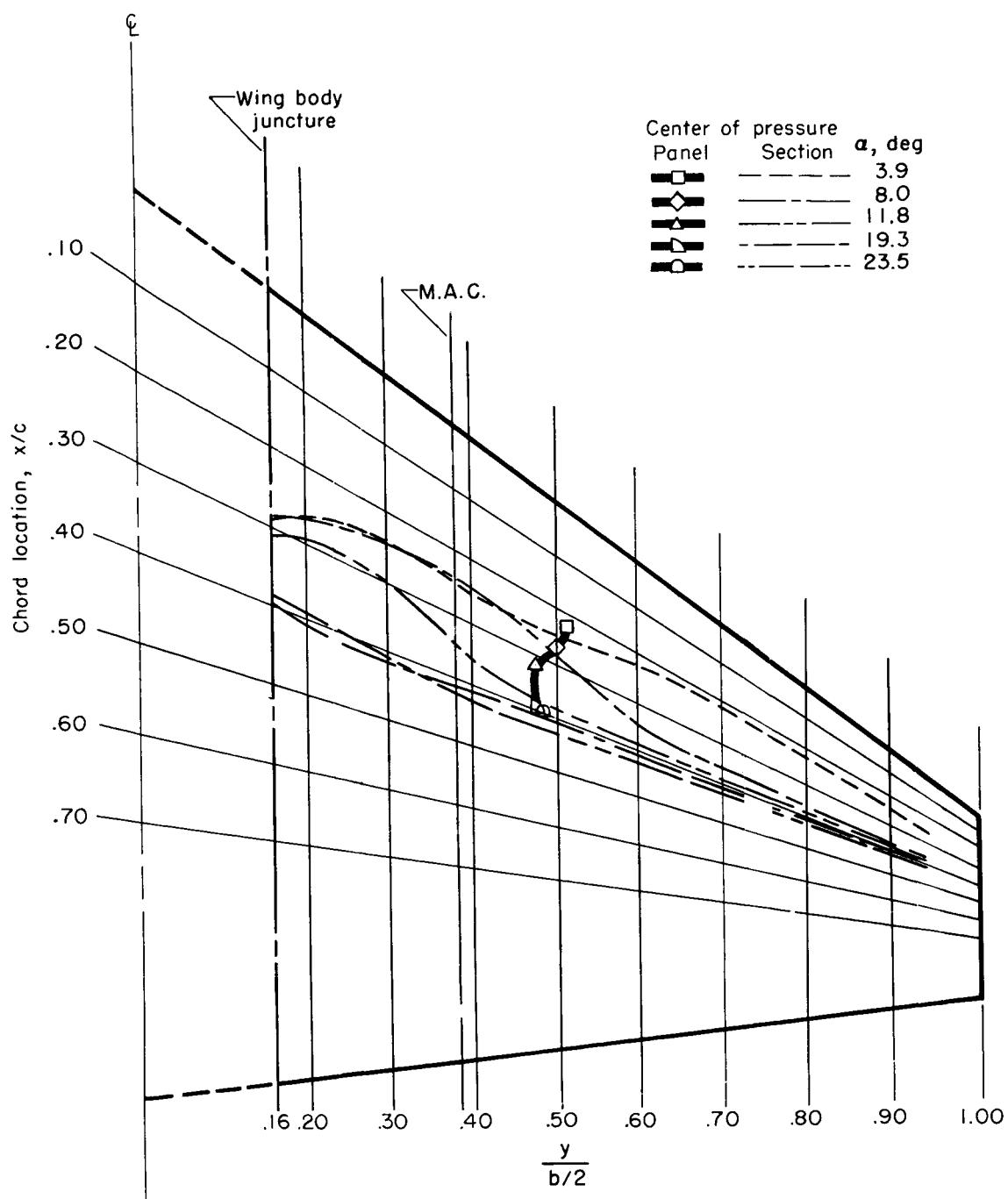
(a) $M = 0.80.$

Figure 8.- Variation of center-of-pressure location for wing panel and for local sections with angle of attack for several Mach numbers.
Steel wing.

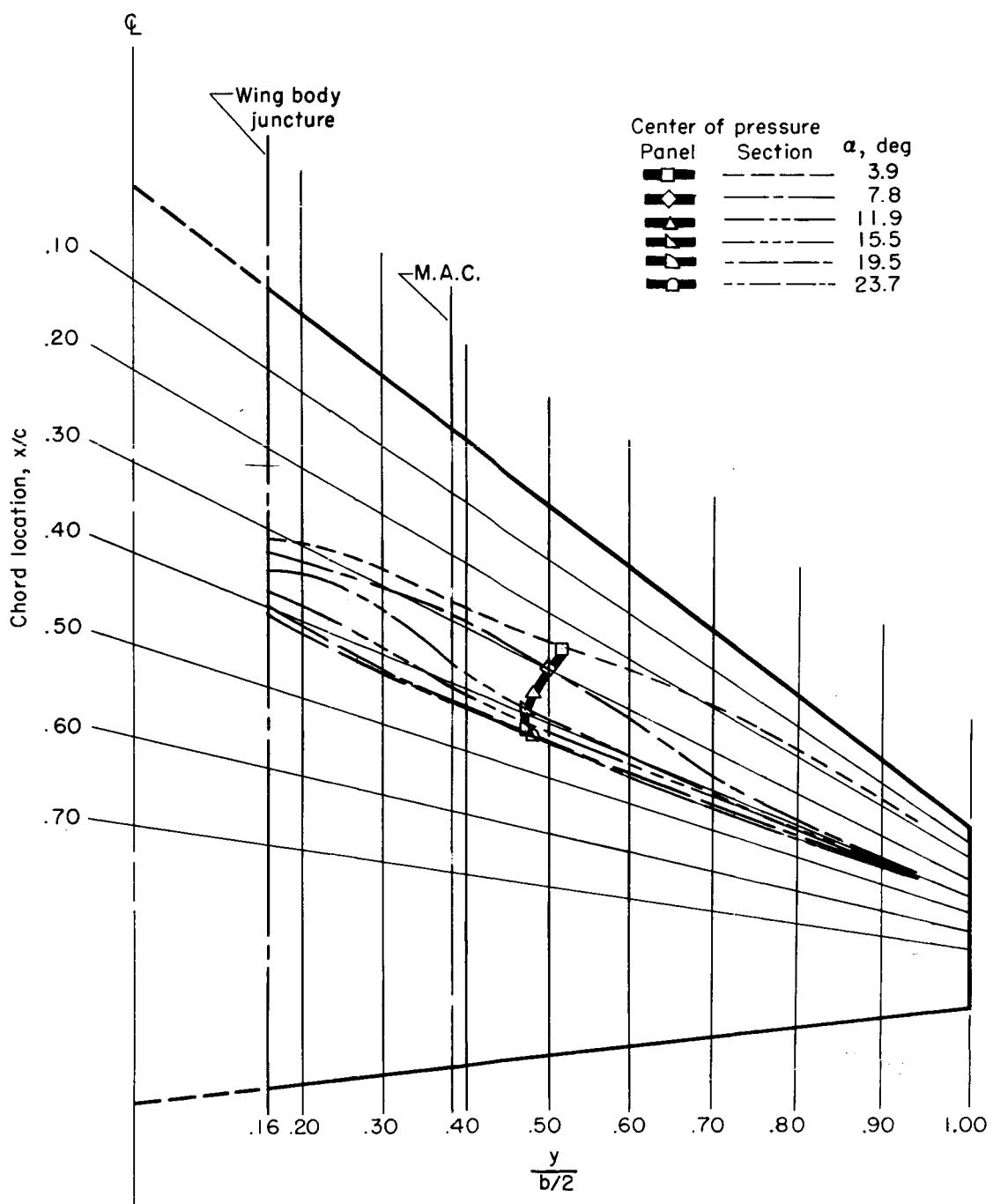
(b) $M = 0.90.$

Figure 8.- Continued.

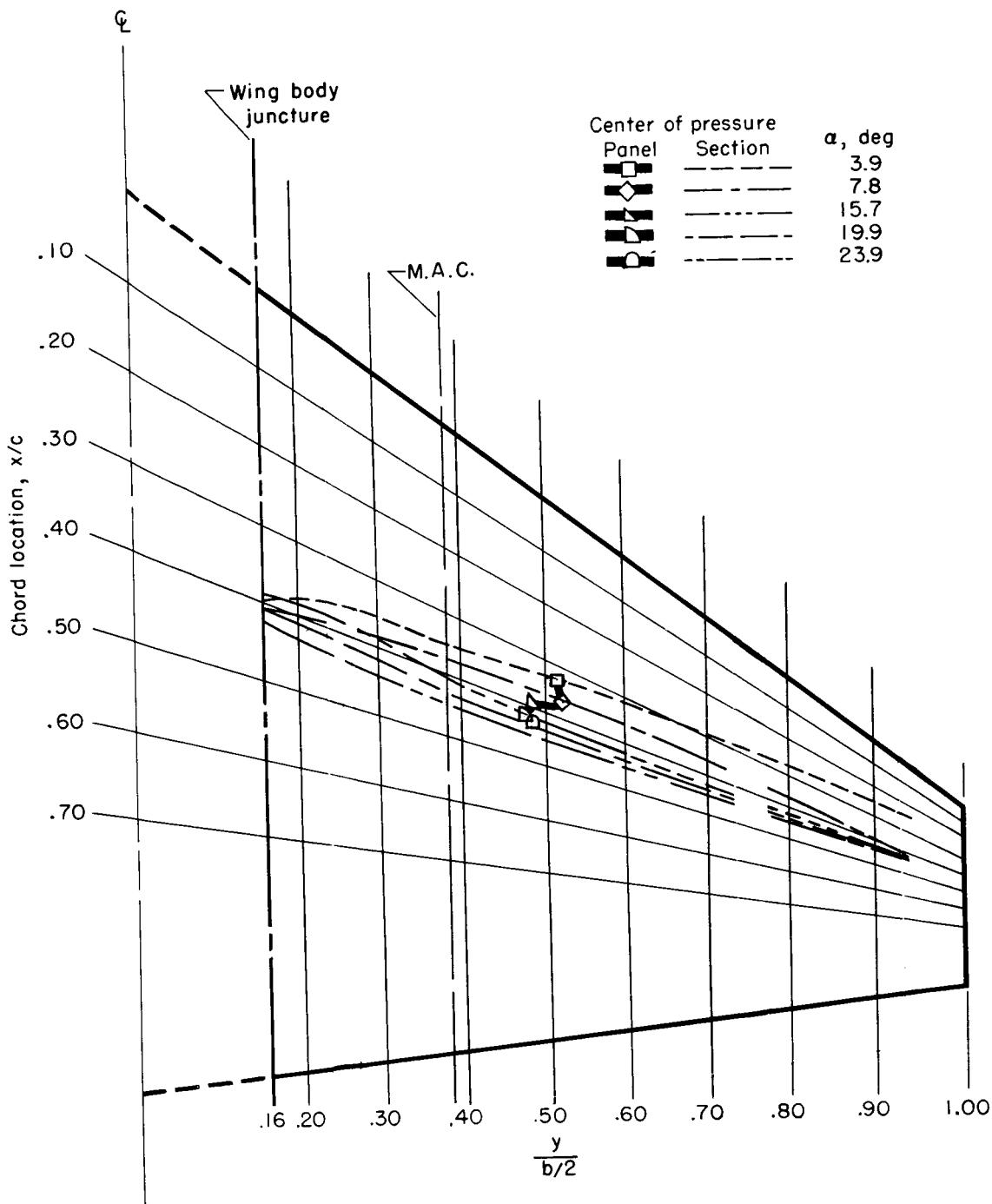
(c) $M = 0.94.$

Figure 8.- Continued.

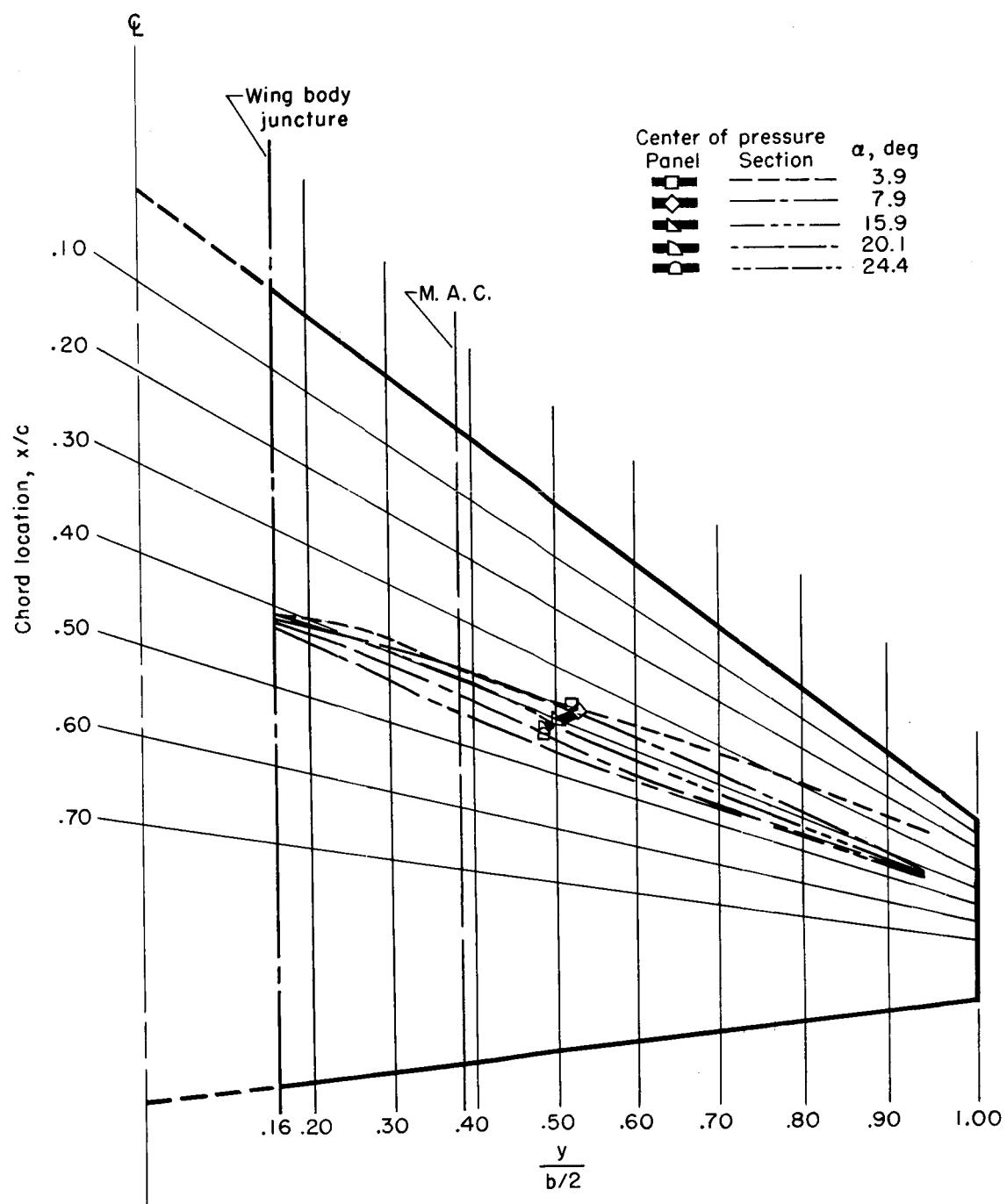
(d) $M = 0.98$.

Figure 8.- Continued.

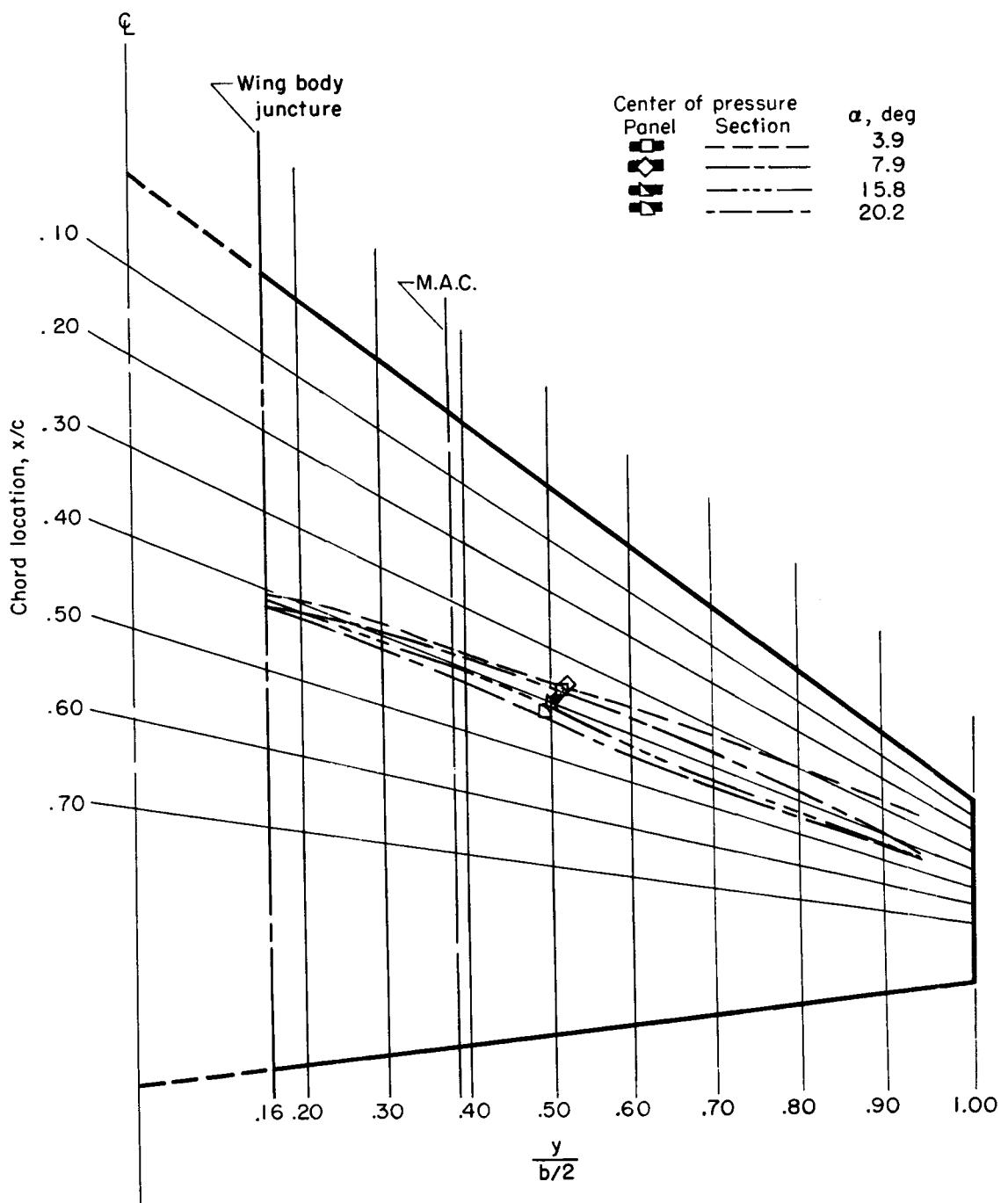
(e) $M = 1.00.$

Figure 8.- Continued.

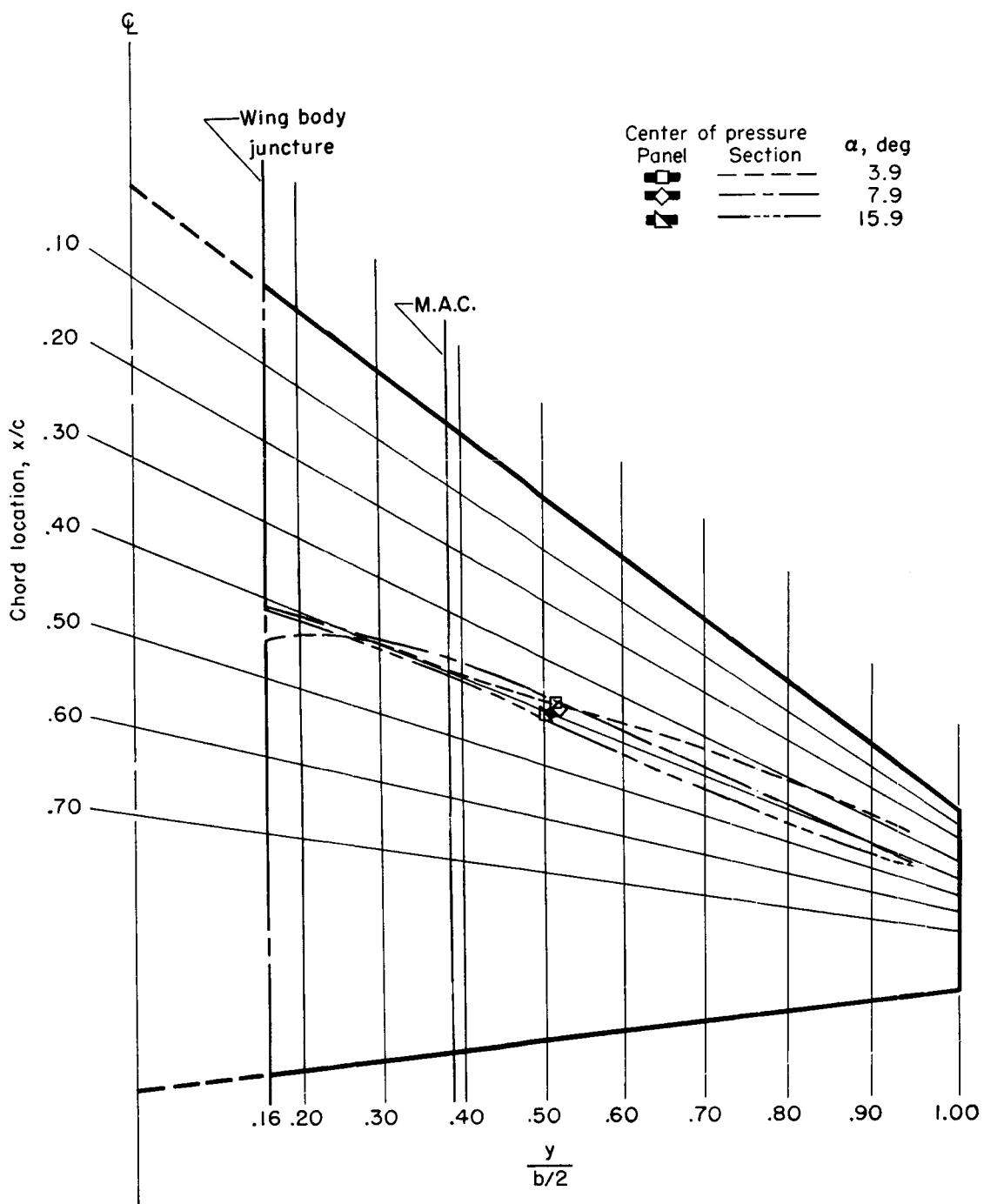
(f) $M = 1.03$.

Figure 8.- Concluded.

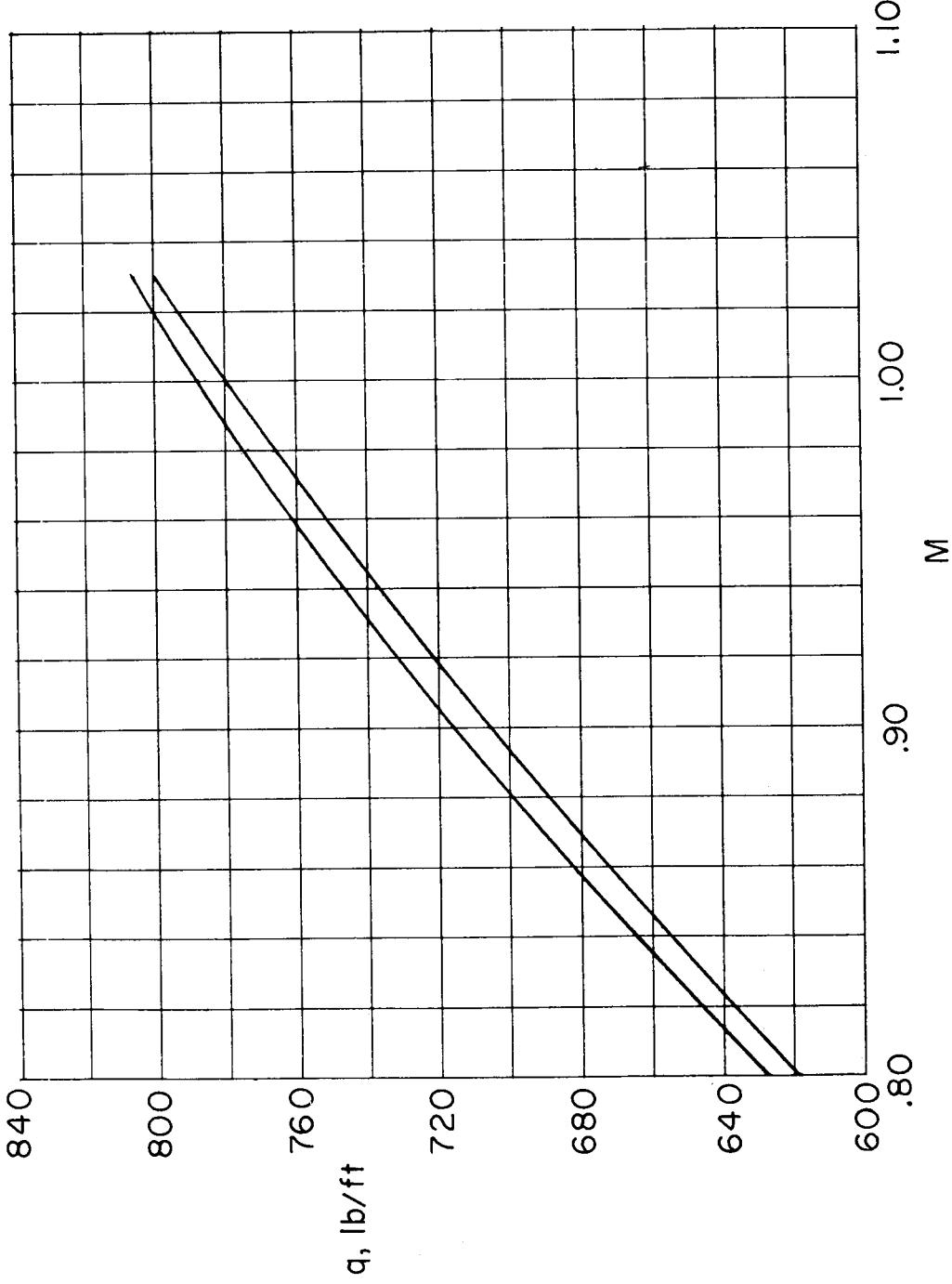


Figure 9.- Range of dynamic pressures for both steel and plastic wings for these tests.

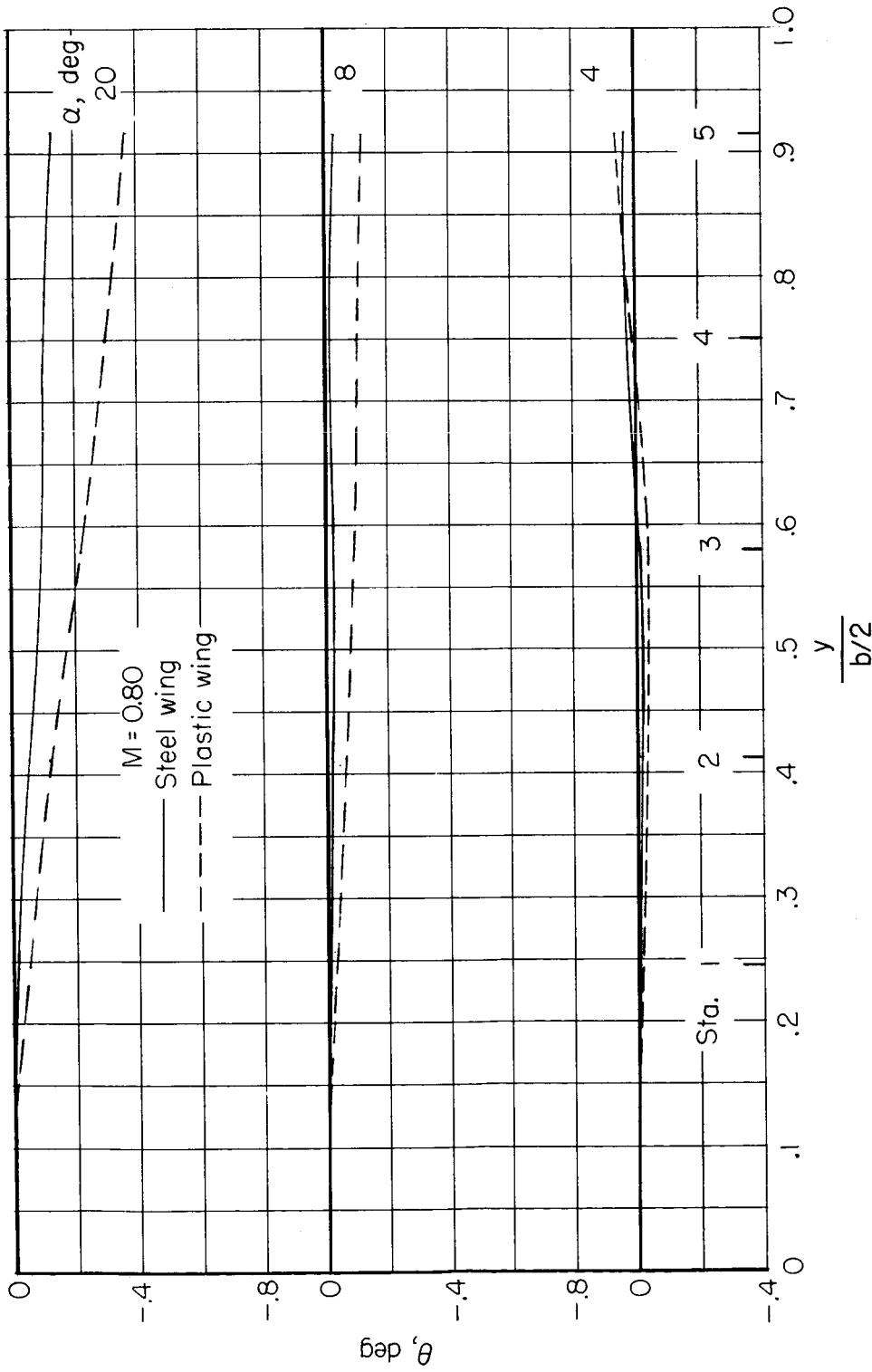


Figure 10.- Comparison of the calculated twist distribution due to experimental aerodynamic forces and moments, measured parallel to the angle-of-attack plane.

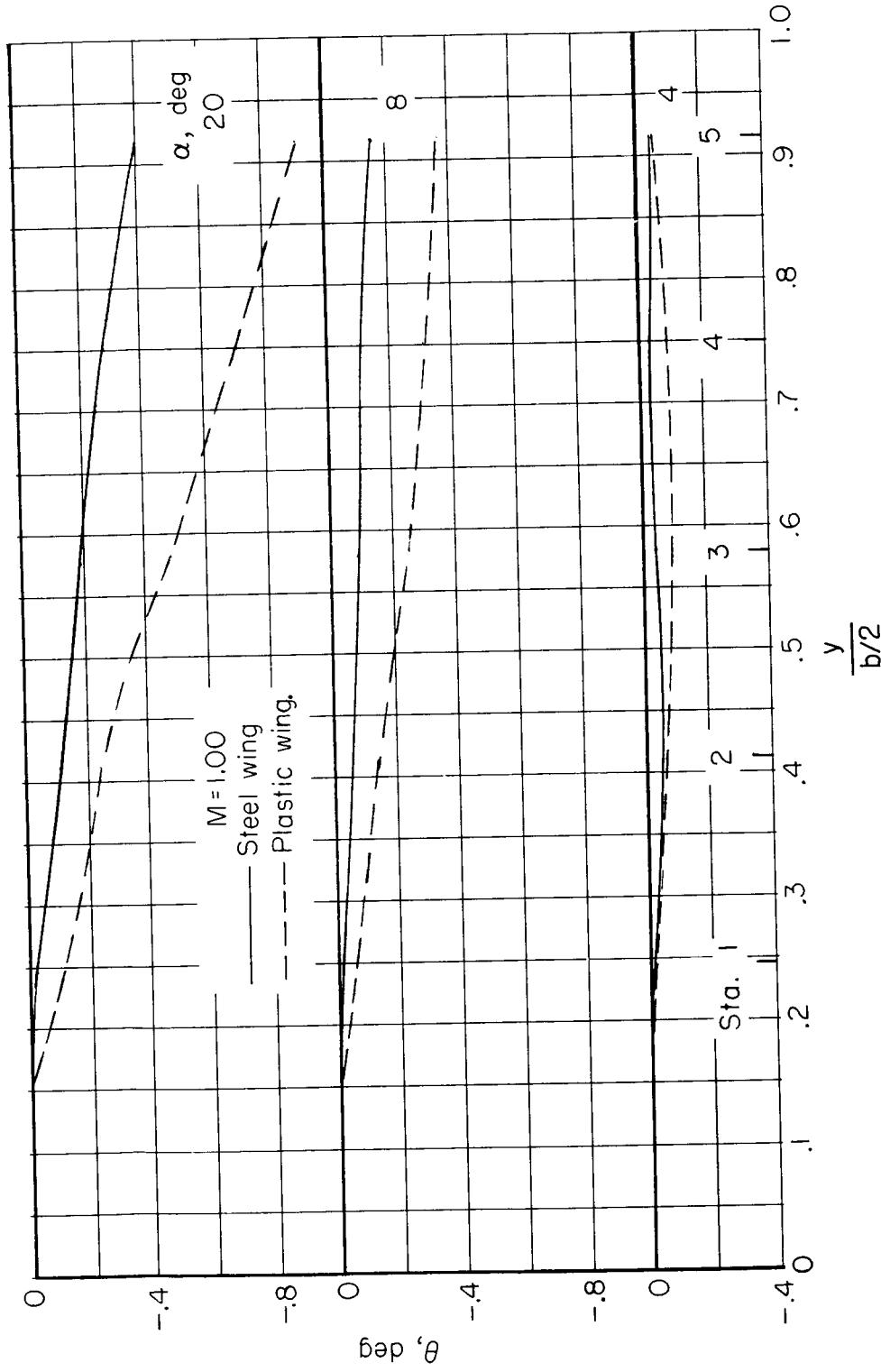
(b) $M = 1.00$.

Figure 10.- Concluded.

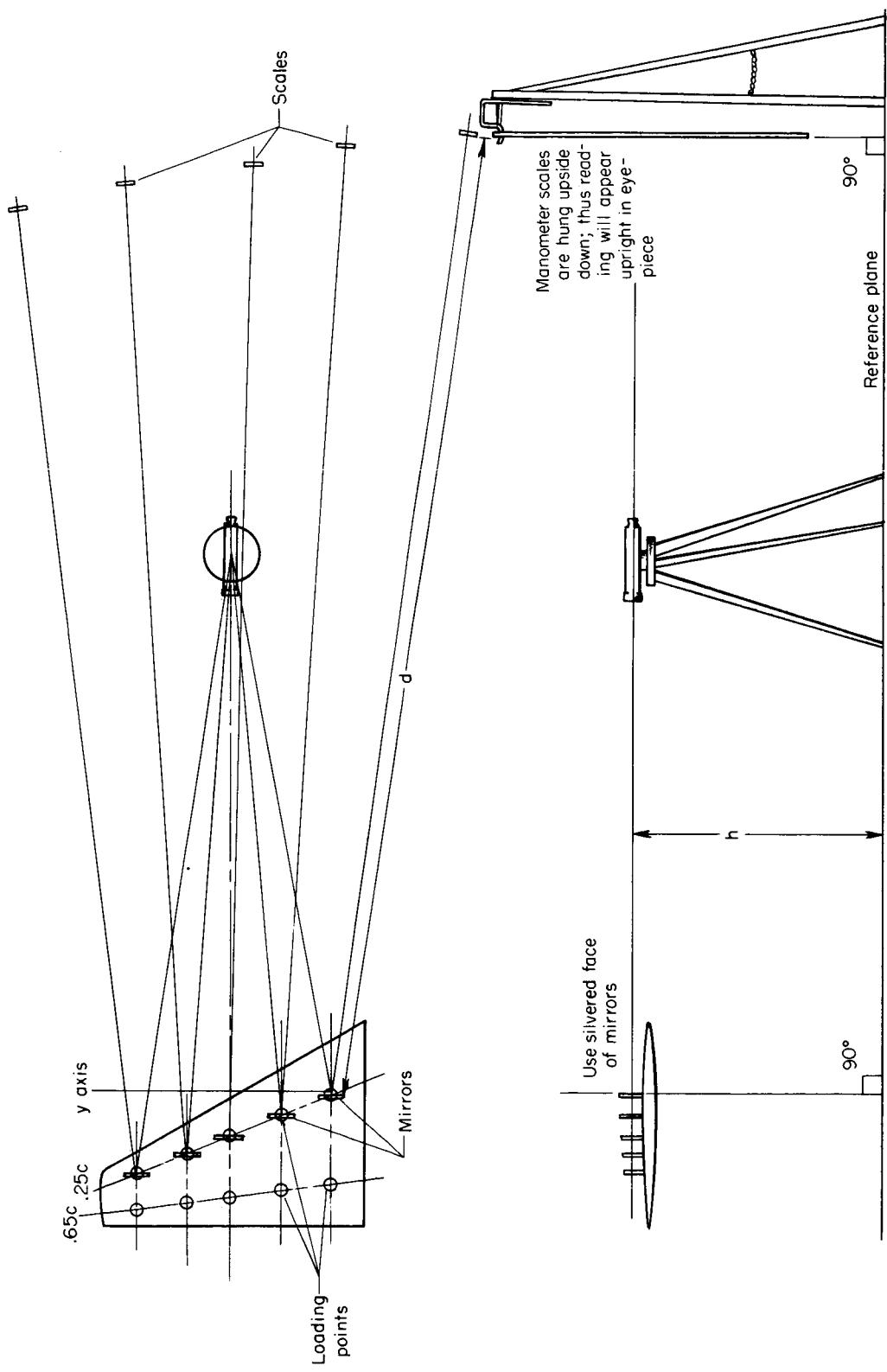


Figure 11.- Typical setup for measuring twist with mirrors.